Results of Proficiency Test LPG Composition & sulfur October 2017

Organised by: Institute for Interlaboratory Studies Spijkenisse, the Netherlands

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### 1 INTRODUCTION

Since 2009, the Institute for Interlaboratory Studies organizes a proficiency test for the analysis of Liquefied Propane (composition only) every year. It was decided to continue the interlaboratory study for Liquefied Propane during the annual program 2017/2018. At the request of several participants, the Institute of Interlaboratory Studies decided to organise an interlaboratory study for Sulphur (total) in LPG in the 2017/2018 PT program. Because iis has limited gas-handling facilities in place to prepare gas samples a co-operation with EffecTech (Uttoxeter, United Kingdom) was set up for the Liquefied Propane PT (iis17S03P) and a co-operation with Praxair NV (Belgium) was set up for the Sulphur in LPG PT (iis17S03S). Both EffecTech and Praxair are fully equipped and have experience in the preparation of gas mixtures.

In the interlaboratory studies for Liquefied Propane (composition only) 52 laboratories in 28 different countries and for Sulphur (total) in LPG 10 laboratories in 6 different laboratories registered for participation. In this report, the results of the 2017 proficiency tests Liquefied Propane (composition only) and Sulphur (total) in LPG are presented and discussed. This report is also electronically available through the iis website www.iisnl.com.

## 2 SET UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, the Netherlands, was the organizer of this proficiency test (PT).

To optimise the costs for the participants for the Liquefied Propane PT (iis17S03P), it was decided to prepare one Liquefied Propane mixture for composition. The mixture was divided over a batch of 55 cylinders (1L cylinder with dip tube device). Each cylinder, filled with approx.. 200 grams of liquefied propane mixture, was labelled #17210 and uniquely coded.

For the Sulphur in LPG PT (iis17S03S) it was decided to use a batch of 12 cylinders, filled with approximately 1500 grams of LPG, each spiked with Dimethyl sulfide (DMS). Each cylinder (5L cylinder with dip tube device), was labelled #17211 and uniquely coded.

The limited cylinder sizes (1L and 5L) are chosen to optimise sample stability, cylinder costs, transport and handling costs.

The preparation and testing of the sample cylinders was subcontracted to ISO 17025 accredited laboratories. Participants were requested to report rounded and unrounded test results. The unrounded test results were preferably used for statistical evaluation.

# 2.1 QUALITY SYSTEM

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, has implemented a quality system based on ISO/IEC 17043:2010. This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentiality of participant's data. Feedback from the participants on the reported data is encouraged and customer's satisfaction is measured on a regular basis by sending out questionnaires.

EffecTech is accredited in conformance ISO/IEC17043:2010 by UKAS (no. 4719), ISO guide 35:2006 and ISO 17025:2005. Praxair is accredited in conformance with ISO 9001-2008, ISO 14001-2004, ISO 17025-No 159 Cal and ISO TS 16949.

## 2.2 PROTOCOL

The protocol followed in the organisation of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of March 2017 (iis-protocol, version 3.4). This protocol is electronically available through the iis website www.iisnl.com, from the FAQ page.

## 2.3 CONFIDENTIALITY STATEMENT

All data presented in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

### 2.4 SAMPLES

### LIQUEFIED PROPANE

In this proficiency test only one sample was used. One batch of 55 one litre cylinders with artificial Liquefied Propane mixture was prepared and tested for homogeneity by EffecTech (Uttoxeter, United Kingdom) in conformance with ISO guide 35:2006 and ISO 17025:2005 (job 17/1075, September 2017). Each cylinder was labelled #17210 and uniquely coded. Every cylinder in the batch was analysed using 5 replicate measurements. The within bottle and between bottle variations were then assessed in accordance with ISO Guide 35:2006 (Annex A.1). This procedure showed that the between bottle variations were all small compared to the uncertainties on the reference values on each component. Hence, a single reference value could be safely assigned to the entire batch of samples.

The repeatability values (r) were calculated per component by multiplication of the respective standard deviation by 2.8. Subsequently, the calculated repeatabilities were compared with 0.3 times the reproducibilities of the reference method in agreement with the procedure of ISO 13528, Annex B2 in the next table:

Component	r(observed) in %mol/mol	0.3 * R(D2163:14e1) in %mol/mol	
Ethane	0.002	0.034	
Propane 0.022		1.258	
Propylene	0.004	0.068	
Iso-Butane	0.007	0.066	
n-Butane	0.008	0.057	
1-Butene	0.002	0.018	
iso-Butylene	0.002	0.017	
n-Pentane	0.006	0.023	

Table 1: homogeneity test results of samples #17210

Each calculated repeatability is equal or less than 0.3 times the corresponding reproducibility of the reference method ASTM D2163:14e1. Therefore, homogeneity of the subsamples #17210 was assumed.

### <u>Sulphur</u>

In this proficiency test one batch of twelve 5L cylinders with artificial LPG mixture (Dimethylsulfide in Propane/n-Butaan) was prepared and tested for homogeneity by Praxair NV (Belgium) in conformance with ISO 9001-2008, ISO 14001-2004, ISO 17025-No 159 Cal and ISO TS 16949 in September 2017. Each cylinder was labelled #17211 and uniquely coded.

	Sulphur in mg/kg
Sample #17211-1	40.5
Sample #17211-2	39.8
Sample #17211-3	39.8
Sample #17211-4	39.7
Sample #17211-5	40.5
Sample #17211-6	39.9
Sample #17211-7	40.3
Sample #17211-8	39.9
Sample #17211-9	40.1
Sample #17211-10	39.7
Sample #17211-11	39.5
Sample #17211-12	40.4

Table 2: homogeneity test results of subsamples #17211

From the above test results, the repeatability was calculated and compared with 0.3 times the corresponding reproducibility of the reference test method and in agreement with the procedure of ISO 13528, Annex B2 in the next table:

	Sulphur in mg/kg
r (observed)	0.9
reference test method	ASTM D6667:14
0.3 * R (ref. test method)	3.8

Table 3: evaluation of the repeatability of subsamples #17211

The calculated repeatability is equal or less than 0.3 times the corresponding reproducibility of the reference test method ASTM D6667:14. Therefore, homogeneity of the subsamples #17211 was assumed.

Depending on their registration to each of the participating laboratories one 1L cylinder of Liquefied Propane labelled #17210 and/or one 5L cylinder of Sulphur in LPG labelled #17211 was sent on October 4, 2017. Per cylinder one SDS was added to the sample package.

### 2.5 STABILITY OF THE SAMPLES

The shelf life time of the prepared gas cylinders is sufficient for the period of the proficiency test.

### 2.6 ANALYSES

The participants were asked to determine on the Liquefied Propane sample # 17210 the composition: Ethane, Propane, Propene, n-Butane, iso-Butane, 1-Butene, iso-Butene, n-Pentane and to calculate several physical parameters from the composition: Molar Mass, Relative Density at 60F, Absolute and Relative Vapour pressure at 100F, Absolute and Relative Vapour pressure at 40°C, MON, Ideal Gross Heating Value and Ideal Net Heating Value at 14.696 psi and 60F.

On the LPG sample #17211 the total Sulphur content was requested.

It was explicitly requested to treat the samples as if they were routine samples and to report the test results using the indicated units on the report form and not to round the test results, but report as much significant figures as possible. It was also requested not to report 'less than' results, which are above the detection limit, because such test results cannot be used for meaningful statistical calculations.

To get comparable test results, a detailed report form and a letter of instructions are prepared. On the report form the reporting units are given as well as the reference test methods that will be used during the evaluation. The detailed report form and the letter of instructions are both made available on the data entry portal www.kpmd.co.uk/sgs-iis/. The participating laboratories are also requested to confirm the sample receipt on this data entry portal. The letter of instructions can also be downloaded from the iis website www.iisnl.com.

### 3 RESULTS

During five weeks after sample dispatch, the test results of the individual laboratories were gathered via the data entry portal www.kpmd.co.uk/sgs-iis/. The reported test results are tabulated per determination in appendix 1 of this report. The laboratories are presented by their code numbers.

Directly after the deadline, a reminder was sent to those laboratories that had not reported test results at that moment.

Shortly after the deadline, the available test results were screened for suspect data. A test result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the reported test results (no reanalysis). Additional or corrected test results are used for data analysis and original test results are placed under 'Remarks' in the test result tables in appendix 1. Test results that came in after the deadline were not taken into account in this screening for suspect data and thus these participants were not requested for checks.

## 3.1 STATISTICS

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of March 2017 (iis-protocol, version 3.4).

For the statistical evaluation the *unrounded* (when available) figures were used instead of the rounded test results. Test results reported as '<...' or '>...' were not used in the statistical evaluation.

First, the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test, a variant of the Kolmogorov-Smirnov test and by the calculation of skewness and kurtosis. Evaluation of the three normality indicators in combination with the visual evaluation of the graphic Kernel density plot, lead to judgement of the normality being either 'unknown', 'OK', 'suspect' or 'not OK'. After removal of outliers, this check was repeated. If a data set does not have a normal distribution, the results of the statistical evaluation should be used with due care.

According to ISO 5725 the original test results per determination were submitted to Dixon's, Grubbs' and/or Rosner's outlier tests. Outliers are marked by D(0.01) for the Dixon's test, by G(0.01) or DG(0.01) for the Grubbs' test and by R(0.01) for the Rosner's test. Stragglers are marked by D(0.05) for the Dixon's test, by G(0.05) or DG(0.05) for the Rosner's test. Both outliers and stragglers were not included in the calculations of averages and standard deviations.

For each assigned value the uncertainty was determined in accordance with ISO13528. Subsequently the calculated uncertainty was evaluated against the respective requirement based on the target reproducibility in accordance with ISO13528. When the uncertainty passed the evaluation, no remarks are made in the report. However, when the uncertainty failed the evaluation it is mentioned in the report and it will have consequences for the evaluation of the test results.

Finally, the reproducibilities were calculated from the standard deviations by multiplying them with a factor of 2.8.

## 3.2 GRAPHICS

In order to visualise the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported test results are plotted. The corresponding laboratory numbers are on the X-axis. The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected reference test method. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle.

Furthermore, Kernel Density Graphs were made. This is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. Also a normal Gauss curve was projected over the Kernel Density Graph for reference.

## 3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements, e.g. ASTM reproducibilities, the z-scores were calculated using a target standard deviation. This results in an evaluation independent of the variation in this interlaboratory study.

The target standard deviation was calculated from the literature reproducibility by division with 2.8. In case no literature reproducibility was available, other target values were used. In some cases, a reproducibility based on former iis proficiency tests could be used. When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate whether the reported test result is fit-for-use.

The z-scores were calculated according to:

 $z_{(target)} = (test result - average of PT) / target standard deviation$ 

The  $z_{(target)}$  scores are listed in the test result tables in appendix 1.

Absolute values for z<2 are very common and absolute values for z>3 are very rare. The usual interpretation of z-scores is as follows:

|z| < 1 good 1 < |z| < 2 satisfactory 2 < |z| < 3 questionable 3 < |z| unsatisfactory

## 4 EVALUATION

In this interlaboratory study, some problems were encountered with the dispatch of the samples. For the Liquefied Propane PT (iis17S03P), not all laboratories did report all test results requested and five participants didn't report any test result at all. In total 47 participants reported 536 numerical test results. Observed were 30 outlying test results, which is 5.6%. In proficiency studies outlier percentages of 3% - 7.5% are quite normal.

