Results of Proficiency Test Liquefied Propane & Sulfur (total) in LPG October 2019

Organised by: Institute for Interlaboratory Studies

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1 Introduction

Since 2009, the Institute for Interlaboratory Studies organizes a proficiency test for the analysis of Liquefied Propane every year. In 2017, at the request of several participants, the Institute of Interlaboratory Studies decided to organize an interlaboratory study for Sulfur (total) in LPG together with the Liquified Propane proficiency test. It was decided to continue both the interlaboratory study for Liquefied Propane as well as the interlaboratory study for Sulfur during the annual program 2019/2020.

Because iis has limited gas-handling facilities in place to prepare gas samples, a cooperation with EffecTech (Uttoxeter, United Kingdom) was set up for the Liquefied Propane PT (iis19S03P) and a co-operation with Praxair NV (Belgium) was set up for the Sulfur in LPG PT (iis19S03S). Both EffecTech and Praxair are fully equipped and have experience in the preparation of gas mixtures.

In the interlaboratory studies for Liquefied Propane 56 laboratories in 31 different countries and for Sulfur (total) in LPG 20 laboratories in 13 different countries registered for participation. In this report, the results of the 2019 proficiency tests Liquefied Propane and Sulfur (total) in LPG are presented and discussed. This report is also electronically available through the iis website www.iisnl.com.

2 SET UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, the Netherlands, was the organizer of this proficiency test (PT).

To optimize the costs for the participants for the Liquefied Propane PT (iis19S03P), it was decided to prepare one Liquefied Propane mixture for composition analyzes. The mixture was divided over a batch of 61 cylinders (1L cylinder with dip tube device). Each cylinder, filled with approximately 250 grams of Liquefied Propane mixture, was labelled #19215 and uniquely coded.

For the Sulfur in LPG PT (iis19S03S) it was decided to use a batch of 21 cylinders, filled with approximately 1500 grams of LPG, each spiked with Dimethyl Sulfide (DMS). Each cylinder (5L cylinder with dip tube device), was labelled #19216 and uniquely coded.

The limited cylinder sizes (1L and 5L) are chosen to optimize sample stability, cylinder costs, transport and handling costs.

The preparation and testing of the sample cylinders were subcontracted to ISO17025 accredited laboratories. Participants were requested to report rounded and unrounded test results. The unrounded test results were preferably used for statistical evaluation.

2.1 QUALITY SYSTEM

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, has implemented a quality system based on ISO/IEC17043:2010. This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentiality of participant's data. Feedback from the participants on the reported data is encouraged and customer's satisfaction is measured on a regular basis by sending out questionnaires.

EffecTech is accredited in conformance with ISO/IEC17043:2010 by UKAS (no. 4719) and ISO17025:2005 by UKAS (no. 0590). Praxair is accredited in conformance with ISO9001-2008, ISO14001-2004, ISO17025-No 159 Cal and ISO/TS16949.

2.2 PROTOCOL

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5). This protocol is electronically available through the iis website www.iisnl.com, from the FAQ page.

2.3 CONFIDENTIALITY STATEMENT

All data presented in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

2.4 SAMPLES

Liquefied Propane: sample #19215

One batch of 61 one liter cylinders with artificial Liquefied Propane mixture was prepared and tested for homogeneity by EffecTech (Uttoxeter, United Kingdom) in conformance with ISO guide 35:2006 and ISO17025:2005 (job 19/0968, August 2019). Each cylinder was labelled #19215 and uniquely coded. Every cylinder in the batch was analysed using 5 replicate measurements. The within bottle and between bottle variations were assessed in accordance with ISO Guide 35:2006 (Annex A.1). This procedure showed that the between bottle variations were small compared to the uncertainties on the reference values on each component. Hence, a single reference value could be safely assigned to the entire batch of samples.

The repeatability values (r) were calculated per component by multiplication of the respective standard deviation by 2.8. Subsequently, the calculated repeatabilities were compared with 0.3 times the corresponding reproducibility of the reference method in agreement with the procedure of ISO13528, Annex B2 in the next table.

| Component | r(observed) in %mol/mol | reference test method | 0.3*R(ref. test method) in %mol/mol |
|------------|----------------------------|--------------------------|--|
| Ethane | 0.0028 | D2163:14e1 | 0.0534 |
| Propane | 0.0285 | D2163:14e1 | 1.2527 |
| Propene | 0.0040 | D2163:14e1 | 0.0679 |
| iso-Butane | 0.0231 | D2163:14e1 | 0.0658 |
| n-Butane | 0.0104 | D2163:14e1 | 0.0576 |
| 1-Butene | 0.0012 | D2163:14e1 | 0.0192 |
| iso-Butene | 0.0026 | D2163:14e1 | 0.0199 |
| n-Pentane | 0.0093 | D2163:14e1 | 0.0257 |

Table 1: evaluation of the repeatabilities of samples #19215

Each calculated repeatability is less than 0.3 times the corresponding reproducibility of the reference method ASTM D2163:14e1(2019). Therefore, homogeneity of the subsamples #19215 was assumed.

Sulfur (total) in LPG: sample #19216

In this proficiency test, one batch of twenty-one 5L cylinders with artificial LPG mixture with Dimethylsulfide in Propane/n-Butane was prepared and tested for homogeneity by Praxair NV (Belgium) in conformance with ISO9001-2008, ISO14001-2004, ISO17025-No 159 Cal and ISO/TS 16949 in September 2019. Each cylinder was labelled #19216 and uniquely coded.

From the test results for Sulfur for all cylinders, the repeatability of the test results of this batch were calculated by multiplication of the deviation by 2.8. Subsequently, the calculated repeatability was compared with 0.3 times the corresponding reproducibility of the reference method in agreement with the procedure of ISO13528, Annex B2 in the next table.

| | Sulfur in mg/kg |
|----------------------------|--------------------|
| r (observed) | 2.9 |
| reference test method | ASTM D6667:14 |
| 0.3 * R (ref. test method) | 4.5 |

Table 2: evaluation of the repeatability of subsamples #19216

The calculated repeatability is less than 0.3 times the corresponding reproducibility of the reference test method ASTM D6667:14(2019). Therefore, homogeneity of the subsamples #19216 was assumed.

Depending on their registration to each of the participating laboratories one 1L cylinder of Liquefied Propane labelled #19215 and/or one 5L cylinder of Sulfur in LPG labelled #19216 was sent on October 2, 2019. An SDS was added to the sample package.

2.5 STABILITY OF THE SAMPLES

The shelf life time of the prepared gas cylinders is sufficient for the period of the proficiency test.

2.6 ANALYSES

The participants were asked to determine on the Liquefied Propane sample #19215 the composition: Ethane, Propane, Propene, iso-Butane, n-Butane, 1-Butene, iso-Butene, n-Pentane and to calculate several physical parameters from the composition: Molar Mass, Relative Density at 60°F, Absolute and Relative Vapor pressure at 100°F, Absolute and Relative Vapor pressure at 40°C, MON, Ideal Gross Heating Value and Ideal Net Heating Value at 14.696 psia and 60°F.

On the LPG sample #19216 the total Sulfur content was requested.

It was explicitly requested to treat the samples as if they were routine samples and to report the test results using the indicated units on the report form and not to round the test results but report as much significant figures as possible. It was also requested not to report 'less than' results, which are above the detection limit, because such test results cannot be used for meaningful statistical calculations.

To get comparable test results, a detailed report form and a letter of instructions are prepared. On the report form the reporting units are given as well as the appropriate reference test methods that will be used during the evaluation. The detailed report form and the letter of instructions are both made available on the data entry portal www.kpmd.co.uk/sgs-iis/. The participating laboratories are also requested to confirm the sample receipt on this data entry portal. The letter of instructions can also be downloaded from the iis website www.iisnl.com.

3 RESULTS

During five weeks after sample dispatch, the test results of the individual laboratories were gathered via the data entry portal www.kpmd.co.uk/sgs-iis/. The reported test results are tabulated per determination in appendix 1 of this report. The laboratories are presented by their code numbers.

Directly after the deadline, a reminder was sent to those laboratories that had not reported test results at that moment.

Shortly after the deadline, the available test results were screened for suspect data. A test result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the reported test results (no reanalysis). Additional or corrected test results are used for data analysis and original test results are placed under 'Remarks' in the test result tables in appendix 1. Test results that came in after the deadline were not taken into account in this screening for suspect data and thus these participants were not requested for checks.

3.1 STATISTICS

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of June 2018 (iis-protocol, version 3.5).

For the statistical evaluation the *unrounded* (when available) figures were used instead of the rounded test results. Test results reported as '<...' or '>...' were not used in the statistical evaluation.

First, the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test, a variant of the Kolmogorov-Smirnov test and by the calculation of skewness and kurtosis. Evaluation of the three normality indicators in combination with the visual evaluation of the graphic Kernel density plot, lead to judgement of the normality being either 'unknown', 'OK', 'suspect' or 'not OK'. After removal of outliers, this check was repeated. If a data set does not have a normal distribution, the results of the statistical evaluation should be used with due care.

According to ISO5725 the original test results per determination were submitted to Dixon's, Grubbs' and/or Rosner's outlier tests. Outliers are marked by D(0.01) for the Dixon's test, by G(0.01) or DG(0.01) for the Grubbs' test and by R(0.01) for the Rosner's test. Stragglers are marked by D(0.05) for the Dixon's test, by G(0.05) or DG(0.05) for the Grubbs' test and by R(0.05) for the Rosner's test. Both outliers and stragglers were not included in the calculations of averages and standard deviations.

For each assigned value, the uncertainty was determined in accordance with ISO13528. Subsequently the calculated uncertainty was evaluated against the respective requirement based on the target reproducibility in accordance with ISO13528. In this PT, the criterion of ISO13528, paragraph 9.2.1. was met for all evaluated tests, therefore, the uncertainty of all assigned values may be negligible and need not be included in the PT report.

Finally, the reproducibilities were calculated from the standard deviations by multiplying them with a factor of 2.8.

3.2 GRAPHICS

In order to visualize the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported test results are plotted. The corresponding laboratory numbers are on the X-axis.

The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected reference test method. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle.

Furthermore, Kernel Density Graphs were made. This is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. Also, a normal Gauss curve was projected over the Kernel Density Graph for reference.

3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements, e.g. ASTM or ISO reproducibilities, the z-scores were calculated using a target standard deviation. This results in an evaluation independent of the variation in this interlaboratory study.

The target standard deviation was calculated from the literature reproducibility by division with 2.8. In case no literature reproducibility was available, other target values were used. In some cases, a reproducibility based on former iis proficiency tests could be used.

When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate whether the reported test result is fit-for-use.

