# Results of Proficiency Test Hydraulic Fluid (fresh) November 2017

Organised by: Institute for Interlaboratory Studies Spijkenisse, the Netherlands

ing. G.A. Oosterlaken-Buijs Author: dr. R.G. Visser & ing. R.J. Starink Corrector:

iis17L07 Report no.

February 2018

- EMPTY PAGE -

# **CONTENTS**

1	INTRODUCTION	4
2	SET UP	4
2.1	ACCREDITATION	4
2.2	PROTOCOL	4
2.3	CONFIDENTIALITY STATEMENT	4
2.4	SAMPLES	5
2.5	STABILITY OF THE SAMPLES	5
2.6	ANALYSES	6
3	RESULTS	6
3.1	STATISTICS	6
3.2	GRAPHICS	7
3.3	Z-SCORES	7
4	EVALUATION	8
4.1	EVALUATION PER TEST	8
4.2	PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES	11
4.3	COMPARISON OF THE PT OF NOVEMBER 2017 WITH THE PREVIOUS PTS	12

# Appendices:

1.	Data and statistical results	14
2.	Reported details: Foam determination	37
3.	Number of participants per country	39
4	Abhreviations and literature	40

### 1 Introduction

Since 2003, the Institute for Interlaboratory Studies (iis) organizes a proficiency test (PT) for the analysis on <u>used</u> Hydraulic Fluid every year. In 2014 it was decided to organize a proficiency test for the analyses on <u>fresh</u> Hydraulic Fluid next to used Hydralic Fluid. This decision was based on the outcome of a questionnaire that was sent to all participants in 2014. During the annual program 2017/2018, it was decided to continue the round robin for the analysis on fresh Hydraulic Fluid. In this interlaboratory study, 46 laboratories from 33 different countries did register for participation. See appendix 3 for the number of participants per country. In this report, the test results of the 2017 interlaboratory study on fresh Hydraulic Fluid are presented and discussed. This report can also be downloaded from the iis website www.iisnl.com.

### 2 SET UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, the Netherlands, was the organiser of this proficiency test (PT). Sample analyses for fit-for-use and homogeneity testing were subcontracted to an ISO/IEC 17025 accredited laboratory. It was decided to send one sample of one litre of fresh oil, labelled #17225. The participants were requested to report rounded and unrounded test results. The unrounded test results were preferably used for statistical evaluation.

### 2.1 ACCREDITATION

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, is accredited in agreement with ISO/IEC 17043:2010 (R007), since January 2000, by the Dutch Accreditation Council (Raad voor Accreditatie). This PT falls under the accredited scope. This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentiality of participant's data. Feedback from the participants on the reported data is encouraged and customer's satisfaction is measured on regular basis by sending out questionnaires.

### 2.2 PROTOCOL

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organization, Statistics and Evaluation' of March 2017 (iis-protocol, version 3.4). This protocol is electronically available through the iis website www.iisnl.com, from the FAQ page.

### 2.3 CONFIDENTIALITY STATEMENT

All data presented in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

### 2.4 SAMPLES

The necessary bulk material was obtained from a local supplier. The bulk material was homogenised. After homogenisation, 68 amber glass bottles of 1 litre were filled and labelled #17225. The homogeneity of the subsamples #17225 was checked by determination of Density at 15°C in accordance with ASTM D4052 and Kinematic Viscosity at 40°C according to ASTM D445 on 10 stratified randomly selected samples.

	Density at 15 °C in kg/L	Kinematic Viscosity at 40 °C in mm²/s
Sample #17225-1	0.87460	97.91
Sample #17225-2	0.87460	97.92
Sample #17225-3	0.87460	97.91
Sample #17225-4	0.87461	97.89
Sample #17225-5	0.87460	97.92
Sample #17225-6	0.87460	97.93
Sample #17225-7	0.87460	97.90
Sample #17225-8	0.87461	97.93
Sample #17225-9	0.87461	97.88
Sample #17225-10	0.87461	97.92

Table 1: homogeneity test results of subsamples #17225

From the test results of table 1, the repeatabilities were calculated and compared with 0.3 times the corresponding reproducibilities of the reference test methods in agreement with the procedure of ISO 13528, Annex B2 in the next table:

	Density at 15 °C in kg/L	Kinematic Viscosity at 40 °C in mm²/s
r (observed)	0.00001	0.05
reference test method	D4052:16	D445:17a
0.3 x R (ref. test method)	0.00015	0.36

Table 2: evaluation of the repeatabilities of subsamples #17225

The calculated repeatabilities in table 2 were both less than 0.3 times the corresponding reproducibilities of the reference test methods. Therefore, homogeneity of the subsamples #17225 was assumed.

To each of the participating laboratories one sample of 1 litre amber glass bottle, labelled #17225, was sent on October 25, 2017. An SDS was added to the sample package.

### 2.5 STABILITY OF THE SAMPLES

The stability of fresh Hydraulic Fluid, packed in amber glass bottles was checked. The material was found sufficiently stable for the period of the proficiency test.

### 2.6 ANALYSES

The participants were asked to determine on sample #17225; Acid Number (total), Copper Corrosion (3hrs at 50°C), Density at 15°C, Flash Point PMcc, Foam Characteristics (Foam Tendency, Foam Stability), Kinematic Viscosity at 40°C and at 100°C, Viscosity Index, Viscosity Stabinger at 40°C and at 100°C, Pour Point (manual and automated), Sulphur, Water content (by KF), Water Separability at 82°C and Calcium, Phosphorus and Zinc. Also additional guestions were asked about the foam determination.

It was explicitly requested to treat the samples as if they were routine samples and to report the test results using the indicated units on the report form and not to round the test results, but report as much significant figures as possible. It was also requested not to report 'less than' results, which are above the detection limit, because such test results cannot be used for meaningful statistical calculations.

To get comparable test results, a detailed report form and a letter of instructions are prepared. On the report form the reporting units are given as well as the reference test methods that will be used during the evaluation. The detailed report form and the letter of instructions are both made available on the data entry portal www.kpmd.co.uk/sgs-iis/. The participating laboratories are also requested to confirm the sample receipt on this data entry portal. The letter of instructions can also be downloaded from the iis website www.iisnl.com.

### 3 RESULTS

During five weeks after sample dispatch, the test results of the individual laboratories were gathered via the data entry portal www.kpmd.co.uk/sgs-iis/. The reported test results are tabulated per determination in appendix 1 of this report. The laboratories are presented by their code numbers.

Directly after the deadline, a reminder was sent to those laboratories that had not reported test results at that moment. Shortly after the deadline, the available test results were screened for suspect data. A test result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the reported test results (no reanalysis). Additional or corrected test results are used for data analysis and original test results are placed under 'Remarks' in the test result tables in appendix 1. Test results that came in after the deadline were not taken into account in this screening for suspect data and thus these participants were not requested for checks.

### 3.1 STATISTICS

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of March 2017 (iis-protocol, version 3.4).

For the statistical evaluation, the *unrounded* (when available) figures were used instead of the rounded test results. Test results reported as '<...' or '>...' were not used in the statistical evaluation.

First, the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test a variant of the Kolmogorov-Smirnov test and by the calculation of skewness and kurtosis. Evaluation of the three normality indicators in combination with the visual evaluation of the graphic Kernel density plot, lead to judgement of the normality being either 'unknown', 'OK', 'suspect' or 'not OK'. After removal of outliers, this check was repeated. If a data set does not have a normal distribution, the (results of the) statistical evaluation should be used with due care.

According to ISO 5725 the original test results per determination were submitted to Dixon's, Grubbs' and/or Rosner's outlier tests. Outliers are marked by D(0.01) for the Dixon's test, by G(0.01) or DG(0.01) for the Grubbs' test and by R(0.01) for the Rosner's test. Stragglers are marked by D(0.05) for the Dixon's test, by G(0.05) or DG(0.05) for the Grubbs' test and by R(0.05) for the Rosner's test. Both outliers and stragglers were not included in the calculations of averages and standard deviations.

For each assigned value the uncertainty was determined in accordance with ISO13528. Subsequently the calculated uncertainty was evaluated against the respective requirement based on the target reproducibility in accordance with ISO13528. When the uncertainty passed the evaluation, no remarks are made in the report. However, when the uncertainty failed the evaluation it is mentioned in the report and it will have consequences for the evaluation of the test results.

Finally, the reproducibilities were calculated from the standard deviations by multiplying them with a factor of 2.8.

### 3.2 GRAPHICS

In order to visualize the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported test results are plotted. The corresponding laboratory numbers are on the X-axis. The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected reference test method. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle.

Furthermore, Kernel Density Graphs were made. This is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. Also a normal Gauss curve was projected over the Kernel Density Graph for reference.

### 3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements, e.g. ASTM, EN or ISO reproducibilities, the z-scores were calculated using a target standard deviation. This results in an evaluation independent of the variation of this interlaboratory study. The target standard deviation was calculated from the literature reproducibility by division with 2.8.

When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate whether the reported test result is fit-for-use.