For the Sulphur in LPG PT (iis17S03S), two participants didn't report any result at all (one laboratory reported that DMS wasn't included in their calibration mixture). In total 8 participants reported 8 numerical test results. Observed was 1 outlying test result, which is 12.5%. In proficiency studies outlier percentages of 3% - 7.5% are quite normal.

Not all original data sets proved to have normal Gaussian distribution. These are referred to as "not OK" or "suspect". The statistical evaluation of these data sets should be used with due care, see also paragraph 3.1.

### 4.1 EVALUATION PER SAMPLE AND PER TEST

In this section, the reported test results are discussed per sample and per test. The test methods, which were used by the various laboratories, were taken into account for explaining the observed differences when possible and applicable. These test methods are also in the tables together with the original data. The abbreviations, used in these tables, are listed in appendix 3.

In the iis PT reports, ASTM methods are referred to with a number (e.g. D3588) and an added designation for the year that the method was adopted or revised (e.g. D3588:98). If applicable, a designation in parentheses is added to designate the year of reapproval (e.g. D3588:98(2017)). In the test results tables of appendix 1 only the method number and year of adoption or revision (e.g. D3588:98) will be used. Because the majority of the participating laboratories used ASTM D2163 as test method for the determination of the Propane Composition, it was decided to use the reproducibilities of this test method as target reproducibilities, and to mention the reproducibilities of EN27941 (identical to IP 405 and ISO 7941) for reference only. In ASTM D2163 no reproducibilities of 1-butene and iso-butene are mentioned, the reproducibilities of n-butane were used to calculate the reproducibilities of these two components.

Three laboratories (337, 6018 and 6108) reported deviating results for many of the Propane composition test results and many of the eight test results appeared to be statistical outliers. As the eight test results are not independent, it was decided not to use any of the reported results of these three laboratories for the statistical evaluation. Also the reported physical test results of these three laboratories were excluded, since these values were calculated from the measured Propane composition.

### Liquefied Propane: sample #17210

- Ethane: The determination of this component was not problematic. Four statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers, is in agreement with the requirements of ASTM D2163:14e1 and also with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).
- <u>Propane:</u> The determination of this component was not problematic. Two statistical outliers were observed and two test results were excluded. However, the calculated reproducibility after rejection of the suspect data is in agreement with the requirements of ASTM D2163:14e1 and in good agreement with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).

- Propene: The determination of this component was not problematic. Three statistical outliers were observed and one test result was excluded. However, the calculated reproducibility after rejection of the suspect data is in agreement with the requirements of ASTM D2163:14e1 and also with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).
- iso-Butane: The determination of this component was not problematic. Five statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in full agreement with the requirements of ASTM D2163:14e1 and in good agreement with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).
- <u>n-Butane:</u> The determination of this component may be problematic, depending on the test method used by the laboratory. Three statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ASTM D2163:14e1. However, the calculated reproducibility is in good agreement with the less strict reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).
- <u>1-Butene:</u> The determination of this component was not problematic. Four statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D2163:14e1 and also with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).
- <u>Iso-Butene:</u> The determination of this component was not problematic. Four statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D2163:14e1 and also with the reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).
- <u>n-Pentane:</u> The determination of this component may be problematic, depending on the test method used by the laboratory. Two statistical outliers were observed and one test result was excluded. The calculated reproducibility after rejection of the suspect data is not in agreement with the requirements of ASTM D2163:14e1. However, the calculated reproducibility is in agreement with the less strict reproducibility requirements of EN27941:93 (identical to IP405 and ISO7941).
- <u>Molar Mass:</u> This calculated parameter may not be problematic. The results vary over a range from 44.3 45.582 g/mol. One statistical outlier was observed, and three test results were excluded. The calculated reproducibility after

rejection of the suspect data is in agreement with the reproducibility observed in the previous iis16S03P (0.085 vs. 0.135).

- <u>Rel. Density at 60F</u>: This calculated parameter may not be problematic. The results vary over a range from 0.5107 0.5156. No statistical outliers were present, but four test results were excluded. The calculated reproducibility after rejection of the suspect data is in agreement with the reproducibility observed in the previous iis16S03P (0.00101 vs. 0.00229).
- Abs. VP at 100F: As the reported results calculated via ASTM D2598 and ISO8973 are not identical, it was decided to calculate the absolute vapour pressure for each laboratory according to both test methods by using all reported components concentrations. When the result of the calculation method of ASTM D2598 is compared with the result of the calculation method of ISO8973, it is noticed that the difference in the means is significant, while the difference in the reproducibilities is not significant. See also the discussion in paragraph 5. The calculated reproducibilities after rejection of the five suspect test results are in agreement with the reproducibilities observed in the previous PT iis16S03P (0.872 vs 0.962 for ISO8973:97 and 0.956 vs 1.007 for ASTM D2598:16).
- Rel. VP at 100F: As the reported results calculated via ASTM D2598 and ISO8973 are not identical, it was decided to calculate the relative vapour pressure for each laboratory according to both test methods by using all reported components concentrations. When the result of the calculation method of ASTM D2598 is compared with the result of the calculation method of ISO8973, it is noticed that the difference in the means is significant, while the difference in the reproducibilities is not significant. See also the discussion in paragraph 5. The calculated reproducibilities after rejection of the five suspect test results are in agreement with the reproducibilities observed in the previous PT iis16S03P (0.872 vs 0.962 for ISO8973:97 and 0.956 vs 1.007 for ASTM D2598:16).
- <u>Abs. VP at 40°C:</u> This determination may be problematic for a number of laboratories. The range of the reported test results is large: from 1299 1327 kPa. One statistical outlier was observed and two test results were excluded. The calculated reproducibility after rejection of the suspect data is in agreement with the reproducibility observed in the previous iis16S03P (3.91 vs.5.83).
- <u>Rel. VP at 40°C:</u> This determination may be problematic for a number of laboratories. The range of the reported test results is large: from 1198 1227 kPa. One statistical outlier was observed and two test results were excluded. The calculated reproducibility after rejection of the suspect data is in agreement with the reproducibility observed in the previous iis16S03P (3.88 vs.6.64).

# MON: As the reported results calculated via ASTM D2598 and EN589 are not identical, it was decided to calculate MON for each laboratory according to both test methods by using all reported components concentrations. When the result of the calculation method of ASTM D2598 is compared with the result of the calculation method of EN589, it is noticed that the difference in the means is significant and the difference in the precisions is also significant. See also the discussion in paragraph 5. The calculated reproducibilities after rejection of the suspect data are in agreement with the reproducibilities observed in the previous PT iis16S03P (0.038 vs 0.035 for EN589:08-A1:12 and 0.064 vs 0.069 for ASTM D2598:16). Unfortunately, method ASTM D2598:16 does not mention a MON factor for iso-Butene. Therefore, iis has used the value of cis-2-Butene (83.5) for iso-Butene.

## Ideal Gross Heating Value at 14.696 psi / 60F:

This calculated parameter may be problematic for a number of laboratories. The results vary over a range from 2068.3493 – 2269.1 kJ/mol. As the effect of the different factors from ASTM D3588 and ISO6976 on the calculation is very small, it was decided to calculate Ideal Gross Heating Value according to ASTM D3588:98(2017). See also the discussion in paragraph 5.

## Ideal Net Heating Value at 14.696 psi / 60F:

This calculated parameter may be problematic for a number of laboratories. The results vary over a range from 2049.74 – 2088.3 kJ/mol. As the effect of the different factors from ASTM D3588 and ISO6976 on the calculation is very small, it was decided to calculate Ideal Gross Heating Value according to ASTM D3588:98(2017). See also the discussion in paragraph 5.

## Sulphur in LPG: sample #17211

<u>Sulphur, total</u>: The determination of this component was not problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier, is in good agreement with the requirements of ASTM D6667:14.

### 4.2 PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES

A comparison has been made between the reproducibility as declared by the relevant standard and the reproducibility as found for the group of participating laboratories. The average results per sample, calculated reproducibilities and reproducibilities, derived from literature standards (in casu ASTM, ISO standards) are compared in the next tables.

Parameter	unit	n	average	2.8 * sd	R(D2163:14°1)	R(EN27941)
					in <b>%mol</b>	liqinj. in <b>%mol</b>
Ethane	%mol/mol	43	0.184	0.040	0.107	0.298
Propane	%mol/mol	43	93.95	0.66	4.19	1.02
Propene	%mol/mol	42	0.701	0.076	0.225	0.213
iso-Butane	%mol/mol	42	2.10	0.21	0.22	0.39
n-Butane	%mol/mol	44	2.14	0.30	0.19	0.39
1-Butene	%mol/mol	42	0.150	0.022	0.059	0.160
Iso-Butene	%mol/mol	42	0.151	0.021	0.059	0.160
n-Pentane	%mol/mol	44	0.621	0.097	0.077	0.311
Molar Mass	g/mol	21	44.86	0.08	n.a.	n.a.
Rel. Density at 60F		25	0.5115	0.0010	n.a.	n.a.
Abs. VP at 100F-ISO	psi	41	185.2	0.9	n.a.	n.a.
Abs. VP at 100F-ASTM	psi	41	181.7	1.0	n.a.	n.a.
Rel. VP at 100F-ISO	psi	41	170.5	0.9	n.a.	n.a.
Rel. VP at 100F-ASTM	psi	41	167.0	1.0	n.a.	n.a.
Abs. VP at 40°C	kPa	18	1313.6	3.9	n.a.	n.a.
Rel. VP at 40°C	kPa	18	1212.3	3.9	n.a.	n.a.
MON – EN589		41	95.12	0.04	n.a.	n.a.
MON – D2598		43	96.53	0.06	n.a.	n.a.
Ideal Gross HV	kJ/mol	40	2256.1	3.8	n.a.	n.a.
Net Gross HV	kJ/mol	40	2076.4	3.5	n.a.	n.a.

Table 4: reproducibilities of tests on sample #17210

Parameter	unit	n	average	2.8 * sd	R(lit)
Sulphur, total	mg/kg	7	36.2	9.5	11.3

Table 5: reproducibilitiy of test on sample #17211

Without further statistical calculations it can be concluded that for a large number of parameters there is a good compliance of the group of participating laboratories with the relevant reference test methods. The problematic tests have been discussed in paragraph 4.1.

### 4.3 COMPARISON OF THE PROFICIENCY TEST OF OCTOBER 2017 WITH PREVIOUS PTS

	Oct. 2017	Oct. 2016	Oct. 2015	Oct. 2014	Oct. 2013
Number of reporting labs	47	43	41	44	35
Number of test results reported	536	472	468	395	367
Statistical outliers	30	34	24	27	26
Percentage outliers	5.6%	7.2%	5.1%	6.8%	7.1%

Table 6: comparison with previous proficiency tests on Liquefied Propane (excluded Sulphur in LPG)

In proficiency tests, outlier percentages of 3% - 7.5% are quite normal.

The performance of the determinations of the proficiency tests was compared against the requirements of the respective standards. The conclusions are given the following tables:

Component	Oct. 2017	Oct. 2016	Oct. 2015	Oct. 2014	Oct. 2013
Ethane	++	++	++	-	
Propane	++	++	++	+/-	+/-
Propene	++	++	+	+/-	-
iso-Butane	+/-	-	+	+/-	-
n-Butane	-	-	-	-	
1-Butene	++	++	++		
Iso-Butene	++	+	++		
n-Pentane	-	-	-		

Table 7: comparison determinations on Liquefied Propane against the requirements of the reference standards

For 2013 against D2163:96 and for 2014 – 2017 against D2163:14e1.