The z-scores were calculated according to:

```
z_{\text{(target)}} = (test result - average of PT) / target standard deviation
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The $z_{(target)}$ scores are listed in the test result tables in appendix 1.

Absolute values for z<2 are very common and absolute values for z>3 are very rare. The usual interpretation of z-scores is as follows:

|z| < 1 good 1 < |z| < 2 satisfactory 2 < |z| < 3 questionable 3 < |z| unsatisfactory

4 EVALUATION

In this interlaboratory study, some problems were encountered with the dispatch of the samples. For the Liquefied Propane PT (iis19S03P), not all laboratories did report all test results requested. One participant reported test results after the deadline and ten participants did not report any test result at all.

In total 46 participants reported 574 numerical test results. Observed were 48 outlying test results, which is 8.4%. In proficiency studies outlier percentages of 3% - 7.5% are quite normal.

For the Sulfur in LPG PT (iis19S03S), seven participants did not report any result at all. In total 13 participants reported 13 numerical test results. No outlying test results were observed.

Not all original data sets proved to have normal Gaussian distribution. These are referred to as "not OK" or "suspect". The statistical evaluation of these data sets should be used with due care, see also paragraph 3.1.

4.1 EVALUATION PER SAMPLE AND PER TEST

In this section, the reported test results are discussed per sample and per test. The test methods, which were used by the various laboratories, were taken into account for explaining the observed differences when possible and applicable. These test methods are also in the tables together with the original data. The abbreviations used in these tables are explained in appendix 3.

In the iis PT reports, ASTM methods are referred to with a number (e.g. D2163) and an added designation for the year that the method was adopted or revised (e.g. D2163:14e1). If applicable, a designation in parentheses is added to designate the year of reapproval (e.g. D2163:14e1(2019)). In the test results tables of appendix 1 only the method number and year of adoption or revision (e.g. D2163:14e1) will be used.

Because the majority of the participating laboratories used ASTM D2163 as test method for the determination of the Propane Composition, it was decided to use the reproducibilities of this test method as target reproducibilities, and to mention the reproducibilities of EN27941 (identical to IP405 and ISO7941) for reference only. In ASTM D2163 no reproducibilities of 1-

butene and iso-butene are mentioned, the reproducibilities of n-butane were used to calculate the reproducibilities of these two components.

Two laboratories (1011 and 1528) reported deviating test results for many of the gas composition test results. At least six of the eight test results were statistical outliers. As the eight test results are not independent, it was decided not to use any of the reported results of these two laboratories for the statistical evaluation.

For comparison to the reported test results for the Physical Properties, iis calculated these Physical Properties for all laboratories that reported composition results. In the statistical evaluation of these calculated properties, the calculated results of above mentioned two laboratories were excluded as well as the calculated results of four other laboratories (333, 334, 337 and 508) with three or four outliers in the composition. For extra information on the calculated parameters, see paragraph 5 Discussion.

Liquefied Propane: sample #19215

Ethane:

The determination of this component was not problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D2163:14e1(2019) and also with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).

Propane:

The determination of this component was not problematic. One statistical outlier was observed and one other test result was excluded. However, the calculated reproducibility after rejection of the suspect data is in agreement with the requirements of ASTM D2163:14e1(2019) and also in agreement with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).

Propene:

The determination of this component was not problematic. Four statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in good agreement with the requirements of ASTM D2163:14e1(2019) and also with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).

iso-Butane:

The determination of this component was not problematic. Six statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D2163:14e1(2019) and also with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).

n-Butane:

The determination of this component was not problematic. Six statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D2163:14e1 (2019) and also with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).

1-Butene:

The determination of this component may not be problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the estimated requirements of ASTM D2163:14e1(2019) and also with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).

iso-Butene:

The determination of this component may not be problematic. Two statistical outliers were observed and one other test result was excluded. However, the calculated reproducibility after rejection of the suspect data is in agreement with the estimated requirements of ASTM D2163:14e1(2019) and also with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).

n-Pentane:

The determination of this component was problematic for several laboratories. Seven statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D2163:14e1(2019) and also with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).

Molar Mass:

This calculated parameter may not be problematic. Two statistical outliers were observed and two test results were excluded. The calculated reproducibility after rejection of the suspect data is in line with the calculated reproducibility using the published molar mass factors obtained from ASTM D2421:18 over all reported component concentrations (0.08 vs. 0.07 g/mol).

Rel. Density at 60°F: This calculated parameter may not be problematic. Three statistical outliers were observed and one other test result was excluded. The calculated reproducibility after rejection of the suspect data is in line with the calculated reproducibility using the published relative density factors obtained from ASTM D2598:16 over all reported component concentrations (0.0004 vs. 0.0004).

<u>Abs. VP at 100°F:</u> As the reported results calculated via ISO8973 and ASTM D2598 are not identical, it was decided to evaluate the test results for both methods separately.

ISO8973; This calculated parameter may not be problematic. Two statistical outliers were observed (both calculation errors). The calculated reproducibility after rejection of statistical outlier is smaller than the calculated reproducibility using the published vapor pressure factors obtained from ISO8973:97 over all reported component concentrations (0.25 *vs* 0.97 psi).

ASTM D2598; This calculated parameter may not be problematic. No statistical outliers were observed. The calculated reproducibility is in line with the calculated reproducibility using the published vapor pressure factors obtained from ASTM D2598:16 over all reported component concentrations (0.80 vs. 0.96 psi).

Rel. VP at 100°F: As the reported results calculated via ISO8973 and ASTM D2598 are not identical, it was decided to evaluate the test results for both methods separately.

ISO8973; This calculated parameter may not be problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of statistical outliers is smaller than the calculated reproducibility using the published vapor pressure factors obtained from ISO8973:97 over all reported component concentrations (0.26 *vs* 0.97 psi).

ASTM D2598; This calculated parameter may be problematic. One statistical outlier was observed and one other test result excluded (both also calculation errors). The calculated reproducibility after rejection of the suspect data is larger than the calculated reproducibility using the published vapor pressure factors obtained from ASTM D2598:16 over all reported component concentrations (1.27 vs. 0.96 psi).

Abs. VP at 40°C: This determination may not be problematic. Two statistical outliers were observed (both calculation errors) and one test result was excluded. The calculated reproducibility after rejection of the suspect data is smaller than the calculated reproducibility using the published vapor pressure factors obtained from ISO8973:97 over all reported component concentrations (4.8 vs. 6.9 kPa).

Rel. VP at 40°C: This determination may not be problematic. Two statistical outliers were observed (both calculation errors) and three other test results were excluded. The calculated reproducibility after rejection of the suspect data is in line with the calculated reproducibility using the published vapor pressure factors obtained from ISO8973:97 over all reported component concentrations (5.4 vs. 6.9 kPa).

MON:

As the reported results calculated via EN589 and ASTM D2598 are not identical, it was decided to evaluate the test results for both methods separately.

EN589; This calculated parameter may not be problematic. Two statistical outliers were observed and two test results were excluded. The calculated reproducibility after rejection of suspect data is smaller than the calculated reproducibility using the published vapor pressure factors obtained from EN589:18 over all reported component concentrations (0.03 *vs* 0.05). D2598; Five test results were reported, so no conclusions could be drawn.