The z-scores were calculated according to:

```
z_{\text{(target)}} = \text{(test result - average of PT)} / \text{target standard deviation}
```

The  $z_{\text{(target)}}$  scores are listed in the test result tables in appendix 1. Absolute values for z<2 are very common and absolute values for z>3 are very rare. The usual interpretation of z-scores is as follows:

```
|z| < 1 good

1 < |z| < 2 satisfactory

2 < |z| < 3 questionable

3 < |z| unsatisfactory
```

### 4 EVALUATION

In this proficiency test no severe problems were encountered with the dispatch of the samples. Not all laboratories were able to report all analyses requested. In total 45 participants reported 610 numerical test results. Observed were 28 outlying test results, which is 4.6% of the numerical test results. In proficiency studies, outlier percentages of 3% - 7.5% are quite normal.

Not all original data sets proved to have a normal Gaussian distribution. These are referred to as "not OK" or "suspect". The statistical evaluation of these data sets should be used with due care.

### 4.1 EVALUATION PER TEST

In this section, the test results are discussed per test. The test methods that are reported by the laboratories are taken into account for explaining the observed differences when possible and applicable. These test methods are also mentioned in the tables in appendix 1 together with the original data. The abbreviations used in these tables are listed in appendix 4.

Unfortunately, a suitable standard test method, providing the precision data, is not available for all determinations. For the tests, that have no available precision data, the calculated reproducibility was compared against the reproducibility from the Horwitz equation.

In the iis PT reports, test methods are referred to with a number (e.g. D2270) and an added designation for the year that the test method was adopted or revised (e.g. D2270:10). If applicable, a designation in parentheses is added to designate the year of reapproval (e.g. D2270:10(2016)). In the tables of appendix 1 only the test method number and year of adoption or revision will be used.

- <u>Acid Number (total)</u>: This determination was not problematic. No statistical outliers were observed and the calculated reproducibility is in good agreement with the requirements of ASTM D664-A:11ae1.
- <u>Copper Corrosion</u>: This determination was not problematic. Almost all participants agreed on a test result of 1 (1a), and one participant reported "nil".
- <u>Density at 15°C:</u> This determination was very problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ASTM D4052:16.
- <u>Flash Point PMcc:</u> This determination was not problematic. Three statistical outliers were observed and two test results were excluded. However, the calculated reproducibility after rejection of the suspect data is in full agreement with the requirements of ASTM D93-A:16a.
- <u>Foaming Characteristics (Tendency and Stability):</u> This determination was problematic. In total four statistical outliers were observed and three test results were excluded over 6 parameters.

The calculated reproducibility in the Foam Tendency determination for sequence I is after rejection of the suspect data almost in agreement with the requirements of ASTM D892:13e1. However, the Foam Tendency determination for sequence II is after rejection of the suspect data not in agreement with the requirements of ASTM D892:13e1. And the Foam Tendency determination for sequence III is after rejection of the suspect data not at all in agreement with the requirements of ASTM D892:13e1. Therefore no z-scores were calculated for sequence III.

For Foam stability also no z-scores were calculated. Almost all participants reported 0 ml.

This determination is very sensitive in maintenance and execution. In ASTM D892:13e1 many tips and tricks are given in the test method part X1. Possible sources for the large variation are the cleaning and checking of the air diffuser, air tubes and test cylinders, the air flow rate used during the blowing period. Therefore extra information was asked (see appendix 2), but no clear conclusion could be drawn based on this information.

- <u>Kinematic Viscosity at 40°C:</u> This determination was not problematic. Three statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in good agreement with the requirements of ASTM D445:17a.
- <u>Kinematic Viscosity at 100°C:</u> This determination was not problematic. No statistical outliers were observed and the calculated reproducibility is in good agreement with the requirements of ASTM D445:17a.
- <u>Viscosity Index</u> This determination was not problematic. No statistical outliers were observed, but three test results were excluded. However, the calculated

reproducibility after rejection of the suspect data is in full agreement with the requirements of ASTM D2270:10(2016).

- <u>Viscosity Stabinger at 40°C:</u> This determination was problematic. No statistical outliers were observed. However, the calculated reproducibility is not in agreement with the requirements of ASTM D7042:16e3.
- <u>Viscosity Stabinger at 100°C:</u> This determination was problematic. No statistical outliers were observed. However, the calculated reproducibility is not in agreement with the requirements of ASTM D7042:16e3.
- <u>Pour Point (manual):</u> This determination was not problematic. No statistical outliers were observed and the calculated reproducibility is almost in agreement with the requirements of ASTM D97:17a.
- <u>Pour Point (automated):</u> This determination was problematic. No statistical outliers were observed, but one test result was excluded. The calculated reproducibility after rejection of the suspect data is not in agreement with the requirements of ASTM D5950:14.
- Sulphur: This determination was not problematic. One statistical outlier was observed. However, the calculated reproducibility after rejection of the statistical outlier is in full agreement with the requirements of ASTM D4294:16e1.
- <u>Water content:</u> This determination was not problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D6304:16e1.
- Water Separability at 82°C: This determination was not problematic. In total six statistical outliers were observed over six parameters. However, the calculated reproducibilities for "time to reach ≤ 3ml emulsion" and "time to reach 37ml water" are both in good agreement with the requirements of ASTM D1401:12e1.
- Calcium: This determination may not be problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the estimated reproducibility using the Horwitz equation, but not at all in agreement with the strict requirements of ASTM D5185:13e1 (mean value of Calcium is identical to the lower limit of the application range).
- Phosphorus: This determination was not problematic. Three statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in good agreement with the requirements of ASTM D5185:13e1.

Zinc:

This determination was problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ASTM D5185:13e1.

### 4.2 PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES

A comparison has been made between the reproducibility as declared by the relevant reference test method and the reproducibility as found for the group of participating laboratories. The target reproducibilities derived from literature reference test methods (R (lit)) and the calculated reproducibilities (2.8 \* sd) are compared in the next table:

Parameter	unit	n	mean	2.8 * sd	R (lit)
Acid Number (total)	mg KOH/g	37	0.37	0.13	0.19
Copper Corrosion, 3 hrs at 50°C	rating	24	1	n.a.	n.a.
Density at 15°C	kg/L	39	0.8747	0.0012	0.0005
Flash Point PMcc	°C	30	237.0	16.3	16.8
Foam Tendency Seq. I	ml	13	11.5	21.7	19.3
Foam Tendency Seq. II	ml	15	18.3	23.5	16.2
Foam Tendency Seq. III	ml	14	7.9	26.7	(3.5)
Foam Stability Seq. I	ml	14	0	0	(0)
Foam Stability Seq. II	ml	16	0	0	(0)
Foam Stability Seq. III	ml	15	0	0	(0)
Kinematic viscosity at 40°C	mm²/s	32	97.843	0.811	1.194
Kinematic viscosity at 100°C	mm²/s	34	11.176	0.120	0.154
Viscosity Index		34	99.4	1.8	2
Viscosity Stabinger at 40°C	mm²/s	18	97.966	1.456	1.180
Viscosity Stabinger at 100°C	mm²/s	18	11.179	0.168	0.120
Pour Point (manual)	°C	23	-16.6	9.9	9
Pour Point (automated), 1°C int.	°C	11	-17.0	6.6	4.5
Sulphur	mg/kg	19	543	113	111
Water content (by KF)	mg/kg	30	51.9	76.6	180.6
Water Separability at 82°C, distille	ed water				
- Time ≤ 3 ml emulsion	min	14	12.3	17.1	25
- Time 37 ml water	min	14	12.4	16.9	25
- Volume Oil phase	ml	12	40.7	3.2	n.a.
- Volume Water phase	ml	13	38.5	4.7	n.a.
- Volume Emulsion phase	ml	12	0.6	3.3	n.a.
Calcium as Ca	mg/kg	27	39.7	7.4	10.2 *)
Phosphorus as P	mg/kg	27	259	46	69
Zinc as Zn	mg/kg	29	271	43	39

Table 3: reproducibilities of tests on sample #17225

<sup>\*)</sup> reproducibility via the Horwitz equation

Without further statistical calculations, it could be concluded that for many tests there is a good compliance of the group of participating laboratories with the relevant reference test methods. The problematic tests have been discussed in paragraph 4.1.

### 4.3 COMPARISON OF THE PROFICIENCY TEST OF NOVEMBER 2017 WITH THE PREVIOUS PTs.

	November 2017	November 2016	November 2015	November 2014
Number of reporting labs	45	43	45	29
Number of test results reported	610	597	569	346
Statistical outliers	28	30	26	19
Percentage outliers	4.6%	5.0%	4.6%	5.5%

Table 4: comparison with previous proficiency tests

In proficiency tests, outlier percentages of 3% - 7.5% are quite normal.

The performance of the determinations of the proficiency tests was compared against the requirements of the respective reference test methods. The conclusions are given the following table:

Determination	November 2017	November 2016	November 2015	November 2014
Acid Number (total)	+	+	++	++
Density at 15°C		+	-	+/-
Flash Point PMcc	+/-	+	+	-
Foam Tendency Seq. I	+/-	n.e.		
Foam Tendency Seq. II	-	+	+/-	
Foam Tendency Seq. III	n.e.	n.e.		
Foam Stability Seq. I	n.e.	n.e.	n.e.	n.e.
Foam Stability Seq. II	n.e.	n.e.	n.e.	n.e.
Foam Stability Seq. III	n.e.	n.e.	n.e.	n.e.
Kinematic viscosity at 40°C	+	+	+/-	+/-
Kinematic viscosity at 100°C	+	+/-	+	
Viscosity Index	+/-		+	
Viscosity Stabinger at 40°C	-	+	+	++
Viscosity Stabinger at 100°C	-	+/-	+	+
Pour Point (manual)	+/-	+/-	+/-	+
Pour Point (automated), 1°C int.	-	-	+	+
Sulphur	+/-	-	+	+
Water content (by KF)	++	++	++	++
Water Separability ≤ 3ml	+	+	++	++
Water Separability 37ml water	+	++	++	++
Calcium as Ca	+ *)	n.e.	n.e.	n.e.
Phosphorus as P	+	+	+	++
Zinc as Zn	-	-	n.e.	n.e.