Component	Oct. 2017
Sulphur, total	+

Table 8: comparison determinations on Sulphur in LPG against the requirements of the reference standard

The performance of the determinations against the requirements of the respective standards is listed in the above tables. The following performance categories were used:

- ++: group performed much better than the reference test method
- + : group performed better than the reference test method
- +/-: group performance equals the reference test method
- : group performed worse than the reference test method
- -- : group performed much worse than the reference test method

### 5 DISCUSSION

Because several of the reproducibility requirements of ASTM D2163 differ significantly from the reproducibility requirements of EN27941 (for liquid injection), the outcome of the evaluation will be strongly dependent on the target test method selected for the evaluation.

The consensus values as determined in this PT are compared with the average values from the homogeneity testing by EffecTech, United Kingdom in the following table.

Parameter	Average values by EffecTech in %mol/mol	Consensus values from participants results in %mol/mol	Absolute differences in %mol/mol	calc. z-score
Ethane	0.200	0.184	-0.016	+0.41
Propane	94.103	93.953	-0.150	+0.10
Propene	0.706	0.701	-0.005	+0.06
iso-Butane	2.032	2.10	0.068	-0.86
n-Butane	2.065	2.14	0.075	-1.06
1-Butene	0.150	0.150	0.000	-0.00
Iso-Butene	0.148	0.151	0.003	-0.16
n-Pentane	0.597	0.621	0.024	-0.88

Table 9: comparison of consensus values with values determined by EffecTech

From this comparison it is clear that <u>all</u> consensus values as determined in this PT are in line with the values as determined by EffecTech during the preparation of the cylinders.

One laboratory reported traces of Cyclopropane. This component is probably present as impurity in one or more of the pure components that were used to prepare the Propane mixure.

In principle no additional variation should be introduced when applying a calculation on the reported component concentrations. However, in practice a significant additional uncertainty is added in most cases. See the differences between the values from the test results as reported by the participating laboratories (each using its own calculation procedure) and the values as calculated by its using one calculation procedure for each set of laboratory test results.

For the calculation of the Molar Mass, Relative Density, Vapour Pressure, Motor Octane Number and Heating Value several standardized test methods are available, e.g. ASTM D2421 for the interconversion of the units to gas-volume, liquid-volume or mass basis. Also different test methods for the calculation of the Vapour Pressure do exist. In ISO 8973 (identical to IP432) the Vapour Pressure is calculated from the <u>mole fraction</u> per component and a Vapour Pressure factor of that component (given for all components). In ASTM D2598 the Vapour Pressure is calculated from the <u>liquid volume percentage</u> per component and a Vapour Pressure factor of that component (given for only several components).

Also the selection of the tables to be used for the calculations may cause additional uncertainty.

It is remarkable to see that the results for Vapour Pressure from the ASTM D2598 calculation are significantly lower than the results from the ISO8973/IP432 calculation.

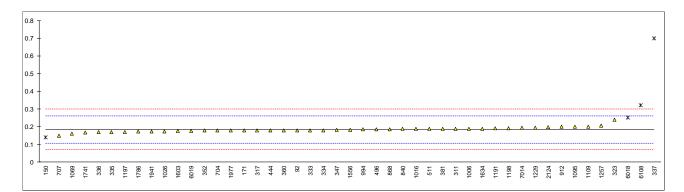
The observed difference is caused by a difference in the VP factor of Ethane. ASTM (Subcommittee D02.H) commented (see also Appendix 3, literature: 20):

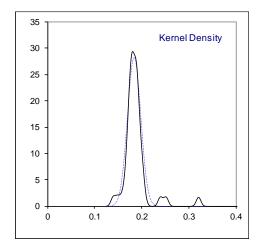
"The vapor pressure of ethane in D2598 was revised a few times prior to 2002. The current value, 611 psi, has remained the same for the last ten years. The revision of ethane was done because components in LPG blends do not necessarily behave as ideal gases. In particular, properties of ethane and ethylene appear to differ from ideality. Factors for these two components have been modified from 'ideal gas' values to make the calculated vapor pressure results more closely approximate actual measured vapor pressures of LPG blends. (i.e. D1267). Chapter 2 of Fuels and Lubricants Handbook (George Totten, © 2003), states that calculated vapor pressure were found to be biased high relative to experimental vapor pressure measured by D1267 for high ethane samples in earlier versions of D2598".

## **APPENDIX 1**

Determination of Ethane on sample #17210; results in %mol/mol

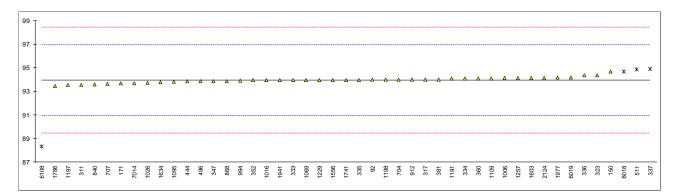
lab	method	value	mark	z(targ)	remarks
92	D2163	0.18	mark	-0.11	Temarko
150	D2163	0.18	R(0.01)	-1.16	
158	52100		11(0.01)		
171	D2163	0.18		-0.11	
311	D2163	0.19		0.15	
317	D2163	0.18		-0.11	
323	D2163	0.24		1.45	
333		0.18		-0.11	
334		0.18		-0.11	
335	D2163	0.17		-0.38	
336	D2163	0.17		-0.38	
337	D2163	0.7	C,R(0.01)	13.46	first reported 0.5
347	D2163	0.184		-0.01	
352	EN27941	0.1788		-0.15	
360	EN27941	0.18		-0.11	
381	EN27941	0.19		0.15	
444	D2163	0.180		-0.11	
496	D2163	0.187		0.07	
511	D2163	0.19		0.15	
529	D0460				
704	D2163	0.179		-0.14	
707	D2163	0.150		-0.90	
754					
823	D0460				
840	D2163	0.189		0.12 0.07	
868 912	D2163 D2163	0.187 0.20		0.07	
912	D2163	0.186		0.41	
1006	D2163	0.190		0.04	
1016	ISO7941	0.189		0.13	
1026	D2163	0.1746		-0.26	
1069	D2712Mod.	0.16		-0.64	
1095	ISO7941	0.2		0.41	
1109	IP405	0.20		0.41	
1191	IP473	0.1915		0.19	
1197	D2163	0.172		-0.32	
1198	D2163	0.192		0.20	
1229	IP473	0.194		0.25	
1257	D2163	0.2056		0.55	
1556	EN27941	0.184		-0.01	
1575					
1603	In house	0.1752		-0.24	
1634	EN27941	0.19		0.15	
1741	EN27941	0.166		-0.48	
1786	D2163	0.173		-0.30	
1941	EN27941	0.1735		-0.28	
1977	D2712	0.1793		-0.13	
2124	D2163	0.1987		0.37	
6018	EN27941	0.252	R(0.01)	1.76	
6019	EN27941	0.176	D(0.04)	-0.22	
6108	D2163	0.321	R(0.01)	3.57	
7014	D2163	0.1933		0.23	
	normality	not OK			
	normanty	43			
	outliers	43			
	mean (n)	4 0.1844			
	st.dev. (n)	0.01412			
	R(calc.)	0.0395			
	st.dev.(D2163:14e1)	0.03832			
	R(D2163:14e1)	0.1073			Compare R(EN27941:93(liq)) = 0.2984
	· · ·				

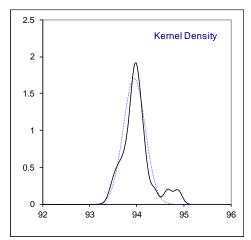




# Determination of Propane on sample #17210; results in %mol/mol

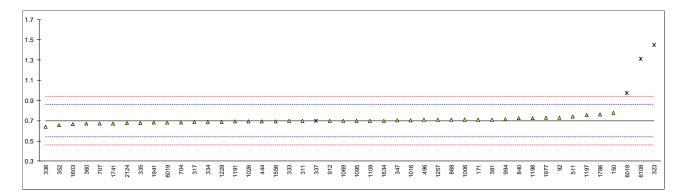
lab	method	value	mark	z(targ)	remarks
			Indik		Tenlaiks
92 150	D2163	93.99		0.02	
150	D2163	94.66		0.47	
158	D0160			0.19	
171	D2163	93.68		-0.18	
311	D2163	93.56		-0.26	
317	D2163	94.01		0.04	
323	D2163	94.38		0.29	
333		93.96		0.00	
334	_	94.07		0.08	
335	D2163	93.97		0.01	
336	D2163	94.37		0.28	
337	D2163	94.9	ex	0.63	excluded, see §4.1
347	D2163	93.855		-0.07	
352	EN27941	93.9334		-0.01	
360	EN27941	94.08		0.08	
381	EN27941	94.01		0.04	
444	D2163	93.839		-0.08	
496	D2163	93.843		-0.07	
511	D2163	94.86	R(0.05)	0.61	
529			. ,		
704	D2163	94.005		0.03	
707	D2163	93.642		-0.21	
754					
823					
840	D2163	93.580		-0.25	
868	D2163	93.866		-0.06	
912	D2163	94.01		0.04	
994	D2163	93.911		-0.03	
1006	D2163	94.117		0.11	
1016	ISO7941	93.934		-0.01	
1026	D2163	93.7351		-0.15	
1069	D2712Mod.	93.96		0.00	
1095	ISO7941	93.8		-0.10	
1109	IP405	94.09		0.09	
1191	IP473	94.0642		0.07	
1197	D2163	93.523		-0.29	
1198	D2163	93.997		0.03	
1229	IP473	93.96		0.00	
1257	D2163	94.1267		0.00	
1556	EN27941	93.963		0.01	
1575					
1603	In house	94.1287		0.12	
1634	EN27941	93.77		-0.12	
1741	EN27941	93.966		0.01	
1786	D2163	93.452		-0.34	
1941	EN27941	93.9355		-0.34	
1941	D2712	93.9355 94.1928		0.01	
2124 6018	D2163 EN27941	94.1536 94.662	ov	0.13	avoludad saa 84.1
6018 6010	EN27941		ex	0.47	excluded, see §4.1
6019 6108	EN27941 D2163	94.200 88.332	R(0.01)	0.17 -3.76	
			R(0.01)		
7014	D2163	93.690		-0.18	
	normolity.	011000			
	normality	suspect			
	n	43			
	outliers	2 (+2 ex)			
	mean (n)	93.9531			
	st.dev. (n)	0.23399			
	R(calc.)	0.6552			
	st.dev.(D2163:14e1)	1.49556			
	R(D2163:14e1)	4.1876			Compare R(EN27941:93(liq)) = 1.017