Ideal Gross Heating Value at 14.696 psia / 60°F: Almost all laboratories reported to have calculated according to ASTM D3588. This calculated parameter may not be problematic. One statistical outlier was observed (also a calculation error) and one test result was excluded. The calculated reproducibility after rejection of the suspect data is in line with the calculated reproducibility using the published Ideal Gross Heating Values obtained from EN3588:98(2017) over all reported component concentrations (3 vs 3).

Ideal Net Heating Value at 14.696 psia / 60°F: Almost all laboratories reported to have calculated according to ASTM D3588. This calculated parameter may not be problematic. One statistical outlier was observed (also a calculation error) and one test result was excluded. The calculated reproducibility after rejection of the suspect data is in line with the calculated reproducibility using the published Ideal Net Heating Values obtained from EN3588:98(2017) over all reported component concentrations (3 vs 3).

Sulfur in LPG: sample #19216

Sulfur, total:

The determination of this component was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D6667:14(2019).

4.2 Performance evaluation for the group of Laboratories

A comparison has been made between the reproducibility as declared by the relevant reference test method and the reproducibility as found for the group of participating laboratories. The number of significant test results, the average result, the calculated reproducibility (2.8 * standard deviation) and the target reproducibility derived from literature reference test methods (in casu ASTM, ISO and EN standards) are presented in the next tables.

| Component | unit | n | average | 2.8 * sd | R(D2163) in %mol | R(EN27941) in %mol |
|------------|----------|----|---------|----------|----------------------------|------------------------------|
| Ethane | %mol/mol | 44 | 0.351 | 0.112 | 0.163 | 0.299 |
| Propane | %mol/mol | 44 | 93.39 | 0.69 | 4.17 | 1.02 |
| Propene | %mol/mol | 42 | 0.688 | 0.057 | 0.223 | 0.213 |
| iso-Butane | %mol/mol | 40 | 2.095 | 0.175 | 0.222 | 0.386 |
| n-Butane | %mol/mol | 40 | 2.177 | 0.189 | 0.195 | 0.386 |
| 1-Butene | %mol/mol | 44 | 0.189 | 0.031 | 0.065 | 0.160 |
| iso-Butene | %mol/mol | 43 | 0.202 | 0.035 | 0.067 | 0.160 |
| n-Pentane | %mol/mol | 39 | 0.850 | 0.084 | 0.087 | 0.311 |

Table 3: reproducibilities of composition tests on sample #19215

| Parameter | unit | n | average | 2.8 * sd | R (all calc.) |
|-----------------------|-------|----|---------|----------|---------------|
| Molar Mass | g/mol | 24 | 44.92 | 0.08 | 0.07 |
| Rel. Density at 60°F | | 27 | 0.5119 | 0.0004 | 0.0004 |
| Abs. VP at 100°F-ISO | psi | 10 | 185.8 | 0.3 | 1.0 |
| Abs. VP at 100°F-ASTM | psi | 7 | 181.8 | 0.8 | 1.0 |
| Rel. VP at 100°F-ISO | psi | 12 | 171.1 | 0.3 | 1.0 |
| Rel. VP at 100°F-ASTM | psi | 10 | 167.1 | 1.3 | 1.0 |
| Abs. VP at 40°C | kPa | 22 | 1317 | 5 | 7 |
| Rel. VP at 40°C | kPa | 20 | 1216 | 5 | 7 |
| MON – EN589 | | 13 | 95.09 | 0.03 | 0.05 |
| MON – D2598 | | 5 | 96.29 | (1.00)* | 0.06 |

| Parameter | unit | n | average | 2.8 * sd | R (all calc.) |
|----------------|--------|----|---------|----------|---------------|
| Ideal Gross HV | kJ/mol | 11 | 2259 | 3 | 3 |
| Net Gross HV | kJ/mol | 11 | 2079 | 3 | 3 |

Table 4: reproducibilities of calculated parameters on sample #19215

all calc. = calculated over all reported composition test results excluded the suspect data.

| Component | unit | n | average | 2.8 * sd | R(lit) |
|---------------|-------|----|---------|----------|--------|
| Sulfur, total | mg/kg | 13 | 44.0 | 12.4 | 13.9 |

Table 5: reproducibility of test on sample #19216

Without further statistical calculations it can be concluded that for a large number of parameters there is a good compliance of the group of participating laboratories with the relevant reference test methods for the component determination. The problematic tests have been discussed in paragraph 4.1.

4.3 COMPARISON OF THE PROFICIENCY TEST OF OCTOBER 2019 WITH PREVIOUS PTS

| | October 2019 | October 2018 | October 2017 | October 2016 | October 2015 |
|----------------------------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Number of reporting laboratories | 46 | 44 | 47 | 43 | 41 |
| Number of test results reported | 574 | 495 | 536 | 472 | 468 |
| Number of statistical outliers | 48 | 20 | 30 | 34 | 24 |
| Percentage outliers | 8.4% | 4.0% | 5.6% | 7.2% | 5.1% |

Table 6: comparison with previous proficiency tests on Liquefied Propane (excluded Sulfur in LPG)

| | October 2019 | October 2018 | October 2017 |
|----------------------------------|-----------------|-----------------|-----------------|
| Number of reporting laboratories | 13 | 15 | 8 |
| Number of test results reported | 13 | 15 | 8 |
| Number of statistical outliers | 0 | 1 | 1 |
| Percentage outliers | 0% | 6.7% | 12.5% |

Table 7: comparison with previous proficiency tests on Sulfur in LPG only

In proficiency tests, outlier percentages of 3% - 7.5% are quite normal.

The performance of the determinations of the proficiency tests was compared against the requirements of the reference test methods. The conclusions are given the following tables.

^{*)} results in brackets based on only five test results.

| Component | October 2019 | October 2018 | October 2017 | October 2016 | October 2015 |
|------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Ethane | + | ++ | ++ | ++ | ++ |
| Propane | ++ | ++ | ++ | ++ | ++ |
| Propene | ++ | ++ | ++ | ++ | + |
| iso-Butane | + | - | +/- | - | + |
| n-Butane | +/- | | - | - | - |
| 1-Butene | ++ | + | ++ | ++ | ++ |
| iso-Butene | + | + | ++ | + | ++ |
| n-Pentane | +/- | - | - | - | - |

Table 8: comparison determinations on Liquefied Propane against the requirements of the reference test methods

| Component | October | October | October |
|---------------|---------|---------|---------|
| | 2019 | 2018 | 2017 |
| Sulfur, total | + | - | + |

Table 9: comparison determinations on Sulfur in LPG against the requirements of the reference test methods

The following performance categories were used:

- ++: group performed much better than the reference test method
- + : group performed better than the reference test method
- +/-: group performance equals the reference test method
- : group performed worse than the reference test method
- -- : group performed much worse than the reference test method

5 DISCUSSION

Because several of the reproducibility requirements of ASTM D2163 differ significantly from the reproducibility requirements of EN27941 (for liquid injection), the outcome of the evaluation will be strongly dependent on the target test method selected for the evaluation.

The consensus values as determined in this PT are compared with the average values from the homogeneity testing by EffecTech, United Kingdom in the following table.

| Parameter | Average by EffecTech in %mol/mol | Average from participants in %mol/mol | Difference in %mol/mol | z-score |
|------------|--|---------------------------------------|---------------------------|---------|
| Ethane | 0.401 | 0.351 | 0.051 | 0.87 |
| Propane | 93.570 | 93.394 | 0.176 | 0.12 |
| Propene | 0.706 | 0.688 | 0.018 | 0.23 |
| iso-Butane | 2.037 | 2.095 | -0.058 | -0.73 |
| n-Butane | 2.095 | 2.177 | -0.082 | -1.17 |
| 1-Butene | 0.182 | 0.189 | -0.007 | -0.31 |
| iso-Butene | 0.198 | 0.202 | -0.004 | -0.16 |
| n-Pentane | 0.811 | 0.850 | -0.040 | -1.30 |

Table 10: comparison of consensus values with values determined by EffecTech

From this comparison it is clear that <u>all</u> consensus values as determined in this PT are in line with the values as determined by EffecTech during the preparation of the cylinders.

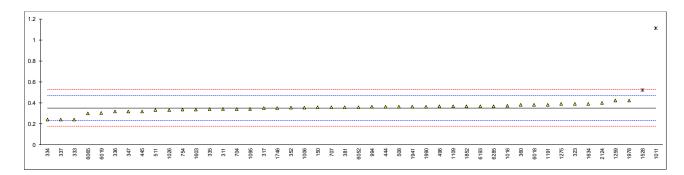
For the calculation of the Molar Mass, Relative Density, Vapor Pressure, Motor Octane Number and Heating Value several standardized test methods are available, e.g. ASTM D2421 for the interconversion of the units to gas-volume, liquid-volume or mass basis. Also, different test methods for the calculation of the Vapor Pressure do exist. In ISO8973 (identical to IP432) the Vapor Pressure is calculated from the mole fraction per component and a Vapor Pressure factor of that component (given for all components). In ASTM D2598 the Vapor Pressure is calculated from the liquid volume percentage per component and a Vapor Pressure factor of that component (given for only several components). The selection of the tables to be used for the calculations may cause additional variation.

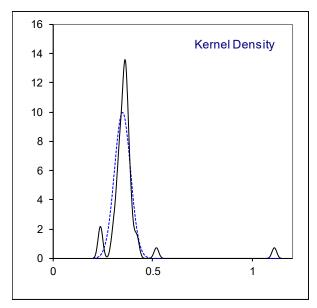
It is remarkable to see that the results for Vapor Pressure from the ASTM D2598 calculation are significantly lower than the results from the ISO8973/IP432 calculation. The observed difference is caused by a difference in the VP factor of Ethane. ASTM (Subcommittee D02.H) commented (see also appendix 3, literature: 15):