Table 5: comparison determinations against the reference test methods

<sup>\*)</sup> against the Horwitz equation

++: group performed much better than the reference test method

+ : group performed better than the reference test method

+/-: group performance equals the reference test method

- : group performed worse than the reference test method

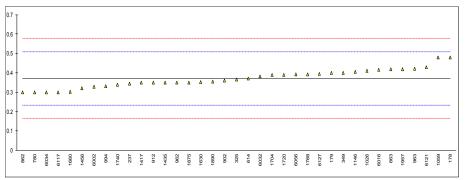
-- : group performed much worse than the reference test method

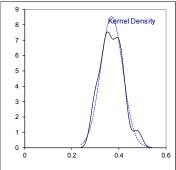
n.e.: not evaluated

# **APPENDIX 1**

Determination of Acid Number (Total) on sample #17225; results in mg KOH/g

		value	-	-	remarks
lab	method		mark	z(targ)	remarks
173	INH-1118	0.40		1.50	
178		0.48		1.58	
179 237	D664-B D664-A	0.40		0.42	
255	D004-A	0.3433		-0.40 	
325	D664-A	0.365		-0.09	
349	D664-A	0.40		0.42	
432	D004-74				
614	D664-A	0.37		-0.02	
621	200171				
663	D664-A	0.418		0.68	
780	D664-A	0.30		-1.03	
862	D664-A	0.3		-1.03	
902	D664-A	0.36		-0.16	
912	D664-A	0.35		-0.31	
962	D974	0.35		-0.31	
963	D664-A	0.42		0.71	
994	D664-A	0.3305		-0.59	
1011					
1026	D664-A	0.41		0.56	
1059	ISO6619	0.48		1.58	
1146	D664-A	0.404		0.48	
1417	D664-A	0.349		-0.32	
1435	D664-A D974	0.350		-0.31 -0.74	
1456 1630	D974	0.32 0.3533		-0.74	
1660	D374	0.333		-1.01	
1682				-1.01	
1704	D664-A	0.388		0.25	
1720	D664-A	0.39		0.27	
1740	D664-A	0.34		-0.45	
1748					
1768	ISO6618	0.3927		0.31	
1875	ISO6618	0.35		-0.31	
1890	ISO6619	0.355		-0.23	
1957	D664-A	0.418		0.68	
4043					
6002	D664-A	0.328		-0.62	
6016	D664-A	0.417		0.67	
6032	D664-A	0.3821		0.16	
6034	D664-A	0.30		-1.03	
6056	INH-5088	0.391		0.29 -1.03	
6117 6121	GB/T4945 DIN51558	0.30 0.43		0.85	
6127	D664-A	0.43		0.83	
7003	D004-A				
7000					
	normality	OK			
	n	37			
	outliers	0			
	mean (n)	0.3711			
	st.dev. (n)	0.04670			
	R(calc.)	0.1308			
	st.dev.(D664:11ae1)	0.06904			
	R(D664:11ae1)	0.1933			



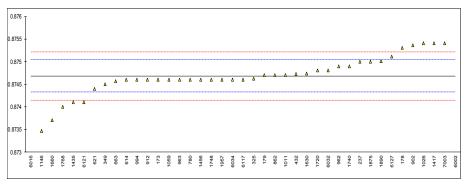


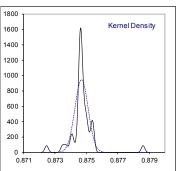
# Determination of Copper Corrosion 3hrs at 50°C on sample #17225; results in rating

lab	method	value	mark	z(targ)	remarks
173					
178					
179					
237	D130	1			
255					
325	D130	1A			
349	D130	1a			
432					
614	D130	1A			
621	D130	IA			
663	D130	1a			
780	D130	1a			
862	D130	1a			
902					
912	D130	1a			
962					
963	D130	1a			
994	D130	1a			
1011	D130	1a			
1026	D130	1A			
1059	ISO2160	1a			
1146	.=				
1417	IP154	1A			
1435	D. 400				
1456	D130	1A			
1630	D130	NIL			
1660					
1682	D400	4 -			Palet areas
1704	D130	1a			light orange
1720	D400	4.0			
1740	D130	1A			
1748 1768	D130	1a			
1875					
1890					
1957					
4043					
6002	ISO2160	1a			
6016	1002100				
6032					
6034	D130	1a			
6056					
6117	GB/T5096	1a			
6121	ISO2160	1a			
6127	D130	1a			
7003					
	n	24			
	mean (n)	1 (1a)			
	` '	` '			

# Determination of Density at 15°C on sample #17225; results in kg/L

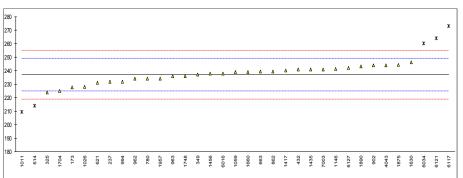
lab	method	value	mark	z(targ)	remarks
			шагк		remarks
173	D4052	0.8746	0	-0.46	first reported 0.0752 kg/m3
178	D4052	0.8753	C C	3.46	first reported 0.8753 kg/m <sup>3</sup>
179	D4052	0.8747	C	0.10	first reported 0.8747 kg/m <sup>3</sup>
237	D4052	0.8750		1.78	
255	D4050	0.07400		0.05	
325	D4052	0.87462		-0.35	
349	D4052	0.8745		-1.02	
432	D4052	0.87472		0.21	
614	D4052	0.8746		-0.46	
621	D4052	0.8744		-1.58	
663	D4052	0.87457		-0.63	
780	D4052	0.8746		-0.46	
862	D4052	0.8747		0.10	
902	D4052	0.87536		3.80	
912	D4052	0.8746		-0.46	
962	D4052	0.8749		1.22	
963	D4052	0.8746		-0.46	
994	D4052	0.8746		-0.46	
1011	D4052	0.8747		0.10	
1026	D4052	0.8754		4.02	
1059	D4052	0.8746		-0.46	
1146	D4052	0.87347		-6.79	
1417	IP365	0.8754		4.02	
1435	D4052	0.8741		-3.26	
1456	D4052	0.8746		-0.46	
1630	D4052	0.87474	С	0.32	first reported 0.87142 kg/m <sup>3</sup>
1660	D7042	0.8737		-5.50	
1682					
1704					
1720	D4052	0.8748		0.66	
1740	D4052	0.8749		1.22	
1748	D4052	0.8746		-0.46	
1768	ISO3675	0.8740		-3.82	
1875	D7042	0.8750		1.78	
1890	ISO12185	0.87501		1.84	
1957	D4052	0.8746		-0.46	
4043					
6002	ISO3675	0.8786	C,R(0.01)	21.94	first reported 876.8 kg/m <sup>3</sup>
6016	D4052	0.87246	R(0.01)	-12.44	
6032	D4052	0.8748		0.66	
6034	D4052	0.8746	U	-0.46	reported 0.8746 kg/m <sup>3</sup>
6056					
6117	SH/T0604	0.8746		-0.46	
6121	ISO12185	0.8741		-3.26	
6127	D4052	0.87511		2.40	
7003	D4052	0.8754		4.02	
	normality	suspect			
	n	39			
	outliers	2			
	mean (n)	0.87468			
	st.dev. (n)	0.000423			
	R(calc.)	0.00118			
	st.dev.(D4052:16)	0.000179			
	R(D4052:16)	0.00050			
	•				

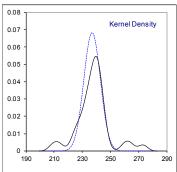




# Determination of Flash Point PMcc on sample #17225; results in °C

lab	method	value	mark	z(targ)	remarks
173	D93-A	227.5		-1.59	
178					
179					
237	D93-B	232.0		-0.84	
255					
325	D93-A	224		-2.17	
349	D93-A	237		0.00	
432	D93-A	241.0		0.66	
614	D93-A	214	R(0.05)	-3.83	
621	D93-A	231	С	-1.00	first reported 213.0
663	D93-A	239.4		0.39	
780	D93-A	234.0		-0.50	
862	D93-A	239.5		0.41	
902	D93-A	244.0		1.16	
912					
962	D93-A	234		-0.50	
963	D93-A	236.0		-0.17	
994	D93-A	232.0		-0.84	
1011	D93-A	209.5	C,R(0.05)	-4.58	first reported 197.5
1026	D93-A	228.0		-1.50	
1059	ISO2719-A	239.0		0.33	
1146	D93-A	241.1		0.68	
1417	D93-A	240		0.49	
1435	D93-A	241.0		0.66	
1456	D93-A	238.0		0.16	
1630	D93-A	246		1.49	
1660	D93-A	239		0.33	
1682	D00 4		0		fact are and all 040
1704	D93-A	225	С	-2.00 	first reported 213
1720			147		first reported 017
1740 1748	D93-A	236	W	-0.17	first reported 217
1748	D93-A	230		-0.17	
1875	ISO2719-A	244.3		1.21	
1890	ISO2719-A	243		0.99	
1957	D93-A	234.0		-0.50	
4043	ISO15267	244.0000		1.16	
6002	10010207				
6016	D93-A	238		0.16	
6032	200 A				
6034	D93-A	260	R(0.05)	3.82	
6056	2007.		(0.00)		
6117	GB/T3536	273	ex	5.99	excluded: open cup method is not equivalent to Flash Point PMcc
6121	ISO2592	264	ex	4.49	excluded: open cup method is not equivalent to Flash Point PMcc
6127	D93-A	242		0.83	
7003	D93-B	241.0		0.66	
	normality	OK			
	n	30			
	outliers	3 (+2 ex)			
	mean (n)	237.03			
	st.dev. (n)	5.838			
	R(calc.)	16.35			
	st.dev.(D93-A:16a)	6.010			
	R(D93-A:16a)	16.83			