# Determination of Propene on sample #17210; results in %mol/mol

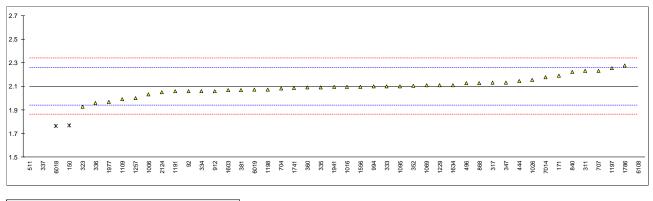
lab	method	value	mark	z(targ)	remarks
92	D2163	0.73		0.36	
150	D2163	0.78		0.98	
158					
171	D2163	0.71		0.11	
311	D2163	0.70		-0.02	
317	D2163	0.69		-0.14	
323	D2163	1.45	R(0.01)	9.30	
333		0.70		-0.02	
334		0.69		-0.14	
335	D2163	0.68		-0.26	
336	D2163	0.64		-0.76	
337	D2163	0.7	ex	-0.02	excluded, see §4.1
347	D2163	0.704		0.03	
352	EN27941	0.6573		-0.55	
360	EN27941	0.67		-0.39	
381	EN27941	0.71		0.11	
444	D2163	0.695		-0.08	
496	D2163	0.707		0.07	
511	D2163	0.74		0.48	
529					
704	D2163	0.684		-0.21	
707	D2163	0.670		-0.39	
754					
823	_				
840	D2163	0.727		0.32	
868	D2163	0.708		0.08	
912	D2163	0.70		-0.02	
994	D2163	0.713		0.15	
1006	D2163	0.709		0.10	
1016	ISO7941	0.704		0.03	
1026	D2163	0.6945		-0.08	
1069	D2712Mod.	0.70		-0.02	
1095	ISO7941	0.7		-0.02	
1109	IP405	0.70		-0.02	
1191	IP473	0.6933		-0.10	
1197	D2163	0.757		0.69	
1198	D2163	0.727		0.32	
1229	IP473	0.69		-0.14	
1257	D2163	0.7075		0.08	
1556	EN27941	0.695		-0.08	
1575	la havea				
1603	In house	0.6695		-0.39	
1634	EN27941	0.70		-0.02	
1741	EN27941	0.671		-0.38	
1786	D2163	0.762		0.75	
1941	EN27941 D2712	0.6806		-0.26	
1977		0.7296		0.35	
2124	D2163	0.6756	P(0.01)	-0.32	
6018	EN27941	0.976	R(0.01)	3.41	
6019 6108	EN27941 D2163	0.681 1.311	R(0.01)	-0.25 7.57	
	D2103		R(0.01)		
7014					
	normality	euenoot			
	normality	suspect 42			
	outliers	4∠ 3 (+1 ex)			
	mean (n)	3 (+1 ex) 0.7012			
	st.dev. (n)	0.7012			
	R(calc.)	0.02720			
	st.dev.(D2163:14e1)	0.0761			
	R(D2163:14e1)	0.08055			Compare R(EN27941:93(liq)) = 0.2132
	(DZ 103.14C1)	0.2200			O(1)part (1)(1)(1)(1)(1)(1)(1)(1)(1)(1)(1)(1)(1)(

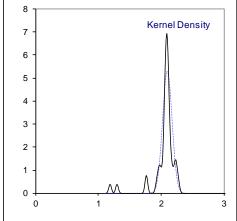


20	
18 -	Kernel Density
16 -	
14 -	
12 -	
10 -	
8 -	
6 -	
4 -	
2 -	
	<u> </u>
	0.0 1 1.0 2

# Determination of iso-Butane on sample #17210; results in %mol/mol

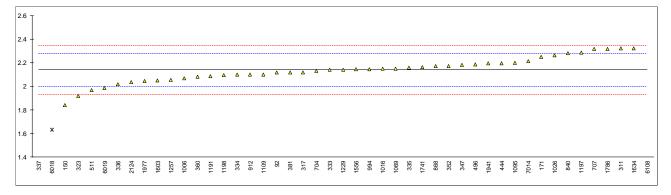
lab	method	value	mark	z(targ)	remarks
92	D2163	2.06		-0.51	
150	D2163	1.77	R(0.01)	-4.17	
158	D0460				
171	D2163 D2163	2.19		1.13 1.63	
311 317	D2163 D2163	2.23 2.13		0.37	
323	D2163	1.93		-2.15	
333	02100	2.10		-0.01	
334		2.06		-0.51	
335	D2163	2.09		-0.13	
336	D2163	1.96		-1.77	
337	D2163	1.3	C,R(0.01)	-10.10	first reported 1.7
347	D2163	2.131		0.38	
352	EN27941	2.1046		0.05	
360	EN27941	2.09		-0.13	
381 444	EN27941	2.07 2.145		-0.39 0.56	
444 496	D2163 D2163	2.145		0.30	
511	D2163	1.19	R(0.01)	-11.48	
529	02100		1((0.01)		
704	D2163	2.082		-0.23	
707	D2163	2.233		1.67	
754					
823					
840	D2163	2.221		1.52	
868	D2163	2.126		0.32	
912	D2163	2.06		-0.51	
994 1006	D2163	2.0996		-0.01	
1006 1016	D2163 ISO7941	2.032 2.095		-0.86 -0.07	
1010	D2163	2.1563		0.70	
1069	D2712Mod.	2.11		0.12	
1095	ISO7941	2.1		-0.01	
1109	IP405	1.99		-1.39	
1191	IP473	2.0599		-0.51	
1197	D2163	2.254		1.93	
1198	D2163	2.074		-0.34	
1229	IP473	2.11		0.12	
1257	D2163	2.0026		-1.24	
1556	EN27941	2.097		-0.05	
1575 1603	In house	 2.0697		-0.39	
1603	EN27941	2.0697 2.11		0.39	
1741	EN27941	2.088		-0.16	
1786	D2163	2.278		2.24	
1941	EN27941	2.0942		-0.08	
1977	D2712	1.9688		-1.66	
2124	D2163	2.0512		-0.62	
6018	EN27941	1.764	R(0.01)	-4.24	
6019	EN27941	2.071		-0.37	
6108	D2163	4.144	R(0.01)	25.77	
7014	D2163	2.1753		0.94	
	normality	OK			
	n	42			
	outliers	5			
	mean (n)	2.1006			
	st.dev. (n) R(calc.)	0.07520 0.2106			
	st.dev.(D2163:14e1)	0.2108			
	R(D2163:14e1)	0.2220			Compare R(EN27941:93(liq)) = 0.3859
	· /	-			

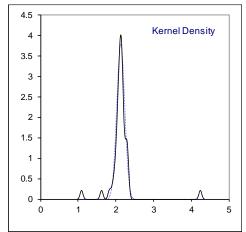




# Determination of n-Butane on sample #17210; results in %mol/mol

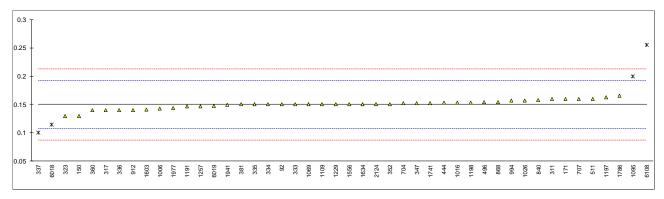
lab	method	value	mark	z(targ)	remarks
92	D2163	2.12		-0.27	
150	D2163	1.84		-4.32	
158 171	D2162	 2.25		1.61	
311	D2163 D2163	2.25		1.61 2.62	
317	D2163 D2163	2.32		-0.27	
323	D2163	1.92		-3.16	
333	02100	2.14		0.02	
334		2.10		-0.56	
335	D2163	2.16		0.31	
336	D2163	2.02		-1.71	
337	D2163	1.1	C,R(0.01)	-15.01	first reported 1.4
347	D2163	2.179		0.58	
352	EN27941	2.1728		0.49	
360	EN27941	2.08		-0.85	
381	EN27941	2.12		-0.27	
444	D2163	2.196		0.83	
496 511	D2163	2.184 1.97		0.66 -2.44	
511 529	D2163	1.97		-2.44	
704	D2163	2.132		-0.10	
707	D2163	2.317		2.58	
754					
823					
840	D2163	2.283		2.09	
868	D2163	2.172		0.48	
912	D2163	2.10		-0.56	
994	D2163	2.144		0.08	
1006	D2163	2.070		-0.99	
1016 1026	ISO7941 D2163	2.148		0.14	
1028	D2703 D2712Mod.	2.2627 2.15		1.79 0.16	
1009	ISO7941	2.15		0.10	
1109	IP405	2.10		-0.56	
1191	IP473	2.0875		-0.74	
1197	D2163	2.285		2.12	
1198	D2163	2.094		-0.65	
1229	IP473	2.14		0.02	
1257	D2163	2.0552		-1.21	
1556	EN27941	2.143		0.06	
1575				4.00	
1603	In house	2.0492		-1.29	
1634 1741	EN27941 EN27941	2.32 2.162		2.62 0.34	
1741	D2163	2.162		2.61	
1941	EN27941	2.1946		0.81	
1977	D2712	2.0445		-1.36	
2124	D2163	2.0349		-1.50	
6018	EN27941	1.631	R(0.01)	-7.34	
6019	EN27941	1.986		-2.21	
6108	D2163	4.246	R(0.01)	30.46	
7014	D2163	2.2144		1.10	
	normality	OK			
	n outliere	44			
	outliers	3 2.1386			
	mean (n) st.dev. (n)	2.1366 0.10555			
	R(calc.)	0.10555			
	st.dev.(D2163:14e1)	0.2555			
	R(D2163:14e1)	0.1937			Compare R(EN27941:93(liq)) = 0.3859
	· ·				

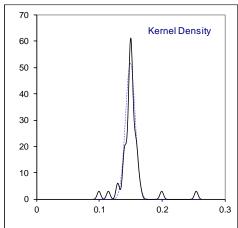




# Determination of 1-Butene on sample #17210; results in %mol/mol

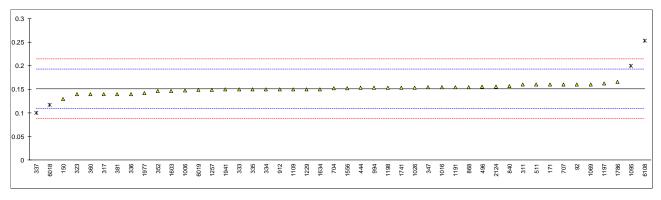
			ampie "		
lab	method	value	mark	z(targ)	remarks
92	D2163	0.15		0.00	
150	D2163	0.13		-0.96	
158	Balaa				
171	D2163	0.16		0.47	
311	D2163	0.16		0.47	
317	D2163	0.14		-0.48	
323	D2163	0.13		-0.96	
333		0.15		0.00	
334 335	D0160	0.15		0.00	
336	D2163 D2163	0.15 0.14		0.00 -0.48	
337	D2163	0.14	R(0.01)	-0.48	
347	D2163	0.152	1((0.01)	0.09	
352	EN27941	0.1506		0.02	
360	EN27941	0.14		-0.48	
381	EN27941	0.15		0.00	
444	D2163	0.153		0.14	
496	D2163	0.154		0.19	
511	D2163	0.16		0.47	
529					
704	D2163	0.152		0.09	
707	D2163	0.160		0.47	
754					
823					
840	D2163	0.158		0.38	
868	D2163	0.154		0.19	
912	D2163	0.14		-0.48	
994	D2163	0.157		0.33	
1006	D2163	0.143		-0.34	
1016	ISO7941	0.153		0.14	
1026	D2163	0.1571		0.34	
1069	D2712Mod.	0.15	D(0.01)	0.00	
1095	ISO7941	0.2	R(0.01)	2.38	
1109 1191	IP405 IP473	0.15 0.1463		0.00 -0.18	
1197	D2163	0.1403		0.62	
1198	D2163	0.153		0.02	
1229	IP473	0.15		0.00	
1257	D2163	0.1465		-0.17	
1556	EN27941	0.150		0.00	
1575					
1603	In house	0.1414		-0.41	
1634	EN27941	0.15		0.00	
1741	EN27941	0.152		0.09	
1786	D2163	0.166		0.76	
1941	EN27941	0.1494		-0.03	
1977	D2712	0.1438		-0.30	
2124	D2163	0.1504		0.02	
6018	EN27941	0.115	R(0.01)	-1.68	
6019	EN27941	0.148	<b>D</b> (a - ··	-0.10	
6108	D2163	0.255	R(0.01)	5.01	
7014					
	a a mar a lite e	01/			
	normality	OK			
	n autliara	42			
	outliers	4 0.1501			
	mean (n) st.dev. (n)	0.1501			
	R(calc.)	0.00773			
	st.dev.(D2163:14e1)	0.02093			
	R(D2163:14e1)	0.02000			Compare R(EN27941:93(liq)) = 0.1599
	(				