"The vapor pressure of ethane in D2598 was revised a few times prior to 2002. The current value, 611 psi, has remained the same for the last ten years. The revision of ethane was done because components in LPG blends do not necessarily behave as ideal gases. In particular, properties of ethane and ethylene appear to differ from ideality. Factors for these two components have been modified from 'ideal gas' values to make the calculated vapor pressure results more closely approximate actual measured vapor pressures of LPG blends. (i.e. D1267). Chapter 2 of Fuels and Lubricants Handbook (George Totten, © 2003), states that calculated vapor pressure were found to be biased high relative to experimental vapor pressure measured by D1267 for high ethane samples in earlier versions of D2598'.

APPENDIX 1
Determination of Ethane on sample #19215; results in %mol/mol

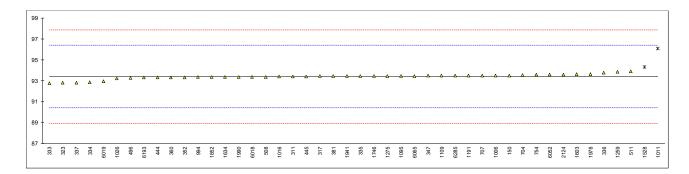
| | | - | | | remarks |
|------|----------------------|----------|------------|-------|-------------------------------------|
| | method | value | mark | | remarks |
| | D2163 | 0.360 | | 0.16 | |
| 171 | 50400 | | | | |
| | D2163 | 0.34 | | -0.18 | |
| | D2163 | 0.35 | | -0.01 | |
| | D2163 | 0.39 | | 0.68 | |
| | D2163 | 0.24 | | -1.90 | |
| 334 | D2163 | 0.24 | | -1.90 | |
| 335 | D2163 | 0.34 | | -0.18 | |
| 336 | EN27941 | 0.32 | | -0.53 | |
| 337 | D2163 | 0.24 | | -1.90 | |
| | D2163 | 0.320 | | -0.53 | |
| | EN27941 | 0.3541 | | 0.06 | |
| 360 | EN27941 | 0.38 | | 0.51 | |
| | EN27941 | 0.36 | | 0.16 | |
| 444 | IP405 | 0.362 | | 0.20 | |
| | D2163 | 0.32 | | -0.53 | |
| | D2163 | 0.369 | | 0.32 | |
| | D2163 | 0.362675 | | 0.21 | |
| | D2163 | 0.33 | С | | first reported: 0.19 |
| 529 | **** | | - | | 1 |
| | D2163 | 0.340 | | -0.18 | |
| | D2163 | 0.360 | | 0.16 | |
| | D2163 | 0.335 | | -0.27 | |
| 868 | 52100 | | | -0.27 | |
| | D2163 | 0.3614 | | 0.19 | |
| | D2163 | 0.356 | | 0.19 | |
| | ISO7941 | 1.11 | C,R(0.01) | | first reported: 1.1 |
| 1011 | 1007341 | 1.11 | C,11(0.01) | | ilist reported. 1.1 |
| | ISO7941 | 0.373 | | 0.39 | |
| | ISO7941 | 0.3336 | | -0.29 | |
| | ISO7941 | 0.3330 | | -0.29 | |
| | IP405 | 0.37 | | 0.33 | |
| | IP473 | 0.37 | | 0.53 | |
| | 15473 | | | 0.32 | |
| 1197 | | | | | |
| 1198 | EN27044 | 0.422 | | 1.23 | |
| | EN27941 | 0.422 | | | |
| | EN27941 | 0.38895 | D(0.01) | 0.66 | |
| | EN27941 | 0.52 | R(0.01) | 2.91 | |
| | In house | 0.3371 | | -0.23 | |
| | ISO7941 | 0.39 | | 0.68 | |
| 1720 | D2163 | 0.35 | | -0.01 | |
| 1746 | D2 103 | 0.55 | | -0.01 | |
| | DIN51619 | 0.37 | | 0.33 | |
| 1941 | DIN51619 DIN51619 | 0.364 | | 0.33 | |
| | D1N51619 D2163 | 0.364 | | 1.24 | |
| | IP473 | 0.4226 | | 0.25 | |
| | D2163 | 0.303 | | 0.23 | |
| | ISO7941 | 0.401 | | 0.67 | |
| | ISO7941 | 0.304 | | -0.80 | |
| | D2163 | 0.36 | | 0.16 | |
| | D2163 D2163 | 0.3020 | | -0.83 | |
| | D2163 D2163 | 0.3020 | | 0.33 | |
| 6201 | DZ 100 | | | | |
| 6215 | | | | | |
| | EN27941 | 0.37 | | 0.33 | |
| 0200 | ENZ/941 | 0.37 | | 0.33 | |
| | normality | not OK | | | |
| | n | 44 | | | |
| | outliers | 2 | | | |
| | mean (n) | 0.3506 | | | |
| | st.dev. (n) | 0.04012 | | | |
| | R(calc.) | 0.04012 | | | |
| | st.dev.(D2163:14e1) | 0.1123 | | | |
| | R(D2163:14e1) | 0.03616 | | | Compare R(EN27941:93(liq)) = 0.2986 |
| | 1 (02 100.1701) | 0.1020 | | | 0.2000 |

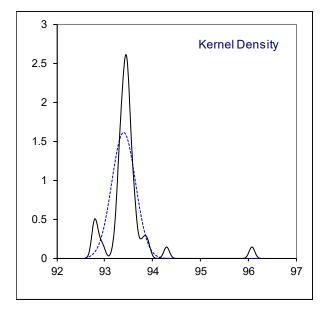




Determination of Propane on sample #19215; results in %mol/mol

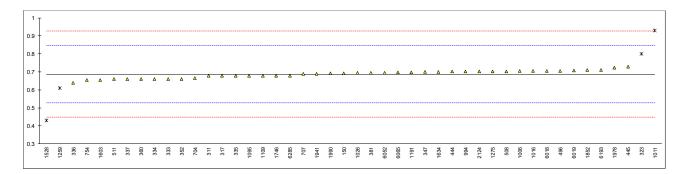
| lab | method | value | mark | z(targ) | remarks |
|--------------|--------------------------------------|-------------------|-----------|----------------|--|
| 150 | D2163 | 93.514 | | 0.08 | |
| 171 | | | | | |
| 311 | D2163 | 93.41 | | 0.01 | |
| 317 | D2163 | 93.43 | | 0.02 | |
| 323 | D2163 | 92.79 | | -0.41 | |
| 333 | D2163 | 92.77 | | -0.42 | |
| 334 | D2163 | 92.86 | | -0.36 | |
| 335 | D2163 | 93.44 | | 0.03 | |
| 336 337 | EN27941 D2163 | 93.76 92.79 | | 0.25 -0.41 | |
| 347 | D2163 | 93.479 | | 0.06 | |
| 352 | EN27941 | 93.31 | | -0.06 | |
| 360 | EN27941 | 93.30 | | -0.06 | |
| 381 | EN27941 | 93.435 | | 0.03 | |
| 444 | IP405 | 93.297 | | -0.06 | |
| 445 | D2163 | 93.41 | | 0.01 | |
| 496 | D2163 | 93.282 | | -0.07 | |
| 508 | D2163 | 93.375151 | | -0.01 | |
| 511 529 | D2163 | 93.9 | | 0.34 | |
| 704 | D2163 | 93.528 | | 0.09 | |
| 707 | D2163 | 93.506 | | 0.08 | |
| 754 | D2163 | 93.575 | | 0.12 | |
| 868 | | | | | |
| 994 | D2163 | 93.3338 | | -0.04 | |
| 1006 | D2163 | 93.507 | | 0.08 | |
| 1011 | ISO7941 | 96.07 | C,R(0.01) | 1.80 | first reported: 97.0 |
| 1012 | 1007044 | | | | |
| 1016 1026 | ISO7941 ISO7941 | 93.399 93.2066 | | 0.00 -0.13 | |
| 1020 | ISO7941 | 93.46 | | 0.04 | |
| 1109 | IP405 | 93.49 | | 0.06 | |
| 1191 | IP473 | 93.503 | | 0.07 | |
| 1197 | | | | | |
| 1198 | | | | | |
| 1259 | EN27941 | 93.839 | | 0.30 | |
| 1275 | EN27941 | 93.4409 | | 0.03 | As a form a south as a shared and a source are sound to find |
| 1528 | EN27941 | 94.29 93.6161 | ex | 0.60 0.15 | test result excluded, see paragraph 4.1 |
| 1603 1634 | In house ISO7941 | 93.36 | | -0.02 | |
| 1720 | 1007541 | | | -0.02 | |
| 1746 | D2163 | 93.44 | | 0.03 | |
| 1786 | | | | | |
| 1852 | DIN51619 | 93.35 | | -0.03 | |
| 1941 | DIN51619 | 93.436 | | 0.03 | |
| 1978 | D2163 | 93.6441 | | 0.17 | |
| 1990 | IP473 | 93.366 | | -0.02 | |
| 2124 6018 | D2163 ISO7941 | 93.600 93.373 | | 0.14 -0.01 | |
| 6019 | ISO7941 | 93.373 | | -0.01 -0.29 | |
| 6052 | D2163 | 93.5934 | | 0.13 | |
| 6065 | D2163 | 93.4660 | | 0.05 | |
| 6193 | D2163 | 93.29 | | -0.07 | |
| 6201 | | | | | |
| 6215 | EN107044 | | | | |
| 6285 | EN27941 | 93.49 | | 0.06 | |
| | normality | suspect | | | |
| | n | 44 | | | |
| | outliers | 1 (+1ex) | | | |
| | mean (n) | 93.3937 | | | |
| | st.dev. (n) | 0.24677 | | | |
| | R(calc.) | 0.6910 | | | |
| | st.dev.(D2163:14e1) R(D2163:14e1) | 1.48932 4.1701 | | | Compare R(EN27941:93(liq)) = 1.0181 |
| | N(DZ 103.1461) | 4.1/01 | | | Compare Γ(ΕΝΖ1941.93(IIQ)) = 1.0101 |

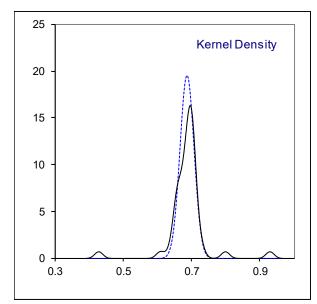




Determination of Propene on sample #19215; results in %mol/mol

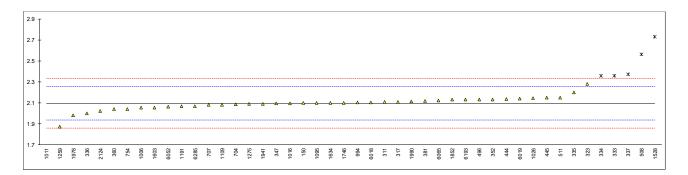
| lab | method | value | mark | z(targ) | remarks |
|--------------|---------------------|-------------------|-----------|----------------|-------------------------------------|
| 150 | D2163 | 0.693 | | 0.07 | |
| 171 | | | | | |
| 311 | D2163 | 0.68 | | -0.10 | |
| 317 | D2163 | 0.68 | | -0.10 | |
| 323 | D2163 | 0.80 | R(0.01) | 1.41 | |
| 333 | D2163 | 0.66 | | -0.35 | |
| 334 | D2163 | 0.66 | | -0.35 | |
| 335 336 | D2163 EN27941 | 0.68 0.64 | | -0.10 | |
| 337 | D2163 | 0.66 | | -0.60 -0.35 | |
| 347 | D2163 | 0.700 | | 0.15 | |
| 352 | EN27941 | 0.6610 | | -0.34 | |
| 360 | EN27941 | 0.66 | | -0.35 | |
| 381 | EN27941 | 0.694 | | 0.08 | |
| 444 | IP405 | 0.7015 | | 0.17 | |
| 445 | D2163 | 0.73 | | 0.53 | |
| 496 508 | D2163 D2163 | 0.705 0.703672 | | 0.22 0.20 | |
| 506 511 | D2163 D2163 | 0.703672 | | -0.35 | |
| 529 | D2100 | | | -0.00 | |
| 704 | D2163 | 0.666 | | -0.27 | |
| 707 | D2163 | 0.690 | | 0.03 | |
| 754 | D2163 | 0.655 | | -0.41 | |
| 868 | | | | | |
| 994 | D2163 | 0.7016 | | 0.17 | |
| 1006 | D2163 | 0.704 | C D(0.01) | 0.20 | first reported: 0.0 |
| 1011 1012 | ISO7941 | 0.93 | C,R(0.01) | 3.05 | first reported: 0.9 |
| 1012 | ISO7941 | 0.704 | | 0.20 | |
| 1026 | ISO7941 | 0.6934 | | 0.07 | |
| 1095 | ISO7941 | 0.68 | | -0.10 | |
| 1109 | IP405 | 0.68 | | -0.10 | |
| 1191 | IP473 | 0.697 | | 0.12 | |
| 1197 1198 | | | | | |
| 1259 | EN27941 | 0.610 | R(0.05) | -0.98 | |
| 1275 | EN27941 | 0.70235 | 11(0.00) | 0.18 | |
| 1528 | EN27941 | 0.43 | R(0.01) | -3.24 | |
| 1603 | In house | 0.6552 | ` , | -0.41 | |
| 1634 | ISO7941 | 0.70 | | 0.15 | |
| 1720 | D0400 | | | | |
| 1746 1786 | D2163 | 0.68 | | -0.10 | |
| 1852 | DIN51619 | 0.71 | | 0.28 | |
| 1941 | DIN51619 | 0.690 | | 0.03 | |
| 1978 | D2163 | 0.7231 | | 0.44 | |
| 1990 | IP473 | 0.691 | | 0.04 | |
| 2124 | D2163 | 0.702 | | 0.18 | |
| 6018 | ISO7941 | 0.704 | | 0.20 | |
| 6019 | ISO7941 | 0.708 | | 0.25 | |
| 6052 6065 | D2163 | 0.6951 0.6966 | | 0.09 0.11 | |
| 6193 | D2163 D2163 | 0.0900 | | 0.11 | |
| 6201 | D2100 | | | | |
| 6215 | | | | | |
| 6285 | EN27941 | 0.68 | | -0.10 | |
| | | OK | | | |
| | normality | OK 42 | | | |
| | n outliers | 42 4 | | | |
| | mean (n) | 0.6878 | | | |
| | st.dev. (n) | 0.02041 | | | |
| | R(calc.) | 0.0572 | | | |
| | st.dev.(D2163:14e1) | 0.07951 | | | Compare B/EN27041:02/lia\\ = 0.2424 |
| | R(D2163:14e1) | 0.2226 | | | Compare R(EN27941:93(liq)) = 0.2134 |

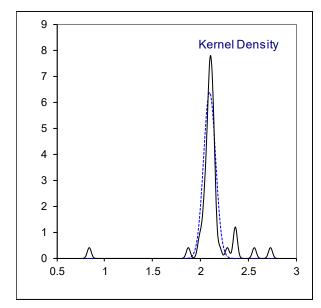




Determination of iso-Butane on sample #19215; results in %mol/mol

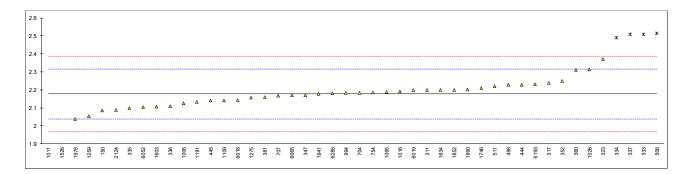
| lab | method | value | mark | z(targ) | remarks |
|--------------|-------------------------|-------------------|-----------|---------------|-------------------------------------|
| 150 | D2163 | 2.099 | | 0.05 | |
| 171 | -: | | | | |
| 311 | D2163 | 2.11 | | 0.19 | |
| 317 | D2163 | 2.11 | | 0.19 | |
| 323 | D2163 | 2.28 | | 2.33 | |
| 333 | D2163 | 2.36 | R(0.01) | 3.34 | |
| 334 | D2163 | 2.36 | R(0.01) | 3.34 | |
| 335 | D2163 | 2.20 | | 1.32 | |
| 336 337 | EN27941 D2163 | 2.00 2.37 | R(0.01) | -1.20 3.47 | |
| 347 | D2163 | 2.094 | 13(0.01) | -0.01 | |
| 352 | EN27941 | 2.1334 | | 0.48 | |
| 360 | EN27941 | 2.04 | | -0.70 | |
| 381 | EN27941 | 2.12 | | 0.31 | |
| 444 | IP405 | 2.134 | | 0.49 | |
| 445 | D2163 | 2.15 | | 0.69 | |
| 496 | D2163 | 2.133 | D(0.04) | 0.48 | |
| 508 | D2163 | 2.561268 | R(0.01) | 5.88 | |
| 511 529 | D2163 | 2.15 | | 0.69 | |
| 704 | D2163 | 2.088 | | -0.09 | |
| 707 | D2163 | 2.080 | | -0.19 | |
| 754 | D2163 | 2.04 | | -0.70 | |
| 868 | | | | | |
| 994 | D2163 | 2.1052 | | 0.13 | |
| 1006 | D2163 | 2.054 | | -0.52 | |
| 1011 | ISO7941 | 0.84 | C,R(0.01) | -15.84 | first reported: 0.8 |