Determination of Foaming Characteristics, Foaming Tendency (at end of 5 min blowing period) on

sample #17225; results in ml

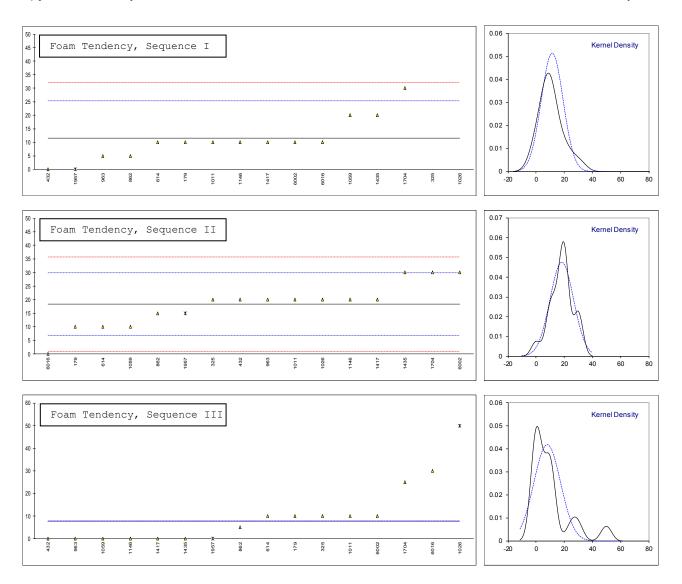
178	lab	method	Seq. I	mark	z(targ)	Seq. II	mark	z(targ)	Seq. III	mark	z(targ)
178					(•• g)						
179											
235		D892			-0.22			-1.44			
325   D892   200 °)   C,G(0.01)   27.35   20   0.29   10 °)   C	237										
349	255										
432   D892   0		D892	200 *)	C,G(0.01)	27.35	20		0.29	10 *)	С	
614   D892   10		5000									
683											
Rec   D892   5		D092						-1.44			
Rec   Despt   S											
886   D892   5											
902		D892						-0.58			
962	902	2002									
963 D892 5 -0.95 20 0.29 0											
983											
1016   D892   350   G(0.01)   49.11   20   0.29   50   G(0.05)		D892	5		-0.95	20		0.29	0		
1059   D892   350   G(0.01)   49.11   20   0.29   50   G(0.05)											
1059 D892				0/0.04				0.29		O (O O = )	
1146				G(0.01)	49.11			0.29		G(0.05)	
1417 D892 10 -0.22 20 0.29 0					1.23 -0.22			-1. <del>44</del>			
1435     ISO6247     20     1.23     30     2.02     0       1680           1660           1704     D892     30     2.68     30 *)     C     2.02     25       1740            1740     1748     D892          1768           1875           1890           1957     0     ex **)     -1.67     15     ex **)     -0.58     0     ex **)       4043     8002     10     -0.22     30     2.02     10       8002     15     ex **)     -0.58     0     ex **)        6016     D892     10     -0.22     30     2.02     10        6034             6117            6121					-0.22			0.29			
1456   1630					1.23			2.02			
1660											
1682   1704   D892   30	1630										
1704 D892 30 2.68 30 *) C 2.02 25	1660										
1720 1740 1748 1768 1875 1875 1890 1957 0 ex **) -1.67 15 ex **) -0.58 0 ex **) 6002 18O6247 10 0 -0.22 0 0 -3.17 30 6032 6034 6056 6117 6121 6127 7003  normality n not OK n normality n not OK n normality n not OK n 13 0											
1740 1748 D892		D892	30		2.68	30 *)	С	2.02	25		
1748 D892   <											
1768		D000									
1875		D892									
1890											
1957   0 ex **) -1.67   15 ex **) -0.58   0 ex **)											
4043				ov **)	1.67	15	ov **)	0.59	0	ov **)	
6002   ISO6247   D892       10       -0.22   0       -3.17   30          6032   Color   D892   D892				<del>6</del> x )	-1.07	15	ex )	-0.56		ex )	
6016 D892		ISO6247			-0.22	30		2.02			
6032					-0.22			-3.17			
6056											
6117	6034										
6121	6056										
6121											
7003											
7003	6127										
n   13   15   14   14 ex)   15   1 (+1 ex)											
n   13   15   14   14 ex)   15   1 (+1 ex)			,								
outliers 2 (+1 ex) 0 (+1 ex) 1 (+1 ex)		lity									
		c									
mean m 111.04 1.10.33 17.86			11.54			18.33			7.86		
st.dev. (n) 7.7418 8.3808 9.550											
R(calc.) 21.68 23.47 26.74	R(calc	:.) ´									
st.dev.(D892:13e1)   6.891   5.788   (1.235)	st.dev.	(D892:13e1)	6.891						(1.235)		
R(D892:13e1)   19.30   16.21   (3.46)	R(D89	2:13e1)	19.30			16.21			(3.46)		

\*)

Lab 325 first reported 460,320 Lab 1704 first reported 60

\*\*)

Lab 1957 excluded: Gas diffuser was not cleansed (see appendix 2)

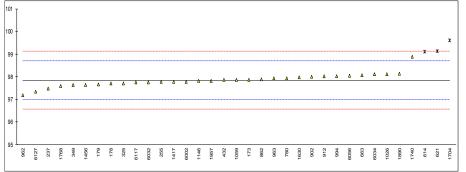


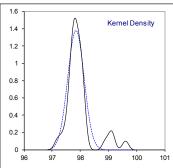
# Determination of Foaming Characteristics, Foaming Stability (at end of 10 min settling period) on sample #17225; results in ml

lab	method	Seq. I	mark	z(targ)	Seq. II	mark	z(targ)	Seq. III	mark	z(targ)
173										
178										
179	D892	Nil			0			Nil		
237 255										
325	D892	0			0			0		
349	D092									
432	D892	0			0			0		
614	D892	0			0			0		
621										
663										
780										
862	D892	0			0			0		
902										
912 962										
963	D892	0			0			0		
994	D092									
1011	D892	0			0			0		
1026	D892	20	G(0.01), false positive?		0			Ö		
1059	D892	0	, ,,		0			0		
1146	D892	0			0			0		
1417	D892	0			0			0		
1435	ISO6247	0			0			0		
1456										
1630										
1660 1682										
1704	D892	0			0			0		
1720	5002									
1740										
1748										
1768										
1875										
1890										
1957 4043		0			0			0		
6002	ISO6247	0			0			0		
6016	D892	0			0			0		
6032	2002									
6034										
6056										
6117										
6121										
6127										
7003	I									
normal	ity	n.a.			n.a.			n a		
normal n	ity	11.a. 14			11.a. 16			n.a. 15		
outliers	<b>S</b>	1			0			0		
mean (		Ö			0			0		
st.dev.		0			0			0		
R(calc.	.)	0			0			0		
st.dev.	(D892:13e1)	(0)			(0)			(0)		
K(D89)	2:13e1)	(0)			(0)			(0)		

# Determination of Kinematic Viscosity at 40°C on sample #17225; results in mm<sup>2</sup>/s

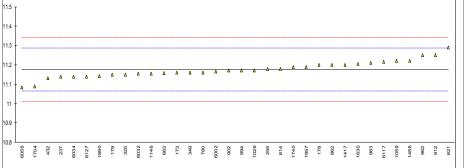
lab	method	value	mark	z(targ)	remarks
173	D445	97.86		0.04	
178	D445	97.7		-0.34	
179	D445	97.66		-0.43	
237	D445	97.48		-0.85	
255		97.76		-0.19	method used: D7279 corrected to D445
325	D445	97.71		-0.31	
349	D445	97.63		-0.50	
432	D445	97.85		0.02	
614	D445	99.10	R(0.01)	2.95	
621	D445	99.12	C,R(0.01)	3.00	first reported 96.41
663	D445	98.062	, ,	0.51	
780	D445	97.92		0.18	
862	D445	97.89		0.11	
902	D445	98.00		0.37	
912	D445	98.01		0.39	
962	D445	97.18		-1.56	
963	D445	97.92		0.18	
994	D445	98.01		0.39	
1011					
1026	D445	98.12	С	0.65	first reported 33.98
1059	ISO3104	97.85		0.02	
1146	D445	97.807		-0.08	
1417	D445	97.76		-0.19	
1435					
1456	D445	97.63		-0.50	
1630	D445	97.9723		0.30	
1660					
1682					
1704	D445	99.60	C,R(0.01)	4.12	first reported 96.302
1720					
1740	D445	98.89		2.46	
1748	1000404			0.50	
1768	ISO3104	97.59		-0.59	
1875	1002104	00 121		0.60	
1890	ISO3104	98.131		0.68	
1957 4043	D445	97.82 		-0.05 	
6002	ISO3104	97.77		-0.17	
6016	1303104	97.77		-0.17	
6032		97.755		-0.21	method used: D7279 corrected to D445
6034	D445	98.10		0.60	method dsed. D1219 confected to D443
6056	D445	98.047		0.48	
6117	GB/T265	97.745		-0.23	
6121	OD/1203			-0.20	
6127	D445	97.35		-1.16	
7003	20				
	normality	not OK			
	n	32			
	outliers	3			
	mean (n)	97.8431			
	st.dev. (n)	0.28972			
	R(calc.)	0.8112			
	st.dev.(D445:17a)	0.42632			
	R(D445:17a)	1.1937			