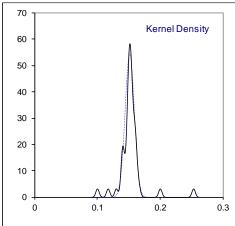




# Determination of iso-Butene on sample #17210; results in %mol/mol

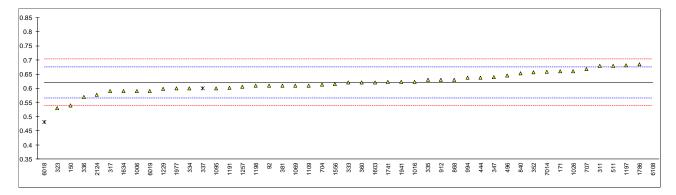
			•		
lab	method	value	mark	z(targ)	remarks
92	D2163	0.16		0.41	
150	D2163	0.13		-1.01	
158					
171	D2163	0.16		0.41	
311	D2163	0.16		0.41	
317	D2163	0.14		-0.54	
323	D2163	0.14		-0.54	
333		0.15		-0.06	
334	_	0.15		-0.06	
335	D2163	0.15		-0.06	
336	D2163	0.14		-0.54	
337	D2163	0.1	R(0.01)	-2.44	
347	D2163	0.154		0.13	
352	EN27941	0.1461		-0.25	
360	EN27941	0.14		-0.54	
381	EN27941	0.14		-0.54	
444	D2163	0.153		0.08	
496	D2163	0.156		0.22	
511	D2163	0.16		0.41	
529	B0/00				
704	D2163	0.152		0.03	
707	D2163	0.160		0.41	
754					
823	D0400				
840	D2163	0.157		0.27	
868	D2163	0.155		0.18	
912	D2163	0.15		-0.06	
994	D2163	0.153 0.148		0.08	
1006 1016	D2163 ISO7941	0.148		-0.16 0.13	
1016	D2163	0.154		0.13	
1020	D2712Mod.	0.1551		0.09	
1009	ISO7941	0.10	R(0.01)	2.32	
11095	IP405	0.2	IX(0.01)	-0.06	
1191	IP473	0.1540		0.13	
1197	D2163	0.163		0.56	
1198	D2163	0.153		0.08	
1229	IP473	0.155		-0.06	
1257	D2163	0.1494		-0.09	
1556	EN27941	0.152		0.03	
1575	ENZIOTI				
1603	In house	0.1461		-0.25	
1634	EN27941	0.15		-0.06	
1741	EN27941	0.153		0.08	
1786	D2163	0.166		0.70	
1941	EN27941	0.1499		-0.07	
1977	D2712	0.1416		-0.46	
2124	D2163	0.1560		0.22	
6018	EN27941	0.117	R(0.01)	-1.63	
6019	EN27941	0.149		-0.11	
6108	D2163	0.253	R(0.01)	4.84	
7014			()		
	normality	OK			
	n	42			
	outliers	4			
	mean (n)	0.1513			
	st.dev. (n)	0.00734			
	R(calc.)	0.0206			
	st.dev.(D2163:14e1)	0.02101			
	R(D2163:14e1)	0.0588			Compare R(EN27941:93(liq)) = 0.1599

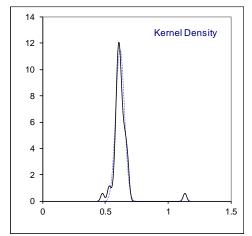




# Determination of n-Pentane on sample #17210; results in %mol/mol

lab	method	value	mark	z(targ)	remarks
92	D2163	0.61		-0.40	
150	D2163	0.54		-2.95	
158	D0400				
171	D2163	0.66		1.42	
311	D2163 D2163	0.68		2.15 -1.13	
317 323	D2163 D2163	0.59 0.53		-1.13	
333	D2103	0.62		-0.04	
334		0.60		-0.77	
335	D2163	0.63		0.33	
336	D2163	0.57		-1.86	
337	D2163	0.6	ex	-0.77	excluded, see §4.1
347	D2163	0.640		0.69	
352	EN27941	0.6565		1.29	
360	EN27941	0.62		-0.04	
381	EN27941	0.61		-0.40	
444	D2163	0.638		0.62	
496	D2163	0.645		0.87	
511	D2163	0.68		2.15	
529 704	D2162			0.26	
704 707	D2163 D2163	0.614 0.668		-0.26 1.71	
754	D2103				
823					
840	D2163	0.653		1.16	
868	D2163	0.631		0.36	
912	D2163	0.63		0.33	
994	D2163	0.637		0.58	
1006	D2163	0.591		-1.10	
1016	ISO7941	0.623		0.07	
1026	D2163	0.6601		1.42	
1069	D2712Mod.	0.61		-0.40	
1095	ISO7941	0.6		-0.77	
1109	IP405	0.61		-0.40	
1191	IP473	0.6024		-0.68	
1197 1198	D2163 D2163	0.682		2.22 -0.44	
1229	IP473	0.609 0.598		-0.44 -0.84	
1225	D2163	0.6065		-0.53	
1556	EN27941	0.616		-0.18	
1575					
1603	In house	0.6202		-0.03	
1634	EN27941	0.59		-1.13	
1741	EN27941	0.622		0.03	
1786	D2163	0.684		2.29	
1941	EN27941	0.6223		0.05	
1977	D2712	0.5997		-0.78	
2124	D2163	0.5780		-1.57	
6018	EN27941	0.481	R(0.05)	-5.10	
6019 6108	EN27941 D2163	0.591 1.137	R(0.01)	-1.10 18.79	
7014	D2163 D2163	0.659	R(U.UT)	18.79	
1014	02100	0.009		1.30	
	normality	ОК			
	n	44			
	outliers	2 (+1 ex)			
	mean (n)	0.6211			
	st.dev. (n)	0.03462			
	R(calc.) st.dev.(D2163:14e1)	0.0969 0.02745			
	R(D2163:14e1)	0.02745 0.0769			Compare R(EN27941:93(liq)) = 0.3109
		0.0700			





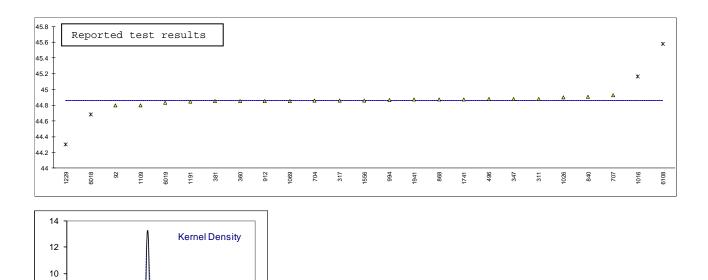
# Determination of Molar Mass on sample #17210; results in g/mol

lab	method	value	mark	z(targ)	remarks
92	D2163	44.8	mark	2(tary)	Tomano
150	22100				
158					
171					
311	INH-407	44.88			
317	INH-001	44.86			
323					
333 334					
334 335					
336					
337					
347	D2598	44.88			
352	10.000				
360	ISO8973	44.85			
381 444	ISO8973	44.8499			
444 496	D2163	44.878			
511					
529					
704	D2421	44.8568			
707	D2421	44.9252			
754					
823	D2508				
840 868	D2598 D2598	44.908 44.87			
912	D2598	44.85			
994	D2163	44.867			
1006					
1016	EN27941	45.1645	ex,E		excluded, iis calculated 44.8617 (D2421)
1026	ISO8973	44.90			
1069 1095	D2712Mod.	44.850			
11095	ISO8973	44.8			
1191	ISO6976	44.8432			
1197					
1198					
1229	ISO8973	44.3	R(0.01)		
1257 1556	Colculated				
1556	Calculated	44.86			
1603					
1634					
1741	D2421	44.8714			
1786	<b>BB</b> ( <b>B</b> (				
1941	D2421	44.8696			
1977 2124					
6018	ISO8973	44.68	ex		excluded, see §4.1
6019	ISO8973	44.83	U.A.		
6108	D2598	45.582	ex		excluded, see §4.1
7014					
	normality	ОК			Calc.by iis from ALL rep. composition results (acc. to D2421:13) OK
	normality n	21			40
	outliers	1 (+3 ex)			40 3 (+3 ex)
	mean (n)	44.862			44.863
	st.dev. (n)	0.0303			0.0291
0.	R(calc.)	0.085			0.082
Comp.	R(iis16S03P)	0.135			

8 -6 -4 -2 -0 -

44

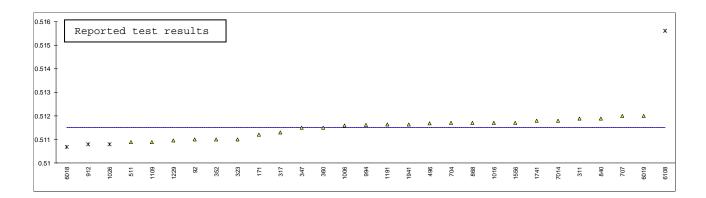
. 44.5 . 45 45.5

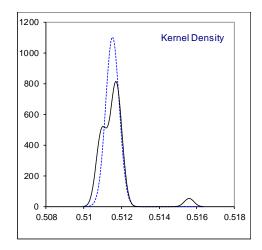


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# Determination of Relative Density at 60/60F on sample #17210; unitless results