| 1012 | 1007044 | 2.005 | | 0.00 | |
| 1016 1026 | ISO7941 ISO7941 | 2.095 2.1436 | | 0.00 0.61 | |
| 1020 | ISO7941 | 2.1430 | | 0.06 | |
| 1109 | IP405 | 2.08 | | -0.19 | |
| 1191 | IP473 | 2.066 | | -0.37 | |
| 1197 | | | | | |
| 1198 | | | | | |
| 1259 | EN27941 | 1.873 | | -2.80 | |
| 1275 | EN27941 | 2.09215 | D(0.04) | -0.04 | |
| 1528 | EN27941 | 2.73 | R(0.01) | 8.01 -0.52 | |
| 1603 1634 | In house ISO7941 | 2.0540 2.10 | | 0.06 | |
| 1720 | 1007541 | | | | |
| 1746 | D2163 | 2.10 | | 0.06 | |
| 1786 | | | | | |
| 1852 | DIN51619 | 2.13 | | 0.44 | |
| 1941 | DIN51619 | 2.093 | | -0.03 | |
| 1978 | D2163 IP473 | 1.9840 | | -1.40 0.23 | |
| 1990 2124 | D2163 | 2.113 2.025 | | -0.89 | |
| 6018 | ISO7941 | 2.106 | | 0.14 | |
| 6019 | ISO7941 | 2.142 | | 0.59 | |
| 6052 | D2163 | 2.0655 | | -0.37 | |
| 6065 | D2163 | 2.1235 | | 0.36 | |
| 6193 | D2163 | 2.13 | | 0.44 | |
| 6201 | | | | | |
| 6215 6285 | EN27941 | 2.07 | | -0.32 | |
| 0200 | LINZ I 34 I | 2.01 | | -0.32 | |
| | normality | not OK | | | |
| | n | 40 | | | |
| | outliers | 6 | | | |
| | mean (n) st.dev. (n) | 2.0952 0.06265 | | | |
| | R(calc.) | 0.06265 | | | |
| | st.dev.(D2163:14e1) | 0.1734 | | | |
| | R(D2163:14e1) | 0.2218 | | | Compare R(EN27941:93(liq)) = 0.3862 |
| | | | | | |

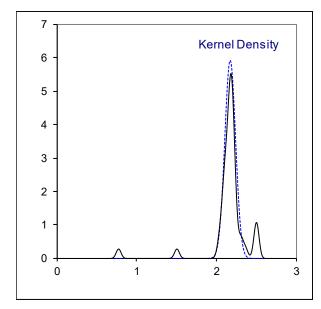




Determination of n-Butane on sample #19215; results in %mol/mol

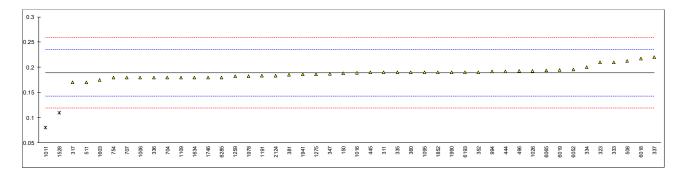
| lab | method | value | mark | z(targ) | remarks |
|--------------|---------------------|----------------|-----------|---------------|-------------------------------------|
| 150 | D2163 | 2.085 | | -1.32 | |
| 171 | -: | | | | |
| 311 | D2163 | 2.20 | | 0.33 | |
| 317 | D2163 | 2.24 | | 0.90 | |
| 323 | D2163 | 2.37 | | 2.77 | |
| 333 | D2163 | 2.51 | R(0.01) | 4.77 | |
| 334 | D2163 | 2.49 | R(0.01) | 4.49 | |
| 335 | D2163 | 2.10 | | -1.11 | |
| 336 337 | EN27941 D2163 | 2.11 2.51 | R(0.01) | -0.96 4.77 | |
| 347 | D2163 | 2.171 | 13(0.01) | -0.09 | |
| 352 | EN27941 | 2.2489 | | 1.03 | |
| 360 | EN27941 | 2.31 | | 1.91 | |
| 381 | EN27941 | 2.159 | | -0.26 | |
| 444 | IP405 | 2.229 | | 0.74 | |
| 445 | D2163 | 2.14 | | -0.53 | |
| 496 | D2163 | 2.229 | | 0.74 | |
| 508 | D2163 | 2.514374 | R(0.01) | 4.84 | factors and d 4.05 |
| 511 | D2163 | 2.22 | С | 0.61 | first reported: 1.85 |
| 529 704 | D2163 | 2.184 | | 0.10 | |
| 704 | D2163 | 2.168 | | -0.13 | |
| 754 | D2163 | 2.185 | | 0.11 | |
| 868 | -: | | | | |
| 994 | D2163 | 2.1839 | | 0.10 | |
| 1006 | D2163 | 2.126 | | -0.73 | |
| 1011 | ISO7941 | 0.78 | C,R(0.01) | -20.03 | first reported: 0.8 |
| 1012 | 10.0=0.44 | | | | |
| 1016 | ISO7941 | 2.192 | | 0.21 | |
| 1026 1095 | ISO7941 ISO7941 | 2.3122 2.19 | | 1.94 0.18 | |
| 11093 | IP405 | 2.19 | | -0.53 | |
| 1191 | IP473 | 2.132 | | -0.65 | |
| 1197 | 0 | | | | |
| 1198 | | | | | |
| 1259 | EN27941 | 2.054 | | -1.77 | |
| 1275 | EN27941 | 2.1567 | | -0.29 | |
| 1528 | EN27941 | 1.51 | R(0.01) | -9.57 | |
| 1603 | In house | 2.1062 | | -1.02 | |
| 1634 1720 | ISO7941 | 2.20 | | 0.33 | |
| 1746 | D2163 | 2.21 | | 0.47 | |
| 1786 | D2100 | | | | |
| 1852 | DIN51619 | 2.20 | | 0.33 | |
| 1941 | DIN51619 | 2.179 | | 0.03 | |
| 1978 | D2163 | 2.0389 | | -1.98 | |
| 1990 | IP473 | 2.201 | | 0.34 | |
| 2124 | D2163 | 2.087 | | -1.29 | |
| 6018 6019 | ISO7941 | 2.144 2.199 | | -0.47 0.31 | |
| 6052 | ISO7941 D2163 | 2.199 | | -1.06 | |
| 6065 | D2163 | 2.1032 | | -0.09 | |
| 6193 | D2163 | 2.23 | | 0.76 | |
| 6201 | | | | | |
| 6215 | | | | | |
| 6285 | EN27941 | 2.18 | | 0.04 | |
| | | | | | |
| | normality | suspect | | | |
| | n outliers | 40 6 | | | |
| | mean (n) | 0 2.1771 | | | |
| | st.dev. (n) | 0.06750 | | | |
| | R(calc.) | 0.1890 | | | |
| | st.dev.(D2163:14e1) | 0.06974 | | | |
| | R(D2163:14e1) | 0.1953 | | | Compare R(EN27941:93(liq)) = 0.3862 |
| | | | | | |

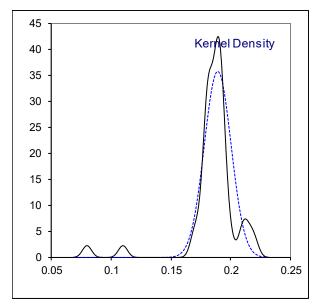




Determination of 1-Butene on sample #19215; results in %mol/mol

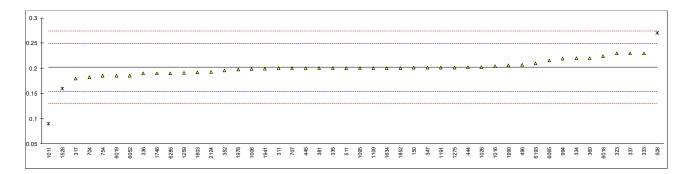
| lab | method | value | mark | z(targ) | remarks |
|--------------|---------------------|----------------|-----------|----------------|-------------------------------------|
| 150 | D2163 | 0.188 | | -0.05 | |
| 171 | -: | | | | |
| 311 | D2163 | 0.19 | | 0.04 | |
| 317 | D2163 | 0.17 | | -0.82 | |
| 323 | D2163 | 0.21 | | 0.90 | |
| 333 | D2163 | 0.21 | | 0.90 | |
| 334 | D2163 | 0.20 | | 0.47 | |
| 335 | D2163 | 0.19 | | 0.04 | |
| 336 337 | EN27941 D2163 | 0.18 | | -0.39 | |
| 347 | D2163 | 0.22 0.187 | | 1.33 -0.09 | |
| 352 | EN27941 | 0.1902 | | 0.05 | |
| 360 | EN27941 | 0.19 | | 0.04 | |
| 381 | EN27941 | 0.185 | | -0.18 | |
| 444 | IP405 | 0.192 | | 0.12 | |
| 445 | D2163 | 0.19 | | 0.04 | |
| 496 | D2163 | 0.193 | | 0.17 | |
| 508 | D2163 | 0.212737 | | 1.02 | |
| 511 520 | D2163 | 0.17 | | -0.82 | |
| 529 704 | D2163 | 0.180 | | -0.39 | |
| 704 | D2163 | 0.180 | | -0.39 | |
| 754 | D2163 | 0.18 | | -0.39 | |
| 868 | | | | | |
| 994 | D2163 | 0.1917 | | 0.11 | |
| 1006 | D2163 | 0.180 | | -0.39 | |
| 1011 | ISO7941 | 0.08 | C,R(0.01) | -4.70 | first reported: 0.1 |
| 1012 | 10.07044 | | | | |
| 1016 | ISO7941 | 0.189 | | 0.00 | |
| 1026 1095 | ISO7941 ISO7941 | 0.1932 0.19 | | 0.18 0.04 | |
| 1109 | IP405 | 0.18 | | -0.39 | |
| 1191 | IP473 | 0.183 | | -0.26 | |
| 1197 | | | | | |
| 1198 | | | | | |
| 1259 | EN27941 | 0.182 | | -0.31 | |
| 1275 | EN27941 | 0.18645 | 5(0.04) | -0.11 | |
| 1528 | EN27941 | 0.11 | R(0.01) | -3.41 | |
| 1603 1634 | In house ISO7941 | 0.1744 0.18 | | -0.63 -0.39 | |
| 1720 | 1307941 | 0.10 | | -0.59 | |
| 1746 | D2163 | 0.18 | | -0.39 | |
| 1786 | | | | | |
| 1852 | DIN51619 | 0.19 | | 0.04 | |
| 1941 | DIN51619 | 0.186 | | -0.13 | |
| 1978 | D2163 | 0.1822 | | -0.30 | |
| 1990 | IP473 | 0.190 | | 0.04 | |
| 2124 6018 | D2163 ISO7941 | 0.183 0.217 | | -0.26 1.20 | |
| 6019 | ISO7941 | 0.217 | | 0.25 | |
| 6052 | D2163 | 0.1958 | | 0.29 | |
| 6065 | D2163 | 0.1942 | | 0.22 | |
| 6193 | D2163 | 0.19 | | 0.04 | |
| 6201 | | | | | |
| 6215 | | | | | |
| 6285 | EN27941 | 0.18 | | -0.39 | |
| | normality | not OK | | | |
| | n | 44 | | | |
| | outliers | 2 | | | |
| | mean (n) | 0.1891 | | | |
| | st.dev. (n) | 0.01115 | | | |
| | R(calc.) | 0.0312 | | | |
| | st.dev.(D2163:14e1) | 0.02323 | | | O D/FN07044 00//:::// 0.4000 |
| | R(D2163:14e1) | 0.0650 | | | Compare R(EN27941:93(liq)) = 0.1600 |

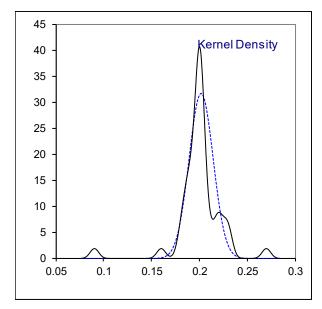




Determination of iso-Butene on sample #19215; results in %mol/mol

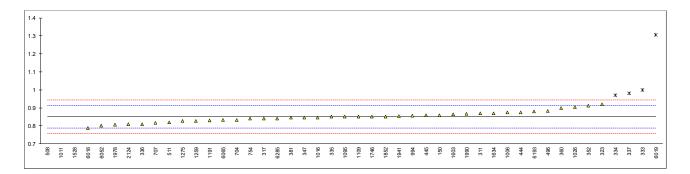
| lab | method | value | mark | z(targ) | remarks |
|--------------|----------------------|-----------------|-----------|----------------|---|
| 150 | D2163 | 0.201 | | -0.03 | |
| 171 | D0.400 | | | | |
| 311 | D2163 | 0.20 | | -0.08 | |
| 317 323 | D2163 D2163 | 0.18 0.23 | | -0.91 1.18 | |
| 323 333 | D2163 D2163 | 0.23 | | 1.18 | |
| 334 | D2163 | 0.22 | | 0.76 | |
| 335 | D2163 | 0.20 | | -0.08 | |
| 336 | EN27941 | 0.19 | | -0.49 | |
| 337 | D2163 | 0.23 | | 1.18 | |
| 347 | D2163 | 0.201 | | -0.03 | |
| 352 | EN27941 | 0.1956 | | -0.26 | |
| 360 381 | EN27941 | 0.22 | | 0.76 | |
| 444 | EN27941 IP405 | 0.2 0.202 | | -0.08 0.01 | |
| 445 | D2163 | 0.202 | | -0.08 | |
| 496 | D2163 | 0.207 | | 0.22 | |
| 508 | D2163 | 0.270123 | R(0.01) | 2.86 | |
| 511 | D2163 | 0.20 | С | -0.08 | first reported: 0.25 |
| 529 | D0400 | 0.400 | | | |
| 704 707 | D2163 D2163 | 0.182 | | -0.83 | |
| 757 754 | D2163 D2163 | 0.200 0.185 | | -0.08 -0.70 | |
| 868 | D2100 | | | -0.70 | |
| 994 | D2163 | 0.2194 | | 0.74 | |
| 1006 | D2163 | 0.198 | | -0.16 | |
| 1011 | ISO7941 | 0.09 | C,R(0.01) | -4.68 | first reported: 0.1 |
| 1012 | 10.0=0.44 | | | | |
| 1016 | ISO7941 | 0.204 | | 0.09 | |
| 1026 1095 | ISO7941 ISO7941 | 0.2023 0.20 | | 0.02 -0.08 | |
| 1109 | IP405 | 0.20 | | -0.08 | |
| 1191 | IP473 | 0.201 | | -0.03 | |
| 1197 | | | | | |
| 1198 | =110=0.44 | | | | |
| 1259 | EN27941 | 0.191 | | -0.45 | |
| 1275 1528 | EN27941 EN27941 | 0.20155 0.16 | ex | -0.01 -1.75 | test result excluded, see paragraph 4.1 |
| 1603 | In house | 0.1917 | CX | -0.42 | test result excluded, see paragraph 4.1 |
| 1634 | ISO7941 | 0.20 | | -0.08 | |
| 1720 | | | | | |
| 1746 | D2163 | 0.19 | | -0.49 | |
| 1786 | DINEACAO | 0.00 | | | |
| 1852 1941 | DIN51619 DIN51619 | 0.20 0.199 | | -0.08 -0.12 | |
| 1941 | D1N31019 D2163 | 0.199 | | -0.12 -0.16 | |
| 1990 | IP473 | 0.206 | | 0.17 | |
| 2124 | D2163 | 0.193 | | -0.37 | |
| 6018 | ISO7941 | 0.224 | | 0.93 | |
| 6019 | ISO7941 | 0.185 | | -0.70 | |
| 6052 | D2163 | 0.1855 | | -0.68 | |
| 6065 6193 | D2163 D2163 | 0.2153 0.21 | | 0.56 0.34 | |
| 6201 | DZ 100 | 0.21 | | 0.34 | |
| 6215 | | | | | |
| 6285 | EN27941 | 0.19 | | -0.49 | |
| | | 014 | | | |
| | normality | OK | | | |
| | n outliers | 43 2 (+1ex) | | | |
| | mean (n) | 0.2018 | | | |
| | st.dev. (n) | 0.01260 | | | |
| | R(calc.) | 0.0353 | | | |
| | st.dev.(D2163:14e1) | 0.02392 | | | |
| | R(D2163:14e1) | 0.0667 | | | Compare R(EN27941:93(liq)) = 0.1600 |

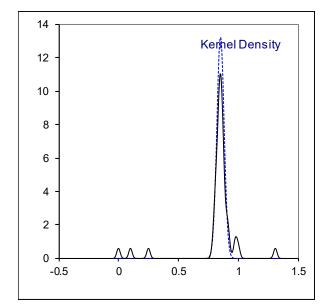




Determination of n-Pentane on sample #19215; results in %mol/mol

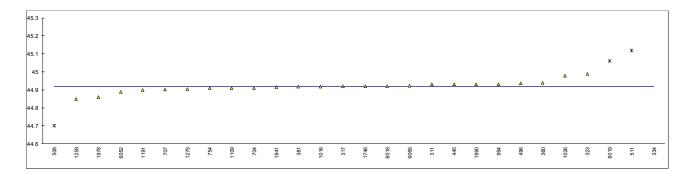
| lab | method | value | mark | z(targ) | remarks |
|--------------|-------------------------|-------------------|-----------|----------------|-------------------------------------|
| 150 | D2163 | 0.860 | | 0.31 | |
| 171 | | | | | |
| 311 | D2163 | 0.87 | | 0.63 | |
| 317 323 | D2163 D2163 | 0.84 0.92 | | -0.33 2.24 | |
| 333 | D2163 | 1.00 | R(0.05) | 4.81 | |