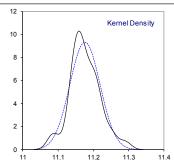




# Determination of Kinematic Viscosity at 100°C on sample #17225; results in mm<sup>2</sup>/s

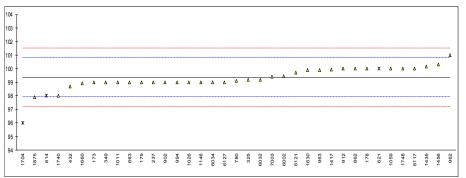
lab	method	value	mark	z(targ)	remarks
173	D445	11.16		-0.29	
178	D445	11.20		0.44	
179	D445	11.15		-0.47	
237	D445	11.14		-0.65	
255		11.18		0.07	method used: D7279 corrected to D445
325	D445	11.15		-0.47	
349	D445	11.16		-0.29	
432	D445	11.13		-0.84	
614	D445	11.18		0.07	
621	D445	11.29		2.07	
663	D445	11.158		-0.33	
780	D445	11.16		-0.29	
862	D445	11.20		0.44	
902	D445	11.17		-0.11	
912	D445	11.25		1.34	
962	D445	11.25		1.34	
963	D445	11.21		0.62	
994	D445	11.17		-0.11	
1011	-				
1026	D445	11.17	С	-0.11	first reported 9.18
1059	ISO3104	11.22		0.80	
1146	D445	11.154		-0.40	
1417	D445	11.20		0.44	
1435	5110				
1456	D445	11.22		0.80	
1630	D445	11.2052		0.53	
1660	D+10				
1682					
1704	D445	11.089		-1.58	
1720	5110				
1740	D445	11.19		0.25	
1748	5110				
1768					
1875					
1890	ISO3104	11.141		-0.64	
1957	D445	11.19		0.25	
4043	5110				
6002	ISO3104	11.165		-0.20	
6016	1000101				
6032		11.1538		-0.40	method used: D7279 corrected to D445
6034	D445	11.14		-0.65	
6056	D445	11.084		-1.67	
6117	GB/T265	11.215		0.71	
6121	05/1200				
6127	D445	11.14		-0.65	
7003	5110				
, 500					
	normality	OK			
	n	34			
	outliers	0			
	mean (n)	11.1760			
	st.dev. (n)	0.04279			
	R(calc.)	0.1198			
	st.dev.(D445:17a)	0.05508			
	R(D445:17a)	0.05500			
	. (Β++υ. 17α)	J. 10-12			

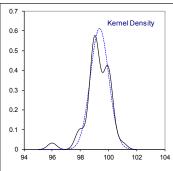




# Determination of Viscosity Index on sample #17225; unit less results

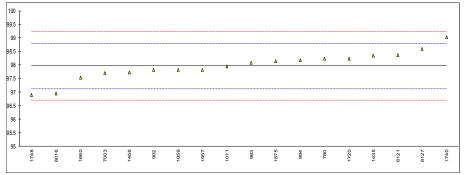
lab	method	value	mark	z(targ)	iis calc.	mark	remarks
173	D2270	99		-0.53	99.19		
178	D2270	100		0.87	100.01		
179	D2270	99		-0.53	99.28		
237	D2270	99		-0.53	99.35		
255					99.63		
325	D2270	99.2		-0.25	99.22		
349	D2270	99		-0.53	99.48		
432	D2270	98.7		-0.95	98.73		
614	D2270	98	ex	-1.93	97.98	ex	outlier in viscosity 40 °C
621	D2270	100	C,ex	0.87	99.56	ex	first reported 103, outlier in viscosity 40 °C
663	D2270	99		-0.53	98.91		
780	D2270	99.1		-0.39	99.12		
862	D2270	100		0.87	99.78		
902	D2270	99		-0.53	99.18		
912 962	D2270 D2270	100 101		0.87 2.27	100.38 101.52		
962	D2270 D2270	99.9		0.73	99.89		
994	D2270	99.9		-0.53	99.17		
1011	D2270	99		-0.53			
1026	D2270 D2270	99	С	-0.53	99.03		first reported 270
1059	ISO2909	100	O	0.87	100.13		mot reported 270
1146	D2270	99		-0.53	99.16		
1417	D2270	99.94		0.79	99.94		
1435	D2270	100.17		1.11			
1456	D2270	100.316		1.32	100.43		
1630	D2270	99.8852		0.71	99.75		
1660	D2270	98.9		-0.67			
1682							
1704	D2270	96	C,ex	-4.73	95.89	ex	first reported 100.16, outlier in viscosity 40 °C
1720							
1740	D2270	98		-1.93	98.40		
1748	D2270	100		0.87	99.77		VI based on Stabinger results
1768	1000000	07.0		2.07	07.55		VI beard on Otahinnan masulta
1875 1890	ISO2909	97.9		-2.07	97.55 98.56		VI based on Stabinger results
1957					99.71		
4043					99.71		
6002	ISO2909	99.46		0.12	99.38		
6016	1002303						
6032	D2270	99.2		-0.25	99.23		
6034	D2270	99		-0.53	98.58		
6056					97.75		
6117	GB/T1995	100		0.87	100.19		
6121	ISO2909	99.7		0.45	99.49		
6127	D2270	99		-0.53	99.51		
7003	D7042	99.4		0.03	99.48		VI based on Stabinger results
		011			iis calculate	<u>ed</u>	
	normality	OK			suspect		
	n outliere	34			35		
	outliers	0 (+3 ex) 99.38			0 (+3 ex)		
	mean (n) st.dev. (n)	99.38 0.652			99.40 0.745		
	R(calc.)	1.83			2.09		
	st.dev.(D2270:10)	0.714			0.714		
	R(D2270:10)	2			2		
	(	-			-		

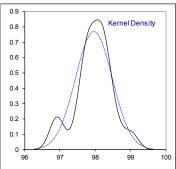




# Determination of Viscosity Stabinger at 40°C on sample #17225; results in mm<sup>2</sup>/s

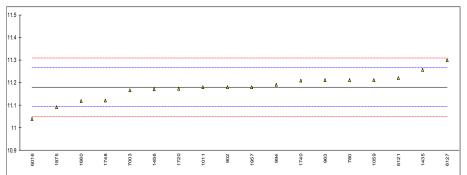
lab	method	value	mark	z(targ)	remarks
173					
178					
179					
237					
255					
325 349					
432					
614					
621					
663					
780	D7042	98.23		0.63	
862					
902	D7042	97.82		-0.35	
912					
962	D70.40				
963	D7042	98.08		0.27	
994 1011	D7042	98.17 97.95		0.48 -0.04	
1011	D7042	97.95		-0.04	
1059	D7042	97.82		-0.35	
1146	51012				
1417					
1435	D7042	98.34		0.89	
1456	D7042	97.72		-0.58	
1630					
1660	D7042	97.531		-1.03	
1682					
1704	D7042	09.24	C	0.65	first reported 00 52
1720 1740	D7042 D7042	98.24 99.02	С	2.50	first reported 99.52
1748	D7042	96.90		-2.53	
1768	51012				
1875	D7042	98.133		0.40	
1890					
1957	D7042	97.82		-0.35	
4043					
6002	D=0.40				
6016	D7042	96.947		-2.42	
6032					
6034 6056					
6117					
6121	DIN51659-2	98.36		0.94	
6127	D7042	98.60		1.51	
7003	D7042	97.7		-0.63	
	normality	OK			
	n	18			
	outliers	0			
	mean (n)	97.9656			
	st.dev. (n)	0.51988			
	R(calc.) st.dev.(D7042:16e3)	1.4557 0.42147			
	R(D7042:16e3)	1.1801			
	11(010-12.1000)	1.1001			