92         D2598         0.511	lab	method	value	mark	z(targ)	remarks
150						
158           311       INI-407       0.5112          317       INI-407       0.5113          323       D2598       0.5110          333           334           335           336           337           338           337						
11       D2421       0.5112         311       NH-407       0.5113         323       D2598       0.5110         333						
311       NN-407       0.5113          317       NN-407       0.5113          333            334            335            336            337            336            337            336            337		D2421				
317       INI-001       0.5113          323       D2598       0.5110          335           336           337           338           336           337           338           337						
333           334           335           336           337           337           337           337       0.511          341           444       D2598       0.5115          444           444           444           444           445       D2598       0.5117						
333           334           335           336           337           337           337           337       0.511          341           444       D2598       0.5115          444           444           444           444           445       D2598       0.5117						
336           337           337           337       0.5115          336       0.2598       0.5115          347       D2598       0.5115          348       0.2598       0.5119          449       D2598       0.5109          704       D2598       0.5117          707       D2598       0.5119          840       D2598       0.5119          823            774            840       D2598       0.5119          823						
336           337       D2598       0.5115          360       D2598       0.5115          381           444           451       D2598       0.5116          529            704       D2598       0.5117          774       D2598       0.5117          840       D2598       0.5117          754           868       D2598       0.5116          994       D2598       0.5116          994       D2598       0.5116	334					
337           347       D2598       0.5115          360       D2598       0.5115          381            444            444            444            444            444            704       D2598       0.5110          774       D2598       0.5117          860       D2598       0.5116          912       D2598       0.5116          929       D2598       0.5116          934       D2598       0.5116          935       0.5116           936       D2598       0.5116          937       0.5108       excluded, iis calculated 0.5115 (ASTM D2598)         94       D2598       0.5116          1040       D2598       0.5116          1191       D2598       0.5117 <td>335</td> <td></td> <td></td> <td></td> <td></td> <td></td>	335					
347       D2598       0.5115	336					
352         ISO8973         0.511            360         D2598         0.5116            444              444              444              444              511         D2598         0.51168             774         D2598         0.5117             774         D2598         0.5119             860         D2598         0.5116             912         D2598         0.5116             910         D2598         0.5116             1016         ISO8973         0.5109	337					
380         D2598         0.5115            444              451         D2593         0.51168            529              704         D2598         0.5117            705         D2598         0.5120            840         D2598         0.5117            842         D2598         0.5117	347	D2598	0.5115			
381           444           446           446           511       D2598       0.51109          704       D2598       0.5117          704       D2598       0.5117          764           764           764           764           764           764           779       D2598       0.5117          784         excluded, iis calculated 0.5115 (ASTM D2598)         994       D2598       0.5116          1006       D2598       0.5116          1199       D2598       0.51183          1199       D2598       0.51163          1199       D2598       0.5117       C          1191       D2598       0.5117       C          1192       ISO8973       0	352	ISO8973	0.511			
444		D2598	0.5115			
496         D2598         0.51118            511         D2598         0.5109            704         D2598         0.5117            704         D2598         0.5117            704         D2598         0.5119            737         D2598         0.5119            738              74         D2598         0.5116            791         D2598         0.5116            706         D2598         0.5116            7010         D2598         0.5116            7025         0.5117             704         D2598         0.5109            705              7199         D2598         0.5117         C            7191         D2598         0.5117         C            7192         ISO8973         0.5170         C            766         ISO8973         0.5116            77						
511       D2598       0.5109          529           529       0.5117          707       D2598       0.5120          840       D2598       0.5119          840       D2598       0.5119          912       D2598       0.5116          914       D2598       0.5116          1016       ISO8973       0.5117          1026       0.5108       ex, E          1016       ISO8973       0.5109          1190       D2598       0.51163          1191       D2598       0.5109          1192       ISO8973       0.51097       C						
529           704       D2598       0.5117          774           784           840       D2598       0.5119          912       D2598       0.5116          940       D2598       0.5116          1066       D2598       0.5116          1016       ISO8973       0.5117          1026       0.5108       ex, E          1016       ISO8973       0.5117          1026       0.5108       ex, E          1026       0.5109           1199            1190       D2598       0.5109          1191       D2598       0.51177       C          1197            1198            1229       ISO8973       0.5117       C          1556       ISO8973       0.5117       C						
704         D2598         0.5117		D2598				
707       D2598       0.5120 $754$ $823$ $840$ D2598       0.5117 $912$ D2598       0.5116 $994$ D2598       0.5116 $1006$ D2598       0.5116 $1016$ ISC8973       0.5116 $1026$ 0.5108       ex, E $1095$ excluded, iis calculated 0.5118 (ASTM D2598) $1096$ excluded, iis calculated 0.5118 (ASTM D2598) $1095$ $1199$ D2598       0.51163 $1191$ D2598       0.5117       C $1197$ reported 510.97 $1198$ reported 511.7 $1198$ reported 511.7 $1197$ reported 511.7		Docoo				
754           823           840       D2598       0.5119          912       D2598       0.5116          1006       D2598       0.5116          1016       ISC08973       0.5117          1026       0.5108       ex, E          1095            1109       D2598       0.51163          11191       D2598       0.51103						
823             844         D2598         0.5119            914         D2598         0.51162            914         D2598         0.51162            1006         D2598         0.5116            1016         ISC0973         0.5117            1026         0.5108         ex, E            1026         0.5108         ex, E            1026         0.5108         ex, E            1026         0.5108         ex. E            1095              1109         D2598         0.5109            11197              11197              11198         0.51097         C          reported 510.97           1227               1556         ISO8973         0.5117         C            1603		DZ298				
840         D2598         0.5119						
868         D2598         0.5117		D0500				
912         D2598         0.5108         ex, E						
994         D2598         0.51162            1006         D2598         0.5116            1026         0.5108         ex, E            1026         0.5108         ex, E            1095              1109         D2598         0.5109            1109         D2598         0.5109            1119         D2598         0.51097         C            1197           reported 510.97           1227         ISO8973         0.5117         C            1556         ISO8973         0.5117         C            1634           reported 511.7           1633              1746              1741         IOS8973         0.51180            1744         D2598         0.5150         excluded, see §4.1           6018         ISO8973         0.512				ov E		excluded iis calculated 0 5115 (ASTM D2508)
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				ex, L		excluded, ils calculated 0.5115 (ASTM D2596)
1016       ISO8973       0.5117          1026       0.5108       ex, E          1095            1095            1109       D2598       0.51163           1119       D2598       0.51163           1129       ISO8973       0.51097       C        reported 510.97         1229       ISO8973       0.5117       C        reported 511.7         1556       ISO8973       0.5117       C        reported 511.7         1603              1634             1741       IOS8973       0.51164           1977             1941       D2598       0.5156       ex          6018       ISO8973       0.512						
1026       0.5108       ex, E        excluded, iis calculated 0.5118 (ASTM D2598)         1069            1095            1109       D2598       0.5109           11191       D2598       0.511633           11191       D2598       0.51097       C        reported 510.97         1129       ISO8973       0.5107       C        reported 511.7         1556       ISO8973       0.5117       C        reported 511.7         1557             1603            1741       IOS8973       0.51180           1741       IOS8973       0.5107       ex        excluded, see §4.1         1018       ISO8973       0.512        excluded, see §4.1          6018       ISO8973       0.5156       ex        excluded, see §4.1						
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		1000010		ex. F		excluded, iis calculated 0.5118 (ASTM D2598)
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				ол, Е		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$						
1191       D2598       0.511633          1197           1198           1299       ISO8973       0.51097       C          1257         reported 510.97         1556       ISO8973       0.5117       C          1556       ISO8973       0.5117       C          1633         reported 511.7         1634            1634           1741       IOS8973       0.51180		D2598	0.5109			
1197           1198           129       ISO8973       0.51097       C          1257         reported 510.97         1556       ISO8973       0.5117       C          1556       ISO8973       0.5117       C          1603            1634            1634            1741       IOS8973       0.51180          1786            1941       D2598       0.51164          1977            2124           6018       ISO8973       0.5107       ex          6019       ISO8973       0.5156       ex          6108       D2598       0.5116        excluded, see §4.1         7014       D2598       0.5118           normality       OK        43						
1229       ISO8973       0.51097       C        reported 510.97         1257          reported 511.7         1556       ISO8973       0.5117       C        reported 511.7         1575          reported 511.7         1603            1634           1741       IOS8973       0.51180          1786           1941       D2598       0.51164          1977           2124           6018       ISO8973       0.5107       ex         6018       ISO8973       0.512          6108       D2598       0.5156       ex          6108       D2598       0.5118        excluded, see §4.1         7014       D2598       0.5118           17014       D2598       0.5118           17014       D2598       0.5118						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1198					
1556       ISO8973       0.5117       C        reported 511.7         1575             1603            1634            1634            1634            1741       IOS8973       0.51180          1786            1941       D2598       0.51164          1977            2124         excluded, see §4.1         6018       ISO8973       0.5107       ex          6108       D2598       0.5156       ex          6108       D2598       0.5118        excluded, see §4.1         7014       D2598       0.5118        Calc.by iis from ALL rep. composition results (acc. to D2598:16) suspect         n       25       43       0 (+3 ex)       0 (+3 ex)	1229	ISO8973	0.51097	С		reported 510.97
1575           1603           1634           1741       IOS8973       0.51180          1786           1941       D2598       0.51164          1977           2124           6018       ISO8973       0.5107       ex          6018       ISO8973       0.512        excluded, see §4.1         6019       ISO8973       0.512        excluded, see §4.1         6108       D2598       0.5156       ex        excluded, see §4.1         7014       D2598       0.5118        Excluded, see §4.1          normality       OK        suspect           n       25       43         43          outliers       0 (+4 ex)       0 (+3 ex)       0 (+3 ex)	1257					
1603           1634           1741       IOS8973       0.51180          1786           1941       D2598       0.51164          1977           2124           6018       ISO8973       0.5107       ex         6019       ISO8973       0.512          6108       D2598       0.5156       ex         6108       D2598       0.516       ex         7014       D2598       0.5118          Calc.by iis from ALL rep. composition results (acc. to D2598:16)       suspect         n       25       43         outliers       0 (+4 ex)       0 (+3 ex)	1556	ISO8973	0.5117	С		reported 511.7
1634           1741       IOS8973       0.51180          1786           1941       D2598       0.51164          1977           2124           6018       ISO8973       0.5107       ex         6019       ISO8973       0.512          6108       D2598       0.5156       ex         6108       D2598       0.516       ex         7014       D2598       0.5118          Calc.by iis from ALL rep. composition results (acc. to D2598:16)       suspect         n       25       43         outliers       0 (+4 ex)       0 (+3 ex)						
1741       IOS8973       0.51180          1786           1941       D2598       0.51164          1977           2124           6018       ISO8973       0.5107       ex         6019       ISO8973       0.512          6108       D2598       0.5156       ex         6108       D2598       0.5156       ex         6108       D2598       0.5118          Calc.by iis from ALL rep. composition results (acc. to D2598:16)       suspect         normality       OK       43         outliers       0 (+4 ex)       0 (+3 ex)						
1786           1941       D2598       0.51164          1977           2124           6018       ISO8973       0.5107       ex         6019       ISO8973       0.512          6108       D2598       0.5156       ex         6108       D2598       0.5156       ex         6108       D2598       0.5118          Calc.by iis from ALL rep. composition results (acc. to D2598:16)       suspect         normality       OK       43         outliers       0 (+4 ex)       0 (+3 ex)						
1941       D2598       0.51164          1977           2124           6018       ISO8973       0.5107       ex         6019       ISO8973       0.512          6108       D2598       0.5156       ex         6108       D2598       0.5156       ex         7014       D2598       0.5118          Calc.by iis from ALL rep. composition results (acc. to D2598:16)         normality       OK       suspect         n       25       43         outliers       0 (+4 ex)       0 (+3 ex)		IOS8973				
1977           2124           6018       ISO8973       0.5107       ex         6019       ISO8973       0.512          6108       D2598       0.5156       ex         6108       D2598       0.5118          routility       OK          normality       OK       Suspect         n       25       43         outliers       0 (+4 ex)       0 (+3 ex)		Docoo				
2124            6018       ISO8973       0.5107       ex          6019       ISO8973       0.512        excluded, see §4.1         6018       D2598       0.5156       ex        excluded, see §4.1         7014       D2598       0.5118        excluded, see §4.1         7014       D2598       0.5118        Calc.by iis from ALL rep. composition results (acc. to D2598:16)         normality       OK       suspect          n       25       43          outliers       0 (+4 ex)       0 (+3 ex)       0 (+3 ex)		D2598				
6018       ISO8973       0.5107       ex        excluded, see §4.1         6019       ISO8973       0.512        excluded, see §4.1         6108       D2598       0.5156       ex        excluded, see §4.1         7014       D2598       0.5118        excluded, see §4.1         7014       D2598       0.5118        Calc.by iis from ALL rep. composition results (acc. to D2598:16)         normality       OK       suspect       43         outliers       0 (+4 ex)       0 (+3 ex)						
6019         ISO8973         0.512            6108         D2598         0.5156         ex            7014         D2598         0.5118          excluded, see §4.1           7014         D2598         0.5118          excluded, see §4.1           normality         OK         Suspect            n         25         43            outliers         0 (+4 ex)         0 (+3 ex)         0 (+3 ex)		1000070		<b></b>		avaludad aga \$4.1
6108         D2598         0.5156         ex          excluded, see §4.1           7014         D2598         0.5118          calc.by iis from ALL rep. composition results (acc. to D2598:16)           normality         OK         suspect           n         25         43           outliers         0 (+4 ex)         0 (+3 ex)				ex		excluded, see 94.1
7014         D2598         0.5118            normality         OK         Suspect           n         25         43           outliers         0 (+4 ex)         0 (+3 ex)				0		ovaludad, soo 84.1
NormalityOKCalc.by iis from ALL rep. composition results (acc. to D2598:16)n2543outliers0 (+4 ex)0 (+3 ex)				ex		excluded, see 34.1
normality         OK         suspect           n         25         43           outliers         0 (+4 ex)         0 (+3 ex)	7014	02090	0.5116			
normality         OK         suspect           n         25         43           outliers         0 (+4 ex)         0 (+3 ex)						Calc.by iis from ALL rep. composition results (acc. to D2598-16)
n 25 43 outliers 0 (+4 ex) 0 (+3 ex)		normalitv	ОК			
outliers 0 (+4 ex) 0 (+3 ex)						
mean (n) 0.51151 0.51156		mean (n)	0.51151			0.51156
st.dev. (n) 0.000361 0.000225						0.000225
R(calc.) 0.00101 0.00063						0.00063
Comp. R(iis16S03P) 0.00229	Comp.	R(iis16S03P)	0.00229			