| 334 | D2163 | 0.97 | R(0.05) | 3.84 | |
| 335 | D2163 | 0.85 | , , | -0.01 | |
| 336 | EN27941 | 0.81 | D(0.05) | -1.30 | |
| 337 347 | D2163 D2163 | 0.98 0.847 | R(0.05) | 4.17 -0.11 | |
| 352 | EN27941 | 0.047 | | 1.96 | |
| 360 | EN27941 | 0.90 | | 1.60 | |
| 381 | EN27941 | 0.847 | | -0.11 | |
| 444 | IP405 | 0.874 | | 0.76 | |
| 445 496 | D2163 D2163 | 0.86 0.882 | | 0.31 1.02 | |
| 508 | D2163 | 0.0000 | R(0.01) | -27.32 | |
| 511 | D2163 | 0.82 | (, | -0.97 | |
| 529 | | | | | |
| 704 | D2163 | 0.832 | | -0.59 | |
| 707 754 | D2163 D2163 | 0.816 0.84 | | -1.10 -0.33 | |
| 868 | D2100 | | | | |
| 994 | D2163 | 0.8569 | | 0.21 | |
| 1006 | D2163 | 0.874 | / | 0.76 | |
| 1011 | ISO7941 | 0.10 | C,R(0.01) | -24.10 | first reported: 0.1 |
| 1012 1016 | ISO7941 | 0.847 | | -0.11 | |
| 1026 | ISO7941 | 0.9044 | | 1.74 | |
| 1095 | ISO7941 | 0.85 | | -0.01 | |
| 1109 | IP405 | 0.85 | | -0.01 | |
| 1191 1197 | IP473 | 0.831 | | -0.62 | |
| 1198 | | | | | |
| 1259 | EN27941 | 0.828 | | -0.72 | |
| 1275 | EN27941 | 0.82745 | | -0.73 | |
| 1528 | EN27941 | 0.25 | R(0.01) | -19.29 | |
| 1603 1634 | In house ISO7941 | 0.8654 0.87 | | 0.48 0.63 | |
| 1720 | 1007941 | | | | |
| 1746 | D2163 | 0.85 | | -0.01 | |
| 1786 | | | | | |
| 1852 | DIN51619 | 0.85 | | -0.01 | |
| 1941 1978 | DIN51619 D2163 | 0.853 0.8069 | | 0.09 -1.40 | |
| 1990 | IP473 | 0.868 | | 0.57 | |
| 2124 | D2163 | 0.809 | | -1.33 | |
| 6018 | ISO7941 | 0.789 | | -1.97 | |
| 6019 | ISO7941 | 1.307 | R(0.01) | 14.67 | |
| 6052 6065 | D2163 D2163 | 0.8016 0.8318 | | -1.57 -0.60 | |
| 6193 | D2163 | 0.88 | | 0.95 | |
| 6201 | | | | | |
| 6215 | | | | | |
| 6285 | EN27941 | 0.84 | | -0.33 | |
| | normality | OK | | | |
| | n | 39 | | | |
| | outliers | 7 | | | |
| | mean (n) | 0.8503 | | | |
| | st.dev. (n) R(calc.) | 0.03008 0.0842 | | | |
| | st.dev.(D2163:14e1) | 0.03113 | | | |
| | R(D2163:14e1) | 0.0872 | | | Compare R(EN27941:93(liq)) = 0.3111 |

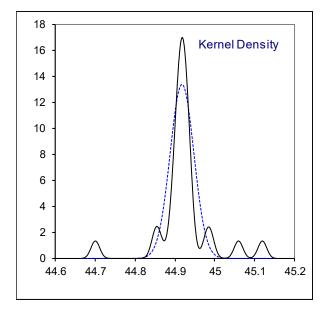




Determination of Molar Mass on sample #19215; results in g/mol

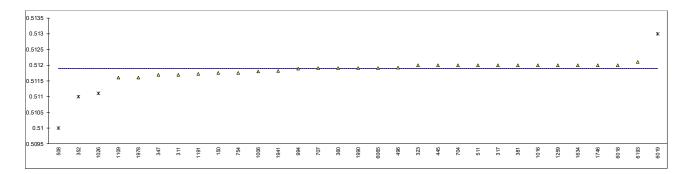
| lab | method | value | mark | z(targ) | remarks |
|--------------|----------------|--------------------|-----------|---------|--|
| 150 | | | | | |
| 171 | | | | | |
| 311 | INH-407 | 44.93 | | | |
| 317 | inh-001 | 44.92 | | | |
| 323 | D2598 | 44.99 | | | |
| 333 | | | _ | | |
| 334 | ISO8973 | 512.8 | ex,E | | test result excluded, see paragr. 4.1, calc. error, iis calc.: 45.05 |
| 335 | | | | | |
| 336 337 | | | | | |
| 347 | | | | | |
| 352 | | | | | |
| 360 | ISO8973 | 44.94 | | | |
| 381 | ISO8973 | 44.9167 | | | |
| 444 | | | | | |
| 445 | D2163 | 44.930 | | | |
| 496 | D2163 | 44.937 | | | |
| 508 | D2598 | 44.70 | ex | | test result excluded, see paragraph 4.1 |
| 511 | D2598 | 45.12 | C,R(0.01) | | first reported: 44.55 |
| 529 | D0404 | 44.0400 | | | |
| 704 707 | D2421 D2421 | 44.9106 44.9016 | | | |
| 707 754 | D2421 D2421 | 44.9016 | | | |
| 868 | JETE I | | | | |
| 994 | D2163 | 44.9304 | | | |
| 1006 | 22.00 | | | | |
| 1011 | | | | | |
| 1012 | | | | | |
| 1016 | EN27941 | 44.9167 | | | |
| 1026 | ISO8973 | 44.98 | | | |
| 1095 | 10.00070 | | | | |
| 1109 | ISO8973 | 44.909 | | | |
| 1191 1197 | ISO6976 | 44.899 | | | |
| 1198 | | | | | |
| 1259 | ISO8973 | 44.85 | | | |
| 1275 | EN589 | 44.904 | | | |
| 1528 | | | | | |
| 1603 | | | | | |
| 1634 | | | | | |
| 1720 | | | | | |
| 1746 | D3588 | 44.92 | | | |
| 1786 | | | | | |
| 1852 | D2424 | 44.0452 | | | |
| 1941 1978 | D2421 D2598 | 44.9153 44.8594 | | | |
| 1976 | D2598 | 44.6594 44.93 | | | |
| 2124 | 22000 | | | | |
| 6018 | ISO8973 | 44.92 | | | |
| 6019 | ISO8973 | 45.06 | R(0.01) | | |
| 6052 | D3588 | 44.89 | C | | first reported: 44.38 |
| 6065 | D2598 | 44.922 | | | |
| 6193 | | | | | |
| 6201 | | | | | |
| 6215 | | | | | |
| 6285 | | | | | |
| | | | | | Calc. by iis from ALL rep. comp. results (acc. to D2421:18): |
| | normality | not OK | | | suspect |
| | n | 24 | | | 38 |
| | outliers | 2 (+2ex) | | | 2 (+6ex) |
| | mean (n) | 44.918 | | | 44.914 |
| | st.dev. (n) | 0.0298 | | | 0.0257 |
| | R(calc.) | 0.083 | | | 0.072 |
| | compare | | | | |
| | R(iis18S03P) | 0.098 | | | 0.173 |
| | | | | | |

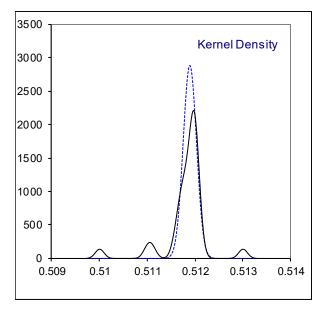




Determination of Relative Density at 60/60°F on sample #19215; unitless results

| lab | method | value | mark | z(targ) | remarks |
|--------------|----------------|------------------|-----------|---------|---|
| 150 | D2598 | 0.51175 | | | |
| 171 | | | | | |
| 311 | INH-407 | 0.5117 | | | |
| 317 | D2598 | 0.512 | | | |
| 323 | D2598 | 0.512 | | | |
| 333 | | | | | |
| 334 | | | | | |
| 335 | | | | | |
| 336 | | | | | |
| 337 | | | | | |
| 347 | D2598 | 0.5117 | | | |
| 352 | ISO8973 | 0.511 | R(0.01),E | | calculation error, iis calculated: 0.5120 |
| 360 | D2598 | 0.5119 | | | |
| 381 | D2598 | 0.512 | | | |
| 444 | ID422 | 0.5400 | | | |
| 445 496 | IP432 | 0.5120 | | | |
| 508 | D2598 D2598 | 0.51192 0.510 | ex, E | | test result excluded, see paragr. 4.1, calc. error, iis calc.: 0.5111 |
| 511 | D2598 | 0.510 | C C | | first reported: 0.5092 |
| 529 | D2000 | | O | | mat reported: 0.3032 |
| 704 | D2598 | 0.5120 | | | |
| 707 | D2598 | 0.5119 | | | |
| 754 | D2598 | 0.51175 | | | |
| 868 | | | | | |
| 994 | D2598 | 0.51189 | | | |
| 1006 | D2598 | 0.5118 | | | |
| 1011 | | | W | | first reported: 507.7 |
| 1012 | | | | | |
| 1016 | ISO8973 | 0.5120 | | | |
| 1026 | ISO8973 | 0.5111 | R(0.01),E | | calculation error, iis calculated: 0.5121 |
| 1095 | | | | | |
| 1109 | D2598 | 0.5116 | | | |
| 1191 | D2598 | 0.511723 | С | | first reported: 511.9 |
| 1197 | | | | | |
| 1198 1259 | ISO8973 | 0.512 | | | |
| 1275 | 1300973 | 0.512 | | | |
| 1528 | | | | | |
| 1603 | | | | | |
| 1634 | ISO8973 | 0.512 | С | | first reported: 512 |
| 1720 | | | | | |
| 1746 | D2598 | 0.512 | | | |
| 1786 | | | | | |
| 1852 | | | | | |
| 1941 | D2598 | 0.51181 | | | |
| 1978 | D2598 | 0.5116 | | | |
| 1990 | D2598 | 0.5119 | | | |
| 2124 | 10.000=0 | | | | |
| 6018 | ISO8973 | 0.512 | D(0.04) | | |
| 6019 | ISO8973 | 0.513 | R(0.01) | | |
| 6052 6065 | D2598 | 0.5119 | | | |
| 6193 | ISO8973 | 0.5119 | | | |
| 6201 | 1000973 | 0.5121 | | | |
| 6215 | | | | | |
| 6285 | | | | | |
| | | | | | |
| | | | | | Calc. by iis from ALL rep. composition results (acc. to D2598:16) |
| | normality | OK | | | not OK |
| | n | 27 | | | 39 |
| | outliers | 3 (+1ex) | | | 1 (+6ex) |
| | mean (n) | 0.51189 | | | 0.51180 |
| | st.dev. (n) | 0.000139 | | | 0.000150 |
| | R(calc.) | 0.00039 | | | 0.00042 |
| | compare | 0.00129 | | | 0.00081 |
| | R(iis18S03P) | 0.00129 | | | 0.0000 i |

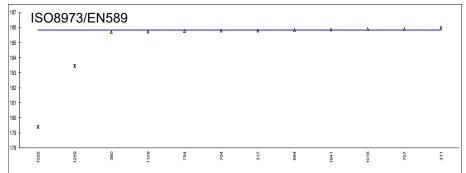


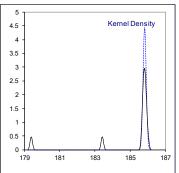


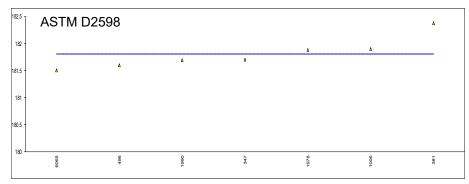
Determination of Absolute Vapor Pressure at 100°F on sample #19215; results in psi

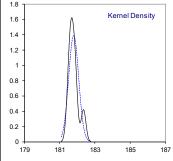
| lab | method | ISO8973 | mark | z(targ) | D2598 | mark | z(targ) | remarks |
|------|---------|----------|-----------|---------|----------|------|---------|--------------------------------------|
| 150 | | | | | | | | |
| 171 | | | | | | | | |
| 311 | ISO8973 | 186 | | | | | | |
| 317 | ISO8973 | 185.8 | | | | | | |
| 323 | | | | | | | | |
| 333 | | | | | | | | |
| 334 | | | | | | | | |
| 335 | | | | | | | | |
| 336 | | | | | | | | |
| 337 | | | | | | | | |
| 347 | D2598 | | | | 181.7 | | | |
| 352 | | | | | | | | |
| 360 | ISO8973 | 185.7 | | | | | | |
| 381 | D2598 | | | | 182.37 | | | |
| 444 | | | | | | | | |
| 445 | | | | | | | | |
| 496 | D2598 | | | | 181.60 | | | |
| 508 | | | | | | | | |
| 511 | | | | | | | | |
| 529 | | | | | | | | |
| 704 | ISO8973 | 185.8 | | | | | | |
| 707 | ISO8973 | 185.9 | | | | | | |
| 754 | ISO8973 | 185.75 | | | | | | |
| 868 | | | | | | | | |
| 994 | ISO8973 | 185.84 | | | | | | |
| 1006 | D2598 | | | | 181.9 | | | |
| 1011 | | | | | | | | |
| 1012 | | | | | | | | |
| 1016 | EN589 | 185.8852 | | | | | | |
| 1026 | ISO8973 | 179.41 | G(0.01),E | | | | | calculation error, iis calc.: 185.31 |
| 1095 | | | , , | | | | | |
| 1109 | ISO8973 | 185.73 | | | | | | |
| 1191 | | | | | | | | |
| 1197 | | | | | | | | |
| 1198 | | | | | | | | |
| 1259 | ISO8973 | 183.43 | G(0.01),E | | | | | calculation error, iis calc.: 186.65 |
| 1275 | | | | | | | | |
| 1528 | | | | | | | | |
| 1603 | | | | | | | | |
| 1634 | | | | | | | | |
| 1720 | | | | | | | | |
| 1746 | | | | | | | | |
| 1786 | | | | | | | | |
| 1852 | | | | | | | | |
| 1941 | ISO8973 | 185.859 | | | | | | |
| 1978 | D2598 | | | | 181.8773 | | | |
| 1990 | D2598 | | | | 181.696 | | | |
| 2124 | | | | | | | | |
| 6018 | | | | | | | | |
| 6019 | | | | | | | | |
| 6052 | | | | | | | | |
| 6065 | D2598 | | | | 181.5 | | | |
| 6193 | | | | | | | | |
| 6201 | | | | | | | | |
| 6215 | | | | | | | | |
| 6285 | | | | | | | | |
| | | | | | | | | |

| | ISO8973/IP432: | D2598: |
|--------------|------------------------------|------------------------------|
| normality | OK | unknown |
| n | 10 | 7 |
| outliers | 2 | 0 |
| mean (n) | 185.826 | 181.806 |
| st.dev. (n) | 0.0899 | 0.2862 |
| R(calc.) | 0.252 | 0.801 |
| compare | | |
| R(iis18S03P) | 2.785 | 2.239 |
| | iis calc. based on ALL | iis calc. based on ALL |
| | reported composition results | reported composition results |
| normality | not OK | not OK |
| n | 40 | 40 |
| outliers | 0 (+6ex) | 0 (+6ex) |
| mean (n) | 185.823 | 181.748 |
| st.dev. (n) | 0.3454 | 0.3444 |
| R(calc.) | 0.967 | 0.964 |
| compare | | |
| R(iis18S03P) | 0.872 | 1.007 |