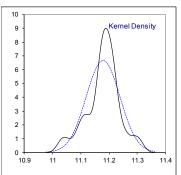




# Determination of Viscosity Stabinger at 100°C on sample #17225; results in mm<sup>2</sup>/s

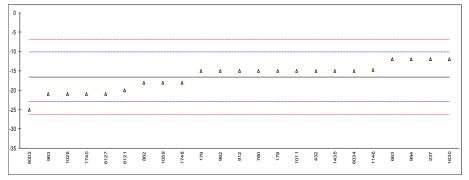
lab	method	value	mark	z(tara)	romarks
	metriou	value	mark	z(targ)	remarks
173					
178					
179					
237					
255					
325					
349					
432					
614					
621					
663					
780	D7042	11.21		0.72	
862					
902	D7042	11.18		0.02	
912					
962					
963	D7042	11.21		0.72	
994	D7042	11.19		0.26	
1011	D7042	11.18		0.02	
1026					
1059	D7042	11.21		0.72	
1146					
1417					
1435	D7042	11.256		1.79	
1456	D7042	11.17		-0.21	
1630					
1660	D7042	11.117		-1.44	
1682					
1704					
1720	D7042	11.173	С	-0.14	first reported 11.62
1740	D7042	11.209	· ·	0.70	
1748	D7042	11.121		-1.35	
1768	5.012				
1875	D7042	11.091		-2.05	
1890	5.012				
1957	D7042	11.18		0.02	
4043	57042				
6002					
6016	D7042	11.039		-3.26	
6032	D1072			5.20	
6034					
6056					
6117					
	DIN51659-2	11.22		0.95	
6121 6127		11.22			
	D7042			2.82	
7003	D7042	11.166		-0.30	
	normality	auanast			
	normality	suspect			
	n	18			
	outliers	0			
	mean (n)	11.1790			
	st.dev. (n)	0.05990			
	R(calc.)	0.1677			
	st.dev.(D7042:16e3)	0.04295			
	R(D7042:16e3)	0.1203			

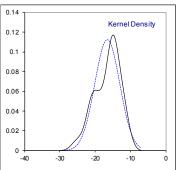




# Determination of Pour Point, manual on sample #17225; results in °C

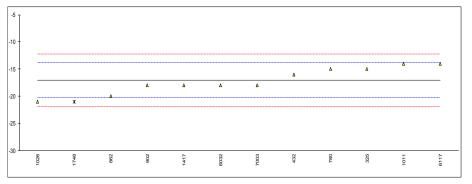
lab	method	value	mark	z(targ)	remarks
173					
178	D97	-15		0.48	
179	D97	-15		0.48	
237	D97	-12		1.42	
255					
325					
349					
432	D97	-15		0.48	
614					
621					
663	D97	-12		1.42	
780	D97	-15		0.48	
862	D97	-18		-0.45	
902					
912	D97	-15		0.48	
962	D97	-15		0.48	
963	D97	-21		-1.38	
994	D97	-12		1.42	
1011	D97	-15		0.48	
1026	D97	-21		-1.38	
1059	ISO3016	-18		-0.45	
1146	D97	-14.8		0.55	
1417	201				
1435	ISO3016	-15		0.48	
1456	1000010				
1630	D97	-12		1.42	
1660	20.				
1682					
1704					
1720					
1740	D97	-21		-1.38	
1748	D97	-18		-0.45	
1768	20.				
1875					
1890					
1957					
4043					
6002	ISO3016	-25		-2.63	
6016					
6032					
6034	D97	-15		0.48	
6056					
6117					
6121	In house	-20		-1.07	
6127	D97	-21		-1.38	
7003					
	normality	OK			
	n	23			
	outliers	0			
	mean (n)	-16.56			
	st.dev. (n)	3.544			
	R(calc.)	9.92			
	st.dev.(D97:17a)	3.214			
	R(D97:17a)	9			

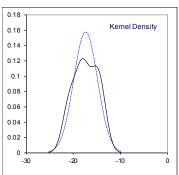




# Determination of Pour Point, automated, 1°C interval on sample #17225; results in °C

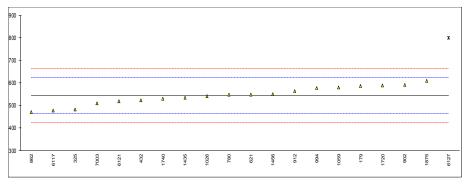
lab	method	value	mark	z(targ)	remarks
173	memou		HIGHN	2(tary)	TOTHIGHT
173					
179					
237					
255					
325	D5950	-15		1.24	
349					
432	D5950	-16		0.62	
614					
621					
663					
780	D5950	-15		1.24	
862	D5950	-20		-1.87	
902	D5950	-18		-0.62	
912					
962					
963					
994					
1011	D6892	-14		1.87	
1026	D5950	-21		-2.49	
1059					
1146	DECEC	 -18		-0.62	
1417 1435	D5950	-10		-0.02	
1456					
1630					
1660					
1682					
1704					
1720					
1740					
1748	D7346	-21	ex	-2.49	excluded: 3 °C interval
1768					
1875					
1890					
1957					
4043					
6002					
6016	D07				
6032	D97	-18		-0.62	
6034					
6056	NB/SH/T0886	 -14		1.87	
6117 6121	ND/3H/10000	- 14		1.07	
6127					
7003	D5950	-18		-0.62	
7000	D0000	-10		-0.02	
	normality	OK			
	n	11			
	outliers	0 (+1 ex)			
	mean (n)	-17.00			
	st.dev. (n)	2.366			
	R(calc.)	6.63			
	st.dev.(D5950:14)	1.607			
	R(D5950:14)	4.5			

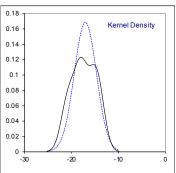




# Determination of Sulphur on sample #17225; results in mg/kg

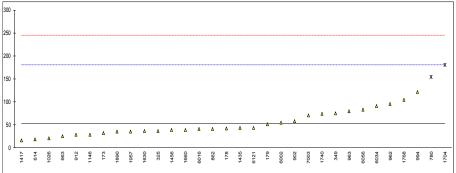
lab	method	value	mark	z(targ)	remarks
173					
178					
179	D4294	586		1.08	
237					
255					
325	D5185	482		-1.54	
349					
432	D5185	523.7		-0.49	
614					
621	D4294	548		0.12	
663	D. 100.1				
780	D4294	547		0.09	
862	D2622	471		-1.82	
902	D4294	590		1.18	
912	D4294	564		0.52	
962					
963 994	D4294	 578		0.87	
1011	D4294			0.07	
1011	D2622	540		-0.08	
1059	ISO14596Mod.	580		0.92	
1146	130 14330W0d.				
1417					
1435	D5185	533		-0.26	
1456	D5185	549		0.14	
1630	20.00				
1660	D4294	<50		<-12.43	possibly a false negative test result?
1682					, ,
1704					
1720	D4294	588		1.13	
1740	D4294	530		-0.33	
1748					
1768					
1875	DIN51724	609		1.66	
1890					
1957					
4043					
6002					
6016					
6032 6034					
6056					
6117	SH/T0689	477		-1.67	
6121	In house	519		-0.61	
6127	D5185	800	R(0.01)	6.47	
7003	D5453	507.9	14(0.01)	-0.89	
1000	20100	007.0		0.00	
	normality	OK			
	n	19			
	outliers	1			
	mean (n)	543.29			
	st.dev. (n)	40.324			
	R(calc.)	112.91			
	st.dev.(D4294:16e1)	39.695			
	R(D4294:16e1)	111.15			

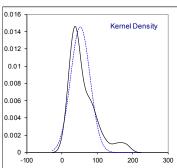




# Determination of Water Content by KF on sample #17225; results in mg/kg

lah	mothod	value	mark	z(tora)	romarke
lab	method Degrad C		mark	z(targ)	remarks
173	D6304-C	32		-0.31	
178	D6304-C	42		-0.15	
179	D6304-C	51		-0.01	
237					
255	D0004.0				
325	D6304-C	36.5		-0.24	
349	D6304-A	75		0.36	
432					
614	D6304-A	18		-0.53	
621					
663	D6304-C	25.4		-0.41	
780	D6304-A	154	R(0.05)	1.58	
862	D6304-C	41		-0.17	
902	D6304-A	57.9		0.09	
912	D6304-C	28		-0.37	
962	D6304-A	95		0.67	
963	D6304-A	79		0.42	
994	D6304-A	122		1.09	
1011					
1026	D6304-C	21		-0.48	
1059					
1146	D6304-C	28		-0.37	
1417	D6304-A	16		-0.56	
1435	D6304-A	43		-0.14	
1456	D6304-A	39	С	-0.20	first reported <10
1630	ISO13567	36.28		-0.24	<b>'</b>
1660	IEC60814	39		-0.20	
1682					
1704	D6304-A	180	R(0.05)	1.99	
1720			(/		
1740	D6304-C	74		0.34	
1748					
1768	ISO3733	105		0.82	
1875					
1890	EN60814	35.0		-0.26	
1957	D6304-A	35.2		-0.26	
4043	2000.71				
6002	D6304-C	55.02		0.05	
6016	D6304-A	40.7		-0.17	
6032	_ 500 1 / 1			-0.17	
6034	D6304-A	90.57		0.60	
6056	ISO12937	83		0.48	
6117	GB/T260				reported: trace %M/M
6121	DIN51777	43		-0.14	Toportoa. If add 7010//101
6127	ווווטוווו	43		-0.14	
7003	E1064	70			
1003	E1064	70		0.28	
	normality	OK			
	-	30			
	n outliere				
	outliers	2			
	mean (n)	51.886			
	st.dev. (n)	27.3528			
	R(calc.)	76.588			
	st.dev.(D6304:16e1)	64.4976			
	R(D6304:16e1)	180.593			





Determination of Water Separability at 82 °C, distilled water on sample #17225; results in min.