# Determination of Absolute Vapour Pressure at 100F on sample #17210; results in psi

lab	method	value	mark	 remarks	
92					
150					
158 171					
311	ISO8973	185.3			
317	ISO8973	185.5			
323					
333					
334					
335					
336					
337	Docoo				
347	D2598	181.6			
352	1909072	 195 5			
360 381	ISO8973	185.5 			
444					
496	D2598	181.57			
511	D2598	169	ex,E	 excluded, iis calculated 183.1 (D2598), mix up with Rel. Vap. Pro	es.?
529					
704	ISO8973	185.4			
707	ISO8973	184.7			
754					
823	Docoo				
840	D2598	181.3			
868 912	D2598	181.6 			
994	D2598	185.3	ex,E	 excluded, iis calc.181.7 (D2598), however iis calc. 185.2 (ISO89	173)
1006	D2598	182.0	0,,		10)
1016		185.4024			
1026		179.1	ex,E	 excluded, iis calculated 181.3 (D2598) and iis calc. 184.8 (ISO8	973)
1069					
1095	ISO8973	183.9	ex,E	 excluded, iis calculated 185.09 (ISO8973) and iis calc. 181.6 (D	2598)
1109	ISO8973	185.5			
1191	ISO8973	185.584			
1197 1198					
1229					
1257					
1556					
1575					
1603					
1634					
1741	ISO8973	185.22			
1786	1000070	 105 055			
1941 1977	ISO8973	185.255			
1977 2124					
6018					
6019	ISO8973	1280	ex	 excluded, unit error? (kPa?)	
6108	D2598	158.0	ex,E	 excluded, see §4.1, iis calculated 175.1 (D2598)	
7014				 -	
	normality n outliers mean (n) st.dev. (n)			Calculated by iis from ALL reported composition results         ISO8973:97/IP432       D2598:16         OK       suspect         41       41         2 (+3 ex)       2 (+3 ex)         185.176       181.704         0.3114       0.3315	
	R(calc.)			0.3114 0.3315 0.872 0.956	
Comp.	R(iis16S03P)			0.962 0.950	