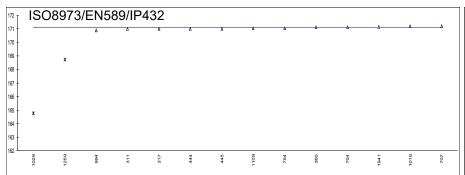


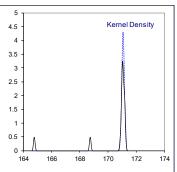


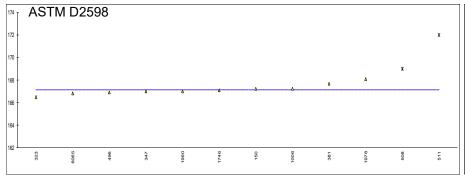
Determination of Relative Vapor Pressure at 100°F on sample #19215; results in psi

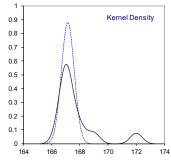
| lab | method | ISO8973 | mark | z(targ) | D2598 | mark | z(targ) | remarks |
|------|---------|--------------|-----------|---------|----------|------------|---------|--|
| 150 | D2598 | | | | 167.2 | | _(| |
| 171 | D2390 | | | | | | | |
| 311 | ISO8973 | 171 | | | | | | |
| | | | | | | | | |
| 317 | ISO8973 | 171 | | | 400.40 | | | |
| 323 | D2598 | | | | 166.48 | | | |
| 333 | | | | | | | | |
| 334 | | | | | | | | |
| 335 | | | | | | | | |
| 336 | | | | | | | | |
| 337 | | | | | | | | |
| 347 | D2598 | | | | 167 | | | |
| 352 | | | | | | | | |
| 360 | ISO8973 | 171.1 | | | | | | |
| 381 | D2598 | | | | 167.67 | | | |
| 444 | ISO8973 | 171 | | | | | | |
| 445 | IP432 | 171 | | | | | | |
| 496 | D2598 | | | | 166.91 | | | |
| 508 | D2598 | | | | 169 | ex, E | | excl., see paragr. 4.1, iis calc. 167.72 |
| 511 | D2598 | | | | 172 | G(0.01), E | | calculation error, iis calc. 166.93 |
| | D2596 | | | | | G(0.01), E | | Calculation error, ils calc. 100.93 |
| 529 | 1000070 | 474.4 | | | | | | |
| 704 | ISO8973 | 171.1 | | | | | | |
| 707 | ISO8973 | 171.2 | | | | | | |
| 754 | ISO8973 | 171.05 | | | | | | |
| 868 | | | | | | | | |
| 994 | ISO8973 | 170.89 | | | | | | |
| 1006 | D2598 | | | | 167.2 | | | |
| 1011 | | | | | | | | |
| 1012 | | | | | | | | |
| 1016 | EN589 | 171.1892 | | | | | | |
| 1026 | ISO8973 | 164.76 | G(0.01),E | | | | | calculation error, iis calc. 170.62 |
| 1095 | | | - (// | | | | | , |
| 1109 | ISO8973 | 171.04 | | | | | | |
| 1191 | | | | | | | | |
| 1197 | | | | | | | | |
| 1198 | | | | | | | | |
| 1259 | ISO8973 | 168.73 | G(0.01),E | | | | | calculation error, iis calc. 171.95 |
| 1275 | 1300913 | | G(0.01),L | | | | | Calculation end, ils calc. 17 1.95 |
| | | | | | | | | |
| 1528 | | | | | | | | |
| 1603 | | | | | | | | |
| 1634 | | | | | | | | |
| 1720 | | | | | | | | |
| 1746 | D2598 | | | | 167.1 | | | |
| 1786 | | | | | | | | |
| 1852 | | | | | | | | |
| 1941 | ISO8973 | 171.163 | | | | | | |
| 1978 | D2598 | | | | 168.0987 | | | |
| 1990 | D2598 | | | | 167 | | | |
| 2124 | | | | | | | | |
| 6018 | | | | | | | | |
| 6019 | | | | | | | | |
| 6052 | | | | | | | | |
| 6065 | D2598 | | | | 166.8 | | | |
| 6193 | | | | | | | | |
| 6201 | | | | | | | | |
| 6215 | | - | | | | | | |
| 6285 | | | | | | | | |
| 0200 | | - | | | | | | |

| | ISO8973/IP432: | D2598: |
|--------------|------------------------------|------------------------------|
| normality | OK | suspect |
| n | 12 | 10 |
| outliers | 2 | 1 (+1ex) |
| mean (n) | 171.061 | 167.146 |
| st.dev. (n) | 0.0924 | 0.4536 |
| R(calc.) | 0.259 | 1.270 |
| compare | | |
| R(iis18S03P) | 2.086 | 2.040 |
| | iis calc. based on ALL | iis calc. based on ALL |
| | reported composition results | reported composition results |
| normality | not OK | not OK |
| n | 40 | 40 |
| outliers | 0 (+6ex) | 0 (+6ex) |
| mean (n) | 171.127 | 167.052 |
| st.dev. (n) | 0.3454 | 0.3444 |
| R(calc.) | 0.967 | 0.964 |
| compare | | |
| R(iis18S03P) | 1.470 | 1.593 |



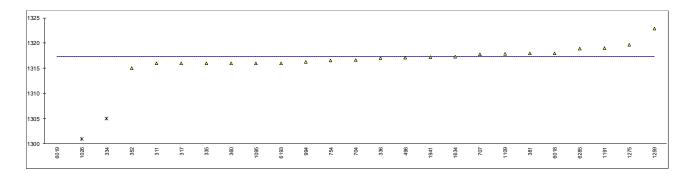


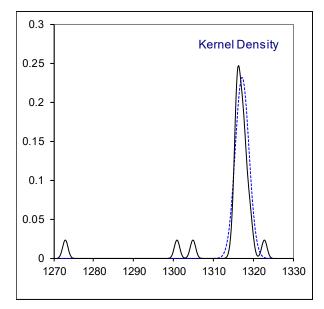




Determination of Absolute Vapor Pressure at 40°C on sample #19215; results in kPa

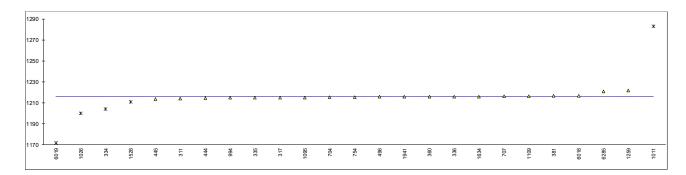
| lab | method | value | mark | z(targ) | remarks |
|--------------|---------------------|---------------|-----------|---------|---|
| 150 | | | | | |
| 171 | | | | | |
| 311 | ISO8973 | 1316 | | | |
| 317 | ISO8973 | 1316 | | | |
| 323 | | | | | |
| 333 | | | | | |
| 334 | ISO8973 | 1305 | ex | | test result excluded, see paragraph 4.1 |
| 335 | ISO8973 | 1316 | | | |
| 336 | ISO8973 | 1317 | | | |
| 337 | | | | | |
| 347 | 10,00070 | 4045 | | | |
| 352 | ISO8973 | 1315 | | | |
| 360 381 | ISO8973 ISO8973 | 1316 1318 | | | |
| 444 | 1300973 | | | | |
| 445 | | | | | |
| 496 | ISO8973 | 1317.16 | | | |
| 508 | 000.0 | | | | |
| 511 | | | | | |
| 529 | | | | | |
| 704 | ISO8973 | 1316.6 | | | |
| 707 | ISO8973 | 1317.8 | | | |
| 754 | ISO8973 | 1316.5 | | | |
| 868 | 10.000=0 | | | | |
| 994 | ISO8973 | 1316.25 | | | |
| 1006 | | | | | |
| 1011 1012 | | | | | |
| 1012 | | | | | |
| 1026 | ISO8973 | 1301 | R(0.01),E | | calculation error, iis calculated: 1313 |
| 1095 | ISO8973 | 1316 | (0.01),_ | | Salsalation office, no outourdiod. 1010 |
| 1109 | ISO8973 | 1317.84 | | | |
| 1191 | ISO8973 | 1319 | | | |
| 1197 | | | | | |
| 1198 | | | _ | | |
| 1259 | ISO8973 | 1322.91 | С | | first reported: 1299.20 |
| 1275 | EN589 | 1319.7 | | | |
| 1528 | | | | | |
| 1603 | ISO2073 | 1317.3 | | | |
| 1634 1720 | ISO8973 | 1317.3 | | | |
| 1746 | | | | | |
| 1786 | | | | | |
| 1852 | | | | | |
| 1941 | ISO8973 | 1317.25 | | | |
| 1978 | | | | | |
| 1990 | | | | | |
| 2124 | 10.000== | | | | |
| 6018 | ISO8973 | 1318 | D(0.04) = | | and and officer account the control of ACCO |
| 6019 | ISO8973 | 1273 | R(0.01),E | | calculation error, iis calculated: 1309 |
| 6052 | | | | | |
| 6065 6193 | ISO8973 | 1316 | | | |
| 6201 | 1000913 | 1310 | | | |
| 6215 | | | | | |
| 6285 | ISO8973 | 1318.9 | | | |
| | | | | | |
| | | | | | Calc. by iis from ALL rep. composition results: |
| | normality | not OK | | | not OK |
| | n | 22 | | | 40 |
| | outliers | 2 (+1ex) | | | 0 (+6ex) |
| | mean (n) | 1317.33 | | | 1316.98 |
| | st.dev. (n) | 1.718 4.81 | | | 2.462 6.89 |
| | R(calc.) compare | 4.81 | | | 0.08 |
| | R(iis18S03P) | 8.61 | | | 10.39 |
| | (110100001) | 3.51 | | | |

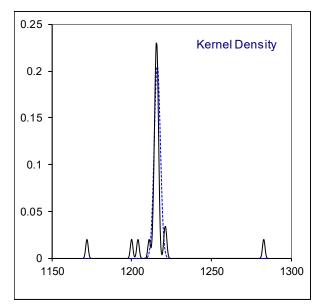




Determination of Relative Vapor Pressure at 40°C on sample #19215; results in kPa

| lab | method | value | mark | z(targ) | remarks |
|--------------|--------------|----------|------------|---------|---|
| 150 | | | | | |
| 171 | | | | | |
| 311 | ISO8973 | 1214 | | | |
| 317 | ISO8973 | 1215 | | | |
| 323 | | | | | |
| 333 | | | | | |
| 334 | ISO8973 | 1204 | ex | | test result excluded, see paragraph 4.1 |
| 335 | ISO8973 | 1215 | | | , 1 3 1 |
| 336 | ISO8973 | 1216 | | | |
| 337 | | | | | |
| 347 | | | | | |
| 352 | | | | | |
| 360 | ISO8973 | 1216 | | | |
| 381 | ISO8973 | 1217 | | | |
| 444 | ISO8973 | 1214.6 | | | |
| 445 | IP432 | 1213.7 | | | |
| 496 | ISO8973 | 1215.84 | | | |
| 508 | | | | | |
| 511 | | | | | |
| 529 | 10.000=0 | | | | |
| 704 | ISO8973 | 1215.3 | | | |
| 707 | ISO8973 | 1216.5 | | | |
| 754 | ISO8973 | 1215.5 | | | |
| 868 | 1000070 | 4044.05 | | | |
| 994 | ISO8973 | 1214.95 | | | |
| 1006 | 1000073 | 1202.0 | ٥٧/ | | test regult evaluded, one personne 4.4 |
| 1011 | ISO8973 | 1282.9 | ex | | test result excluded, see paragraph 4.1 |
| 1012 1016 | | | | | |
| 1016 | ISO8973 | 1200 | R(0.01),E | | calculation error, iis calculated: 1212.03 |
| 1020 | ISO8973 | 1215 | 11(0.01),∟ | | Calculation error, its calculated. 1212.00 |
| 11093 | ISO8973 | 1216.54 | | | |
| 1191 | 1000010 | | | | |
| 1197 | | | | | |
| 1198 | | | | | |
| 1259 | ISO8973 | 1221.58 | С | | first reported: 1197.88 |
| 1275 | | | | | , |
| 1528 | ISO8973 | 1211 | ex, E | | test result excluded, see paragr. 4.1, calc. error, iis calc.: 1232 |
| 1603 | | | • | | |
| 1634 | ISO8973 | 1216 | | | |
| 1720 | | | | | |
| 1746 | | | | | |
| 1786 | | | | | |
| 1852 | | | | | |
| 1941 | ISO8973 | 1215.92 | | | |
| 1978 | | | | | |
| 1990 | | | | | |
| 2124 | 10.00070 | 4047 | | | |
| 6018 | ISO8973 | 1217 | D(0.04) E | | coloulation array iia colo : 1007 |
| 6019 | ISO8973 | 1172 | R(0.01),E | | calculation error, iis calc.: 1207 |
| 6052 6065 | | | | | |
| 6193 | | | | | |
| 6201 | | | | | |
| 6215 | | | | | |
| 6285 | ISO8973 | 1220.7 | | | |
| 0200 | 1000373 | 1220.7 | | | |
| | | | | | Calc. bij iis from ALL rep. composition results: |
| | normality | not OK | | | not OK |
| | n | 20 | | | 40 |
| | outliers | 2 (+3ex) | | | 0 (+6ex) |
| | mean (n) | 1216.11 | | | 1215.66 |
| | st.dev. (n) | 1.942 | | | 2.462 |
| | R(calc.) | 5.44 | | | 6.89 |
| | compare | | | | |
| | R(iis18S03P) | 10.79 | | | 10.39 |
| | • | | | | |

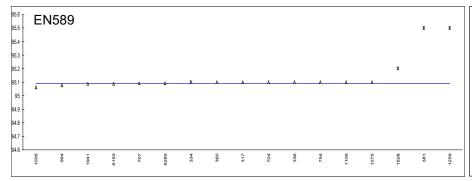


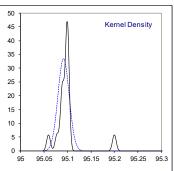


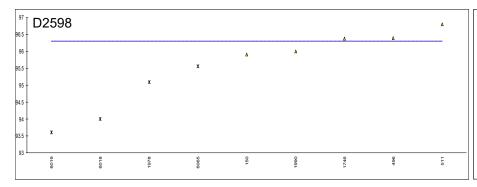
Determination of Motor Octane Number, MON on sample #19215;

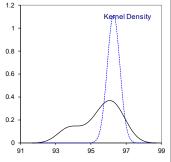
| lab | method | EN589 | mark | z(targ) | D2598 | mark | z(targ) | remarks |
|------------|--------------|------------|-------------|---------|---------|------------|---------|--------------------------------------|
| 150 | D2598 | | | | 95.9 | | | |
| 171 | | | | | | | | |
| 311 | | | | | | | | |
| 317 | EN589 | 95.1 | | | | | | |
| 323 | LINOUS | | | | | | | |
| | | | | | | | | |
| 333 | ENEGO. | 0E 1 | | | | | | test result evaluded ass person 4.4 |
| 334 | EN589 | 95.1 | ex | | | | | test result excluded, see paragr.4.1 |
| 335 336 | ENEGO | 95.1 | | | | | | |
| 337 | EN589 | | | | | | | |
| | | | | | | | | |
| 347 | | | | | | | | |
| 352 | | | | | | | | |
| 360 | EN589 | 95.1 | | | | | | |
| 381 | EN589 | 95.5 | DG(0.01) | | | | | |
| 444 | | | | | | | | |
| 445 | EN589 | | | | | | | |
| 496 | D2598 | | | | 96.391 | | | |
| 508 | D0500 | | | | | | | |
| 511 | D2598 | | | | 96.8 | | | |
| 529 | ENITOO | 05.40 | | | | | | |
| 704 | EN589 | 95.10 | | | | | | |
| 707 | EN589 | 95.09 | | | | | | |
| 754 868 | EN589 | 95.1 | | | | | | |
| 994 | EN589 | 95.078 | | | | | | |
| 1006 | LINJOS | 95.076 | | | | | | |
| | | | | | | | | |