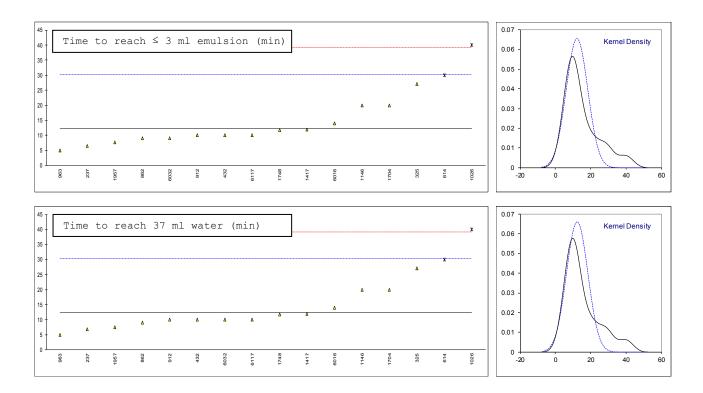
lab	method	≤3 ml emul.	mark	z(targ)	37 ml water	mark	z(targ)	compl. break	mark	z(targ)	aborted	time aborted
173												
178												
179	D4404							10			NO	
237 255	D1401	6.498		-0.65	6.78		-0.63	10.282			NO 	
325	D1401	27		1.65	27		1.64				YES	27
349	51101											
432	D1401	10		-0.26	10		-0.26	>60			YES	60
614	D1401	30	DG(0.05)	1.98	30	DG(0.05)	1.98				YES	
621												
663 780												
862	D1401	9		-0.37	9		-0.38	10			NO	
902												
912	D1401	10		-0.26	10		-0.26				NO	
962	54464											
963 994	D1401	5		-0.82	5		-0.82	6			NO	
1011								20			NO	20
1026	D1401	40 *)	C,DG(0.05)	3.10	40 *)	C,DG(0.05)	3.10	45			NO	
1059			-, -(,			-, -(,						
1146	D1401	20		0.86	20		0.86					
1417	D1401	12		-0.03	12		-0.04	12			NO	
1435 1456												
1630												
1660												
1682												
1704		20		0.86	20		0.86	20			NO	
1720												
1740					 11.7							
1748		11.75		-0.06	5		-0.07	16			NO	
1768												
1875												
1890	D4404	7.07		0.50	7.50		0.50	45.04				
1957 4043	D1401	7.67		-0.52 	7.59 		-0.53 	15.34				
6002	ISO6614	>60	false positive?	>5.34	>60	false positive?		>60			YES	60
6016	D1401	14		0.19	14	,	0.18	>30			YES	30 **)
6032	D1401	9		-0.37	10		-0.26	10			NO	
6034												
6056	CD/T7205	10		0.26	10		0.26	10				
6117 6121	GB/T7305	10		-0.26 	10		-0.26 	10				
6127												
7003												
normal	itv	not OK			not OK		ı					
n	ity	14			14	•						
outliers	3	2			2							
mean (		12.28			12.37							
st.dev.		6.102			6.050							
R(calc.	.) (D1401:12e1)	17.08 8.929			16.94 8.929							
	01:12e1)	25			25							
11(2)140		~					ļ					

\*)

Lab 1026 first reported 45, 45

\*\*)

Lab 6016 reported that the test has been aborted at 30 min. ASTM method D1401 describes that the test may be aborted after 60 min when testing at 82  $^{\circ}$ C



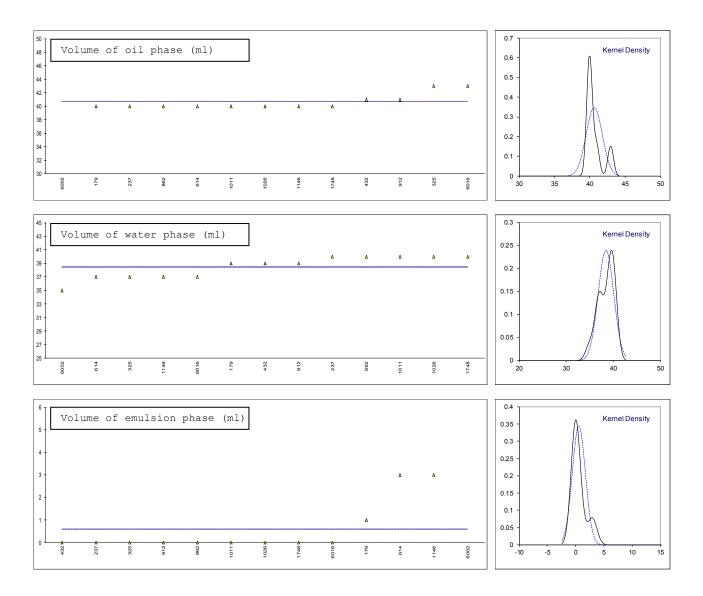
Determination of Water Separability at 82 °C, distilled water on sample #17225; results in ml.

### --- Continued ----

lab	ntinued	oil	mark	z(targ)	water	mark	z(targ)	emulsion	mark	z(targ)	aborted	time
lab	memou	Oii	IIIaik	Z(tary)	water	IIIaik	Z(tary)	emuision	IIIaik	Z(tary)	aborteu	aborted
173												
178												
179	D1401	40			39 40			1 0			NO	
237 255	D1401	40			40						NO 	
325	D1401	43			37			0			YES	27
349 432	D1401	41			39			0			YES	60
614	D1401	40			37			3			YES	
621												
663												
780	D4404											
862 902	D1401	40			40			0			NO 	
912	D1401	41			39			0			NO	
962	5											
963 994	D1401										NO 	
1011		40			40			0			NO	20
1026	D1401	40			40			0			NO	
1059	D4404											
1146 1417	D1401 D1401	40			37			3			NO	
1435	B1401											
1456												
1630												
1660												
1682											NO.	
1704 1720											NO 	
1740												
1748		40			40			0			NO	
1768												
1875												
1890	5											
1957 4043	D1401											
6002	ISO6614	5 *)	G(0.01)		35			40 *)	G(0.01)		YES	60
6016	D1401	43			37			0			YES	30
6032 6034	D1401										NO	
6056												
6117	GB/T7305											
6121												
6127												
7003												
norma	lity	not OK			OK			not OK				
n	-	12			13			12				
outliers mean (		1 40.67			0 38.46			1 0.58				
st.dev.		1.155			1.664			1.165				
R(calc	.)	3.23			4.66			3.26				
st.dev. R(targe	(target)	n.a. n.a.			n.a. n.a.			n.a. n.a.				
i tital ge	,	,a.			, 11.u.		ı	u.			l	

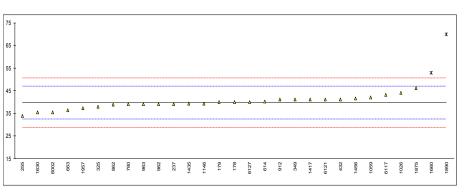
\*)

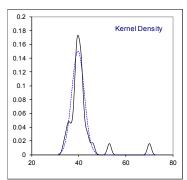
Lab 6002 probably mixed up the test results for volume of oil phase and the test results of volume of emulsion phase



# Determination of Calcium (Ca) on sample #17225; results in mg/kg.

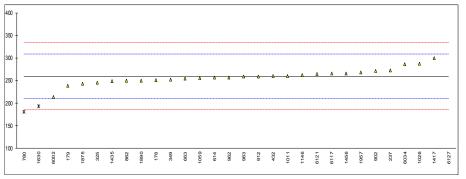
lab	method	value	mark	z(targ)	remarks
173			man	<u> </u>	
178	D5185	40		0.08	
179	D5185	40		0.08	
237	20.00	39.12	С	-0.16	first reported 33.80
255	INH-OL1	33.91	Ċ	-1.59	first reported 31.4
325	D5185	38		-0.47	
349		41		0.36	
432	D4951	41.1		0.38	
614	D5185	40.2		0.14	
621					
663	D5185	36.35		-0.92	
780	D5185	39		-0.19	
862	D5185	38.8		-0.25	
902					
912	D5185	41		0.36	
962		39		-0.19	
963	D5185	39.0		-0.19	
994					
1011					
1026	D5185	44		1.18	
1059	In house	42		0.63	
1146	In house	39.31		-0.11	
1417	D5185	41		0.36	
1435		39.26		-0.12	
1456	D5185	41.6		0.52	#
1630	D5185	35.38	C	-1.18	first reported 25.68
1660	D5185	53	R(0.01)	3.64	
1682					
1704					
1720					
1740					
1748 1768					
1875	DIN51460-1	46		1.73	
1890	In house	70	R(0.01)	8.30	
1957	D5185	37.20	11(0.01)	-0.68	
4043	D3103			-0.00	
6002	D6595	35.42		-1.17	
6016	20000				
6032					
6034					
6056					
6117	GB/T17476	43.19		0.96	
6121	DIN51777	41		0.36	
6127	D5185	40		0.08	
7003					
	normality	OK			
	n	27			
	outliers	2			
	mean (n)	39.698			
	st.dev. (n)	2.6481			
	R(calc.)	7.415			
	st.dev.(Horwitz)	3.6496			D/DE40E 40 4) 4 000 / " " " 10 0000 " "
	R(Horwitz)	10.219			compare R(D5185:13e1) = 1.808 (application range 40-9000 mg/kg)