0 -

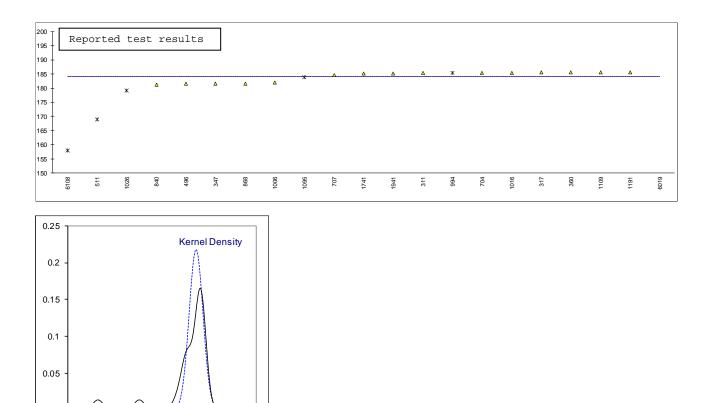
150

160

. 170 180

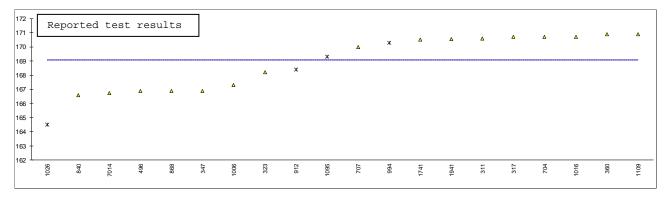
190

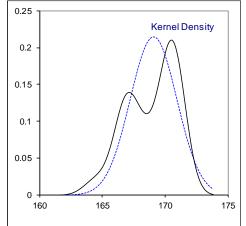
200



# Determination of Relative Vapour Pressure at 100F on sample #17210; results in psi

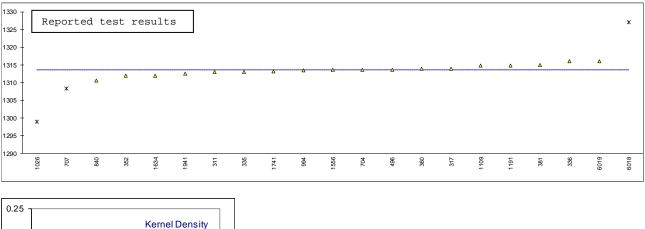
lab	method	value	mark	z(targ)	remarks	
92						
150						
158						
171						
311	ISO8973	170.6				
317	ISO8973	170.7				
323	D2598	168.2				
333						
334						
335						
336						
337						
347	D2598	166.9				
352						
360	ISO8973	170.9				
381						
444						
496	D2598	166.87				
511						
529						
704	ISO8973	170.7				
707	ISO8973	170.0				
754						
823						
840	D2598	166.6				
868	D2598	166.9				
912	D2598	168.4	ex,E		excluded, iis calculated 167.2 (D2598)	
994	D2598	170.3	ex,E		excluded, iis calculated 167.0 (D2598)	
1006	D2598	167.3				
1016		170.7064				
1026		164.5	ex,E		excluded, iis calc. 166.6 (D2598) and iis calc. 170.1 (ISO8973)	
1069						
1095	ISO8973	169.3	ex,E		excluded, iis calculated 170.4 (ISO8973)	
1109	ISO8973	170.9				
1191						
1197						
1198						
1229						
1257						
1556						
1575						
1603						
1634	1000070					
1741	ISO8973	170.52				
1786	1000070					
1941	ISO8973	170.559				
1977						
2124						
6018						
6019						
6108 7014	D2509	 166 75				
7014	D2598	166.75				
					Calculated by iis from ALL reported composition results	
					<u>ISO8973:97/IP432</u> <u>D2598:16</u>	
	normality				OK suspect	
	n				41 41	
	outliers				2 (+3 ex) 2 (+3 ex)	
	mean (n)				170.480 167.008	
	st.dev. (n)				0.3114 0.3415	
	R(calc.)				0.872 0.956	
Comp.	R(iis16S03P)				0.962 1.007	
	```					

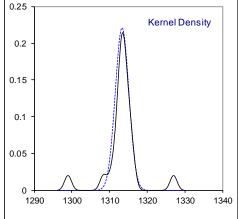




# Determination of Absolute Vapour Pressure at 40°C on sample #17210; results in kPa

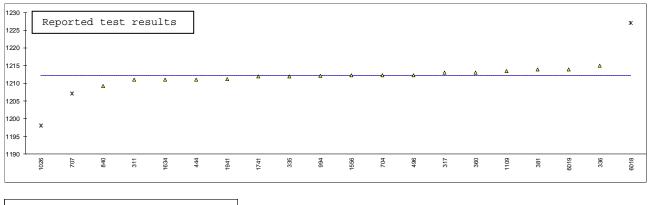
lab	method	value	mark	z(targ)	remarks
92 150					
150 158					
171					
311	ISO8973	1313			
317	ISO8973	1314			
323					
333					
334	1000070				
335 336	ISO8973 ISO8973	1313 1316			
337	1000373				
347					
352	ISO8973	1312			
360	ISO8973	1314			
381	ISO8973	1315			
444	1000070				
496 511	ISO8973	1313.64 			
529					
704	ISO8973	1313.6			
707	ISO8973	1308.4	G(0.05)		
754					
823	10.000-0				
840	ISO8973	1310.6			
868 912					
994	ISO8973	1313.4			
1006	1000010				
1016					
1026		1299	ex,E		excluded, iis calculated 1311 (ISO8973)
1069					
1095	1000070				
1109 1191	ISO8973 ISO8973	1314.8 1314.90			
1197	1000375				
1198					
1229					
1257					
1556	ISO8973	1313.56			
1575					
1603 1634	ISO8973	 1312			
1741	ISO8973	1313.21			
1786					
1941	ISO8973	1312.54			
1977					
2124	1000070				avaluated and \$4.4
6018 6019	ISO8973 ISO8973	1327 1316	ex		excluded, see §4.1
6108	1300973				
7014					
	normality	OK			
	n autliara	18 1 (+ 2 ov)			
	outliers mean (n)	1 (+2 ex) 1313.63			
	st.dev. (n)	1.395			
	R(calc.)	3.91			
Comp.	R(iis16S03P)	5.83			
•					

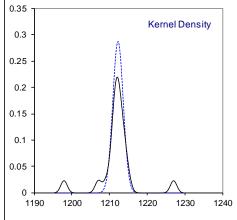




# Determination of Relative Vapour Pressure at 40°C on sample #17210; results in kPa

lab	method	value	mark	z(targ)	remarks
92 150					
150					
171					
311	ISO8973	1211			
317	ISO8973	1213			
323					
333 334					
335	ISO8973	1212			
336	ISO8973	1215			
337					
347					
352 360	1000072				
360	ISO8973 ISO8973	1213 1214			
444	ISO8973	1211.1			
496	ISO8973	1212.32			
511					
529	1000070				
704 707	ISO8973 ISO8973	1212.3 1207.1	G(0.05)		
754	1500375		0(0.03)		
823					
840	ISO8973	1209.3			
868					
912 994	ISO8973	 1212.1			
1006	1300973	1212.1			
1016					
1026		1198	ex,E		excluded, iis calculated 1209 (ISO8973)
1069					
1095	1000072	 1010 E			
1109 1191	ISO8973	1213.5			
1197					
1198					
1229					
1257	1000070				
1556 1575	ISO8973	1212.24			
1603					
1634	ISO8973	1211			
1741	ISO8973	1211.89			
1786	1000070				
1941 1977	ISO8973	1211.22			
2124					
6018	ISO8973	1227	ex		excluded, see §4.1
6019	ISO8973	1214			
6108					
7014					
	normality	ОК			
	n	18			
	outliers	1 (+2 ex)			
	mean (n)	1212.29			
	st.dev. (n)	1.387			
Comp.	R(calc.) R(iis16S03P)	3.88 6.64			
comp.		0.04			





# Determination of Motor Octane Number, MON on sample #17210;

lab	method	value	mark	z(targ)	remarks
92					
150					
158					
171					
311	EN589	95.6			
317	EN589	95.1			
323					
333					
334					
335					
336	EN589	95.1			
337					
347					
352	ENISOO				
360	EN589	95.1			
381	EN589	95.5			
444	Docoo				
496	D2598	96.510			
511 520					
529 704	EN589	 95.12			
704	EN589 EN589	95.12 95.11			
754	LINDOS				
823					
840	D2598	96.47			
868	D2598	96.6			
912	B2000				
994	D2598	95.12			method used is probably EN598?
1006	22000				
1016					
1026		94.77			
1069					
1095					
1109	EN589	95.1			
1191					
1197					
1198					
1229					
1257					
1556					
1575					
1603					
1634	ENICOO				
1741	EN589	95.510			
1786 1941	EN589	 05 500			
1941 1977	LINDOA	95.509			
2124					
6018					
6018					
6108	D2598	95.8	ex		excluded, see §4.1
7014					
					Calculated by iis from ALL reported composition results
					<u>EN589:08-A1:12</u> <u>D2598:16</u>
	normality				suspect OK
	n				41 43
	outliers				2 (+3 ex) 0 (+3 ex)
	mean (n)				96.529 ໌
	st.dev. (n)				0.0136 0.0228
	R(calc.)				0.038 0.064
Comp.	R(iis16S03P)				0.035 0.069

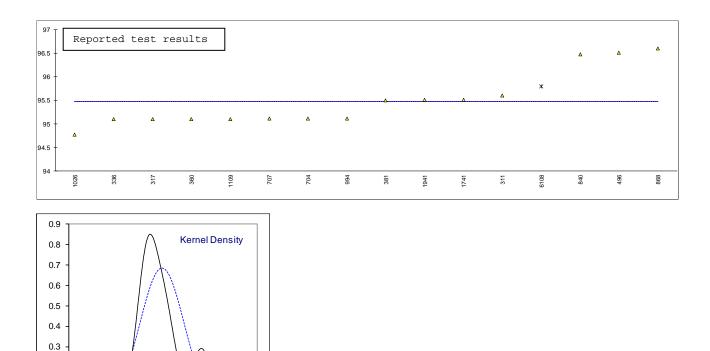
0.2 0.1 0

93

. 94 . 95 97

96

. 98



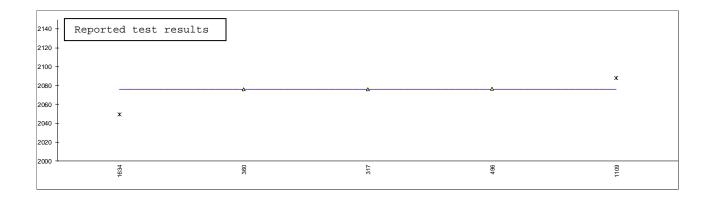
# Determination of Ideal Gross Heating Value at 14.696psi/60Fon sample #17210; in kJ/mol

lab	method	value	mark	z(tora)	remarks
92	metriou	value	mark	z(targ)	Temarka
150					
158					
171					
311	Docoo				
317	D3588	2256.01			
323 333					
334					
335					
336					
337					
347 352					
360	ISO6976	2255.64			
381					
444					
496	D3588	2256.79			
511					
529 704					
704					
754					
823					
840					
868					
912 994					
1006					
1016					
1026					
1069					
1095 1109	D3588	 2269.1	ex,E		excluded, iis calculated 2254.58 (D5388)
1191	20000		0A,L		
1197					
1198					
1229					
1257 1556					
1575					
1603	In house	2068.3493	ex, E		excluded, iis calculated 2255.27 (D5388)
1634	D3588	2227.38	ex, E		excluded, iis calculated 2256.39 (D5388)
1741					
1786					
1941 1977					
2124					
6018					
6019					
6108					
7014					
	normality				Calculated by iis from ALL reported composition results <u>D3588:98</u> OK
	n outlioro				40 2 (12 cm)
	outliers mean (n)				3 (+3 ex) 2256.14
	st.dev. (n)				1.346
	R(calc.)				3.77
	R(target)				n.a.

<sup>2350</sup> T	Reported test results	]				
2300 -	_	]				
2250 -	*	Δ	Δ	<u>۵</u>		*
2200 -						
2150 -						
2100 -						
2050 -	*					
2000	~ +					
	16 03 16 34	39	317	8	5	1109

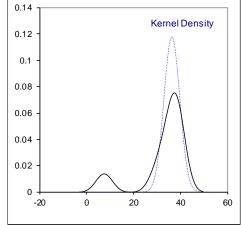
# Determination of Ideal Net Heating Value at 14.696 psi/60F on sample #17210; results in kJ/mol

lab	method	value	mark	z(targ)	remarks
92 150					
158					
171					
311					
317	D3588	2076.12			
323					
333 334					
334 335					
336					
337					
347					
352	1000070				
360 381	ISO6976	2075.89			
444					
496	D3588	2076.54			
511					
529					
704					
707 754					
823					
840					
868					
912					
994					
1006					
1016 1026					
1069					
1095					
1109	D3588	2088.3	ex, E		excluded, iis calculated 2074.95 (D5388)
1191					
1197 1198					
1229					
1257					
1556					
1575					
1603	Docoo		<b>Г</b>		augluded iin colouleted 2070 C4 (DE200)
1634 1741	D3588	2049.74	ex, E		excluded, iis calculated 2076.64 (D5388)
1786					
1941					
1977					
2124					
6018					
6019 6108					
7014					
7014					
	normality n outliers mean (n) st doy (n)				Calculated by iis from ALL reported composition results D3588:98 OK 40 3 (+3 ex) 2076.41 1.261
	st.dev. (n) R(calc.)				1.261 3.53
	R(target)				n.a.



## Determination of Sulphur, total on sample #17211; results in mg/kg

lab	method	value	mark	z(targ)	remarks		
150 158	D6667	38.6	С	0.58	first reported: 4.6		
171	D6667	34		-0.55			
323	D6667	7.4	C,D(0.05)	-7.12	first reported: 6.5		
347	D6667	35.7		-0.13			
1006	D6667	39		0.68			
1095	D6667	39		0.68			
2124	B						
6018	D6667	29.84	0	-1.58	first as a start 70.0 see DMO/La		
6019	D6228	37.5	С	0.31	first reported: 72.6 mg DMS/kg		
	normality	unknown					
	n	7					
	outliers	1					
	mean (n)	36.23					
	st.dev. (n)	3.383					
	R(calc.)	9.47					
	st.dev.(D6667:14)	4.050					
	R(D6667:14)	11.34					
<sup>60</sup> T							
50 -							
40 -					۵	۵	۵
			۵	Δ	<u>u</u>		
30 -	<b>_</b>						
20 -							
20							
10 -	¥						
	*						
0	323		171	347	6019	1006	1095
	ю 09		<del>~</del>	ų	90	<u>0</u>	9
L							
0.1.1							



## **APPENDIX 2**

### Number of participants per country in the Propane PT iis17S03P

- 1 lab in AZERBAIJAN
- 1 lab in BELGIUM
- 1 lab in BULGARIA
- 1 lab in CANADA
- 1 lab in CHINA, People's Republic
- 1 lab in COSTA RICA
- 3 labs in FINLAND
- 5 labs in FRANCE
- 2 labs in GERMANY
- 1 lab in INDIA
- 1 lab in IRAN, Islamic Republic of
- 3 labs in MALAYSIA
- 1 lab in MEXICO
- 4 labs in NETHERLANDS
- 1 lab in PERU
- 5 labs in PORTUGAL
- 1 lab in RUSSIAN FEDERATION
- 4 labs in SERBIA
- 1 lab in SOUTH KOREA
- 1 lab in SPAIN
- 1 lab in SWEDEN
- 1 lab in TAIWAN
- 2 labs in UKRAINE
- 1 lab in UNITED ARAB EMIRATES
- 1 lab in UNITED KINGDOM
- 3 labs in UNITED STATES OF AMERICA
- 2 labs in VIETNAM

#### Number of participants per country in the Sulphur in LPG PT iis17S03S

- 1 lab in AUSTRALIA
- 1 lab in BELGIUM
- 3 labs in PORTUGAL
- 1 lab in SPAIN
- 1 lab in TAIWAN
- 3 labs in UNITED STATES OF AMERICA

## **APPENDIX 3**

### Abbreviations:

С	= final result after checking of first reported suspect test result
D(0.01)	= outlier in Dixon's outlier test
D(0.05)	= straggler in Dixon's outlier test
G(0.01)	= outlier in Grubbs' outlier test
G(0.05)	= straggler in Grubbs' outlier test
DG(0.01)	= outlier in Double Grubbs' outlier test
DG(0.05)	= straggler in Double Grubbs' outlier test
R(0.01)	= outlier in Rosner's outlier test
R(0.05)	= straggler in Rosner's outlier test
E	= probably an error in calculations
ex	= test result excluded from the statistical evaluation
n.a.	= not applicable
n.e.	= not evaluated
fr.	= first reported
SDS	= safety data sheet

## Literature:

- 1 iis Interlaboratory Studies, Protocol for the Organization, Statistics and Evaluation, March 2017
- 2 ASTM D2163:14e1
- 3 ASTM D2421:13
- 4 ISO 5725:86
- 5 ISO 5725, parts 1-6, 1994
- 6 M. Thompson and R. Wood, J. AOAC Int, <u>76</u>, 926, (1993)
- 7 W.J. Youden and E.H. Steiner, Statistical Manual of the AOAC, (1975)
- 8 IP 367:84
- 9 DIN 38402 T41/42
- 10 P.L. Davies, First reported Z. Anal. Chem, <u>331</u>, 513, (1988)
- 11 J.N. Miller, Analyst, <u>118</u>, 455, (1993)
- 12 Analytical Methods Committee Technical Brief, No4 January 2001
- 13 P.J. Lowthian and M. Thompson, The Royal Society of Chemistry, Analyst, 127, 1359-1364 (2002)
- 14 ISO 17043:2010
- 15 EN 27941:1993 = ISO 7941:88 = IP 405:94
- 16 ASTM D2598:16
- 17 IP 432:2000 = ISO 8973:1997
- 18 ASTM D2598:16
- 19 EN 589:08-A1:12
- 20 Private communication ASTM Subcommittee D02.H
- 21 ASTM D3588:98(2017)
- 22 ISO 6976:95(1996)
- 23 ISO 6976:16
- 24 Bernard Rosner, Percentage Points for a Generalized ESD Many-Outlier Procedure, Technometrics, 25(2), pp. 165-172, (1983)