| 1011 | | | | | | | | |
| 1012 | | | | | | | | |
| 1016 | | | | | | | | |
| 1026 | EN589 | 95.06 | | | | | | |
| 1095 | | | | | | | | |
| 1109 | EN589 | 95.1 | | | | | | |
| 1191 | | | | | | | | |
| 1197 | | | | | | | | |
| 1198 | | | | | | | | |
| 1259 | EN589 | 95.5 | DG(0.01) | | | | | |
| 1275 | EN589 | 95.1 | _ (() () | | | | | |
| 1528 | EN589 | 95.2 | ex | | | | | test result excluded, see paragr.4.1 |
| 1603 | | | | | | | | , 1 |
| 1634 | | | | | | | | |
| 1720 | | | | | | | | |
| 1746 | D2598 | | | | 96.37 | | | |
| 1786 | D2330 | | | | | | | |
| 1852 | | | | | | | | |
| 1941 | EN589 | 95.089 | | | | | | |
| 1978 | D2598 | | | | 95.0959 | ex,E | | calculation error, iis calc.: 96.45 |
| 1990 | Calculation | | | | 96 | CX,L | | calculation circl, ils calc 50.45 |
| 2124 | Calculation | | | | | | | |
| 6018 | D2598 | | | | 94.0 | ex,E | | calculation error, iis calc.: 96.44 |
| 6019 | D2598 | | | | 93.6 | ex,E | | calculation error, iis calc.: 96.21 |
| 6052 | 22000 | | | | | , - | | |
| 6065 | D2598 | | | | 95.55 | ex,E | | calculation error, iis calc.: 96.42 |
| 6193 | EN589 | 95.089 | | | | , | | , |
| 6201 | - | | | | | | | |
| 6215 | | | | | | | | |
| 6285 | EN589 | 95.09 | | | | | | |
| | - | | | | | | | |

| | EN589: | D2598: |
|--|--|---|
| normality | not OK | Unknown |
| n | 13 | 5 |
| outliers | 2 (+2ex) | 0 (+4ex) |
| mean (n) | 95.092 | 96.292 |
| st.dev. (n) | 0.0119 | (0.3581) |
| R(calc.) | 0.033 | (1.003) |
| compare | | |
| R(iis18S03P) | 0.445 | (1.229) |
| | iis calc. based on ALL | iis calc. based on ALL |
| | | |
| | reported composition results | reported composition results |
| normality | reported composition results not OK | reported composition results suspect |
| normality n | | |
| • | not OK | suspect |
| n | not OK 39 | suspect 39 |
| n outliers | not OK 39 1 (+6ex) | suspect 39 1 (+6ex) |
| n outliers mean (n) | not OK 39 1 (+6ex) 95.085 | suspect 39 1 (+6ex) 96.419 |
| n outliers mean (n) st.dev. (n) | not OK 39 1 (+6ex) 95.085 0.0178 | suspect 39 1 (+6ex) 96.419 0.0203 |
| n outliers mean (n) st.dev. (n) R(calc.) | not OK 39 1 (+6ex) 95.085 0.0178 | suspect 39 1 (+6ex) 96.419 0.0203 |



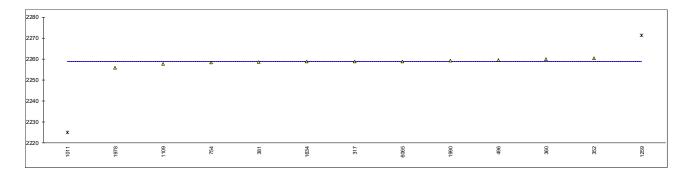


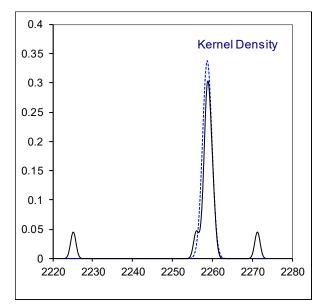




Determination of Ideal Gross Heating Value at 14.696 psia and 60°F on sample #19215; results in kJ/mol

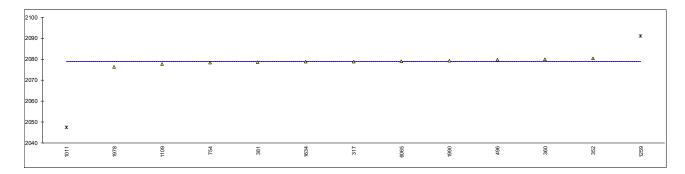
| resuits | s in KJ/Moi | | | | |
|---------|--------------|-----------|-------------|---------|--|
| lab | method | value | mark | z(targ) | remarks |
| | | | | | |
| 150 | | | | | |
| 171 | | | | | |
| 311 | | | | | |
| 317 | D3588 | 2258.8 | | | |
| 323 | | | | | |
| | | | | | |
| 333 | | | | | |
| 334 | | | | | |
| 335 | | | | | |
| 336 | | | | | |
| 337 | | | | | |
| | | | | | |
| 347 | | | | | |
| 352 | D3588 | 2260.364 | | | |
| 360 | D3588 | 2259.85 | | | |
| 381 | D3588 | 2258.53 | | | |
| 444 | 20000 | | | | |
| | | | | | |
| 445 | | | | | |
| 496 | D3588 | 2259.53 | | | |
| 508 | | | | | |
| 511 | | | | | |
| 529 | | | | | |
| | | | | | |
| 704 | | | | | |
| 707 | | | | | |
| 754 | D3588 | 2258.35 | С | | first reported: 2195.45 |
| 868 | | | | | |
| | | | | | |
| 994 | | | | | |
| 1006 | | | | | |
| 1011 | D3588 | 2225.06 | ex,C | | test result excluded, see paragraph 4.1, first reported: 12031 |
| 1012 | | | , - | | , 1 31 , 1 |
| | | | | | |
| 1016 | | | | | |
| 1026 | | | | | |
| 1095 | | | | | |
| 1109 | D3588 | 2257.67 | | | |
| 1191 | | | | | |
| | | | | | |
| 1197 | | | | | |
| 1198 | | | | | |
| 1259 | D3588 | 2271.31 | C,G(0.01),E | | first reported: 5029, calculation error, iis calculated: 2256 |
| 1275 | | | | | |
| 1528 | | | | | |
| | | | | | |
| 1603 | 50500 | | | | |
| 1634 | D3588 | 2258.74 | | | |
| 1720 | | | | | |
| 1746 | | | | | |
| 1786 | | | | | |
| | | | | | |
| 1852 | | | | | |
| 1941 | | | | | |
| 1978 | | 2255.9489 | | | |
| 1990 | Calculation | 2259.25 | | | |
| 2124 | | | | | |
| | | | | | |
| 6018 | | | | | |
| 6019 | | | | | |
| 6052 | | | | | |
| 6065 | D3588 | 2258.8 | | | |
| 6193 | 20000 | | | | |
| | | | | | |
| 6201 | | | | | |
| 6215 | | | | | |
| 6285 | | | | | |
| | | | | | |
| | | | | | Calc. by iis from ALL reported composition results: |
| | | | | | |
| | normality | not OK | | | suspect |
| | n | 11 | | | 38 |
| | outliers | 1 (+1ex) | | | 2 (+6ex) |
| | mean (n) | 2258.71 | | | 2258.45 |
| | | | | | |
| | st.dev. (n) | 1.178 | | | 1.196 |
| | R(calc.) | 3.30 | | | 3.35 |
| | comp | | | | |
| | R(iis18S03P) | 11.72 | | | 8.13 |
| | / | _ | | | |

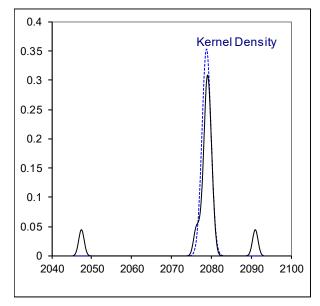




Determination of Ideal Net Heating Value at 14.696 psia and 60°F on sample #19215; results in kJ/mol

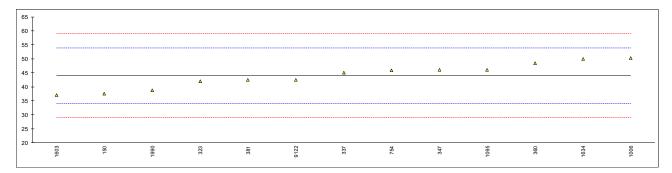
| | III KJ/IIIOI | | | | |
|------|--------------|-----------|-------------|--------|--|
| lab | method | value | mark z | (targ) | remarks |
| 150 | | | | | |
| 171 | | | | | |
| 311 | | | | | |
| | D2500 | | | | |
| 317 | D3588 | 2078.9 | | | |
| 323 | | | | | |
| 333 | | | | | |
| 334 | | | | | |
| 335 | | | | | |
| 336 | | | | | |
| 337 | | | | | |
| | | | | | |
| 347 | D0-00 | | | | |
| 352 | D3588 | 2080.340 | | | |
| 360 | D3588 | 2079.86 | | | |
| 381 | D3588 | 2078.65 | | | |
| 444 | | | | | |
| 445 | | | | | |
| 496 | D3588 | 2079.60 | | | |
| | D0000 | | | | |
| 508 | | | | | |
| 511 | | | | | |
| 529 | | | | | |
| 704 | | | | | |
| 707 | | | | | |
| 754 | D3588 | 2078.45 | С | | first reported: 2020.4 |
| 868 | 20000 | | Ü | | mot reported. 2020. I |
| | | | | | |
| 994 | | | | | |
| 1006 | | | | | |
| 1011 | D3588 | 2047.46 | ex,C | | test result excluded, see paragraph 4.1, first reported: 11065 |
| 1012 | | | | | |
| 1016 | | | | | |
| 1026 | | | | | |
| 1095 | | | | | |
| | D2500 | | | | |
| 1109 | D3588 | 2077.60 | | | |
| 1191 | | | | | |
| 1197 | | | | | |
| 1198 | | | | | |
| 1259 | D3588 | 2091.02 | C,G(0.01),E | | first reported: 46.28, calculation error, iis calculated: 2076 |
| 1275 | | | -,-(,, | | , |
| 1528 | | | | | |
| | | | | | |
| 1603 | D0500 | | | | |
| 1634 | D3588 | 2078.85 | | | |
| 1720 | | | | | |
| 1746 | | | | | |
| 1786 | | | | | |
| 1852 | | | | | |
| 1941 | | | | | |
| | | 2076 2220 | | | |
| 1978 | 0 1 1 " | 2076.2238 | | | |
| 1990 | Calculation | 2079.30 | | | |
| 2124 | | | | | |
| 6018 | | | | | |
| 6019 | | | | | |
| 6052 | | | | | |
| 6065 | D3588 | 2079.1 | | | |
| | D3300 | | | | |
| 6193 | | | | | |
| 6201 | | | | | |
| 6215 | | | | | |
| 6285 | | | | | |
| | | | | | |
| | | | | | Calc. by iis from ALL reported composition results: |
| | | | | | |
| | normality | suspect | | | suspect |
| | n | 11 | | | 38 |
| | outliers | 1 (+1ex) | | | 2 (+2ex) |
| | mean (n) | 2078.81 | | | 2078.58 |
| | st.dev. (n) | 1.127 | | | 1.120 |
| | R(calc.) | 3.16 | | | 3.14 |
| | compare | 5.15 | | | |
| | | 11.04 | | | 7.50 |
| | R(iis18S03P) | 11.04 | | | 7.59 |

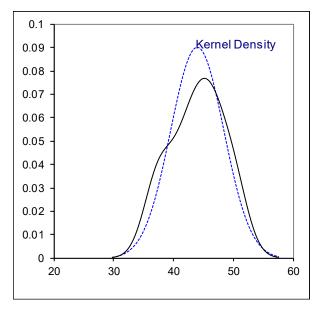




Determination of Sulfur, total on sample #19216; results in mg/kg

| lab | method | value | mark | z(targ) | remarks |
|------|-------------------|---------|------|---------|----------------------|
| 150 | D6667 | 37.5 | С | -1.30 | first reported: 9.2 |
| 171 | | | | | |
| 311 | | | | | |
| 323 | D6667 | 42.0 | | -0.40 | |
| 337 | D6667 | 45 | | 0.21 | |
| 347 | D6667 | 46 | | 0.41 | |
| 360 | D6667 | 48.4 | С | 0.89 | first reported: 20.8 |
| 381 | D6667 | 42.5 | | -0.30 | |
| 445 | | | | | |
| 754 | D6667 | 45.79 | | 0.36 | |
| 1006 | D6667 | 50.35 | | 1.28 | |
| 1011 | | | | | |
| 1095 | D6667 | 46 | | 0.41 | |
| 1603 | in house | 37.0 | _ | -1.40 | |
| 1634 | D6667 | 50 | С | 1.21 | first reported: 60 |
| 1990 | D6667 | 38.67 | | -1.07 | |
| 6018 | | | | | |
| 6019 | | | | | |
| 6201 | D0007 | 40.5 | | 0.20 | |
| 9122 | D6667 | 42.5 | | -0.30 | |
| | normality | OK | | | |
| | n | 13 | | | |
| | outliers | 0 | | | |
| | mean (n) | 43.9777 | | | |
| | st.dev. (n) | 4.43508 | | | |
| | R(calc.) | 12.4182 | | | |
| | st.dev.(D6667:14) | 4.97642 | | | |
| | R(D6667:14) | 13.9340 | | | |
| | | | | | |





APPENDIX 2

Number of participants per country

- 2 labs in AUSTRALIA
- 1 lab in AZERBAIJAN
- 1 lab in BELGIUM
- 1 lab in BULGARIA
- 1 lab in CHILE
- 1 lab in CHINA, People's Republic
- 1 lab in COLOMBIA
- 1 lab in CROATIA
- 1 lab in DENMARK
- 1 lab in FINLAND
- 5 labs in FRANCE
- 3 labs in GERMANY
- 4 labs in MALAYSIA
- 2 labs in MEXICO
- 5 labs in NETHERLANDS
- 1 lab in NIGER
- 1 lab in NIGERIA
- 1 lab in PANAMA
- 1 lab in PERU
- 1 lab in POLAND
- 6 labs in PORTUGAL
- 1 lab in ROMANIA
- 1 lab in RUSSIAN FEDERATION
- 2 labs in SERBIA
- 1 lab in SPAIN
- 1 lab in SUDAN
- 1 lab in TAIWAN
- 2 labs in UKRAINE
- 1 lab in UNITED ARAB EMIRATES
- 3 labs in UNITED KINGDOM
- 3 labs in UNITED STATES OF AMERICA

APPENDIX 3

Abbreviations

C = final result after checking of first reported suspect test result

 $\begin{array}{ll} D(0.01) &= \text{outlier in Dixon's outlier test} \\ D(0.05) &= \text{straggler in Dixon's outlier test} \\ G(0.01) &= \text{outlier in Grubbs' outlier test} \\ G(0.05) &= \text{straggler in Grubbs' outlier test} \\ DG(0.01) &= \text{outlier in Double Grubbs' outlier test} \\ DG(0.05) &= \text{straggler in Double Grubbs' outlier test} \\ \end{array}$

R(0.01) = outlier in Rosner's outlier test R(0.05) = straggler in Rosner's outlier test E = possibly an error in calculations

ex = test result excluded from the statistical evaluation

n.a. = not applicable
n.e. = not evaluated
fr. = first reported
SDS = safety data sheet

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