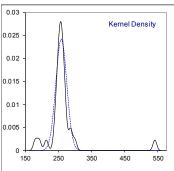




# Determination of Phosphorus (P) on sample #17225; results in mg/kg.

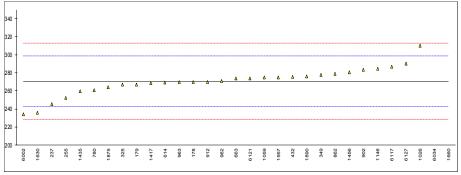
lab	method	value	mark	z(targ)	remarks
173					
178	D5185	251		-0.33	
179	D5185	239		-0.82	
237		272.3	С	0.53	first reported 29.31
255					
325	D5185	245		-0.57	
349		252		-0.29	
432	D4951	259.6		0.02	
614	D5185	256.2		-0.12	
621	D=10=				
663	D5185	254.8	D(0.05)	-0.18	
780	D5185	181	R(0.05)	-3.16	
862 902	D5185	250		-0.37 0.48	
912	D5185	271.0		-0.01	
962	D5185	259 257		-0.01	
963	D5185	258.5		-0.03	
994	D3103			-0.03	
1011	D5185	260		0.03	
1026	D5185	287		1.13	
1059	In house	256		-0.13	
1146	In house	262.3		0.13	
1417	D5185	300		1.65	
1435		248.2		-0.44	
1456	D5185	266.2		0.29	
1630	D5185	192.93	R(0.05)	-2.68	
1660					
1682					
1704					
1720					
1740					
1748					
1768	DINE 1460 1	242		0.65	
1875 1890	DIN51460-1 In house	243 250		-0.65 -0.37	
1957	D5185	267.9		0.35	
4043	D3103				
6002	D6595	214.03		-1.83	
6016	20000				
6032					
6034	D5185	286.29		1.10	
6056					
6117	GB/T17476	265.8		0.27	
6121	DIN51777	265		0.24	
6127	D5185	540	R(0.01)	11.36	
7003					
	***	. 01.			
	normality	not OK			
	n	27			
	outliers	3 259.153			
	mean (n) st.dev. (n)	16.4787			
	R(calc.)	46.140			
	st.dev.(D5185:13e1)	24.7223			
	R(D5185:13e1)	69.222			
	,				

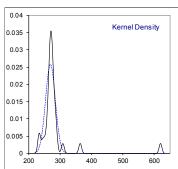




# Determination of Zinc (Zn) on sample #17225; results in mg/kg.

lab	method	value	mark	z(targ)	remarks
173	5-40-				
178	D5185	270		-0.04	
179 237	D5185	267 245.5		-0.25 -1.78	
257 255	INH-OL1	252		-1.76	
325	D5185	267		-0.25	
349	20100	278		0.53	
432	D4951	275.6		0.36	
614	D5185	269.2		-0.10	
621					
663	D5185	273.7		0.22	
780	D5185	261		-0.68	
862	D5185	279		0.60	
902	D5185	283.5		0.92	
912 962	D5185	270 271		-0.04 0.03	
963	D5185	269.7		-0.06	
994	D3103			-0.00	
1011					
1026	D5185	310		2.81	
1059	In house	275		0.32	
1146	In house	284.8		1.01	
1417	D5185	268.5		-0.15	
1435		259.8		-0.77	
1456	D5185	280.3	0	0.69	5 4 4 1000 00
1630	D5185	235.6	C	-2.49	first reported 202.36
1660 1682	D5185	620 	R(0.01)	24.89	
1704					
1720					
1740					
1748					
1768					
1875	DIN51460-1	264		-0.47	
1890	In house	276		0.39	
1957	D5185	275.0		0.32	
4043 6002	D6595	224 12		2.50	
6016	D0090	234.13		-2.59	
6032					
6034	D5185	365.12	R(0.01)	6.73	
6056			` '		
6117	GB/T17476	287.0		1.17	
6121	DIN51777	274		0.24	
6127	D5185	290		1.38	
7003					
	normality	cuencet			
	normality n	suspect 29			
	outliers	29			
	mean (n)	270.563			
	st.dev. (n)	15.4879			
	R(calc.)	43.366			
	st.dev.(D5185:13e1)	14.0416			
	R(D5185:13e1)	39.316			





**APPENDIX 2** 

Reported details: Foam determination

lab	method	Sample used	Diffuser type	Cylinder cleansed	Gas diffuser cleansed	Air tube cleansed	Air flow rate constant
173							
178							
179	D892	As received	Metal (stainless steel)	YES	YES	Unknown	Unknown
237							
255							
325 349	D892	As received	Metal (stainless steel)	YES 	YES	YES 	Yes: without readjustment
	D892	As received	Stone (non-metallic)	YES	YES	YES	Yes: without readjustment
614	D892	As received	Metal (stainless steel)	YES	YES	NO	Yes: without readjustment
621	2002						
663							
780							
	D892	As received	Stone (non-metallic)	YES	YES	YES	Yes: without readjustment
902	D002						
912							
962							
	D892	As received	Metal (stainless steel)	YES	YES	YES	Yes: without readjustment
994	D092	As received		1L3 			res. without readjustifierit
1011	D892	After agitation, option A	Metal (stainless steel)	YES	YES	YES	Yes: without readjustment
1026	D892	As received	Metal (stainless steel)	YES	YES	YES	Yes: without readjustment
1059	D892	As received	Metal (stainless steel)	YES	YES	YES	Yes: readjustment needed
	D892	As received	Metal (stainless steel)	YES	YES	YES	Yes: without readjustment
1417	D892	As received	Metal (stainless steel)	YES	YES	YES	Yes: readjustment needed
1435	ISO6247		Stone (non-metallic)	YES	YES	NO	Yes: without readjustment
1456							
1630							
1660							
1682							
1704	D892	As received	Metal (stainless steel)	YES	YES	YES	Yes: without readjustment
1720							
1740							
1748	D892						
1768							
1875							
1890							
1957		As received	Metal (stainless steel)	YES	NO	NO	
4043							
6002	ISO6247		Metal (stainless steel)	YES	YES	YES	Yes: without readjustment
	D892	As received	Stone (non-metallic)	YES	YES	YES	Yes: without readjustment
6032	<del>-</del>						
6034							
6056							
6117							
							<del>_</del>
6121							
6127							
7003							

# Reported details: Foam determination – continued

lah	math a d		alonging and diffuser	
lab	method	cleansing cylinder	cleansing gas diffuser	cleansing air tube
173				
178				
	D892		Per D892 Standard	Per D892 Standard
237				
255				
	D892	with solvent in Seta cleaning device	with detergent and solvent	with solvent in Seta cleaning device
349				
	D892			
614	D892	air is constantly on, no cleaning	washed with solvent 13	flushed with solvent 13 and air
		required		
621				
663				
780				
862	D892	n-heptane	petroleum ether 60-90¡æ,	n-heptane
			absolute ethyl alcohol,deionized	
			water,absolute ethyl alcohol	
902				
912				
962				
963	D892	Cleaned the gas tube with heptane	Cleaned the cylinder with heptane,	Cleaned the gas diffuser with heptane &
		& toluene, wipe with moistened	Washed with distilled water, then	toluene, repeated washing 5 times &
		heptane & dry cloth.	acetone and dry in oven	dried in clean air.
994				
	D892	heptane	heptane	heptane
	D892			
1059	D892	According 9.1.2. (see ASTM D 892).	Rinsing with solvent (heptane or	According 9.1.2. (see ASTM D 892).
			similar); after that washing and	
1116	D892	Detroloum other 9 dried with dry air	drying in washing machine. Petroleum ether & dried with dry air	Datralaum ather 9 dried with dry air
	D892 D892	Petroleum ether & dried with dry air Toluene & Petroleum Spirit	Detergent, Petroleum Spirit,	Petroleum ether & dried with dry air Toluene & Petroleum Spirit
1417	D092	roldene & Felioleum Spini	Toluene, Distilled water & acetone	Toluene & Felloleum Spirit
1435	ISO6247		with heptane and ether	placed in heptane, blow air through it,
	.000		man noptano ana otno.	repeat with ether and blow dry with air
1456				·
1630				
1660				
1682				
	D892	by Heptane	by Toluene and heptane	by Toluene and heptane
1720	D032	by rieptane	by roldene and neptane	by Tolderic and Heptane
1740				
	D892			
	D092			
1768				
1875				
1890		Not emplicable	Lland taluana wash with tan water	Not emplicable
1957		Not applicable	Used toluene, wash with tap water, wash with acetone and dry in oven	Not applicable
4042			wash with acetone and dry in oven	
4043	ISO6247	the same like a diffuser	we washed cylinder with toluene, 2-	Diffuser cleansed with toluene and
0002	1000247	the same like a diliuser	propanol next detergent, rinsed with	heptane, next dried with air
			distilled water and acetone.	noptano, next and with an
6016	D892	air, wipe outside of air inlet tube with	Heptane, detergent, DI water,	Toluene, air, heptane, air
		cloth moistened with heptane, then	acetone, drying oven	
		dry cloth	- 0	
6032				
6034				
6056				
6117				
6121				
6127				
7003				

### **APPENDIX 3**

### Number of participants per country

- 1 lab in ALGERIA
- 2 labs in AUSTRALIA
- 1 lab in AUSTRIA
- 1 lab in AZERBAIJAN
- 3 labs in BELGIUM
- 2 labs in CHINA, People's Republic
- 1 lab in FRANCE
- 2 labs in GERMANY
- 1 lab in GREECE
- 3 labs in INDIA
- 1 lab in INDONESIA
- 1 lab in IRAN, Islamic Republic of
- 1 lab in ITALY
- 1 lab in JORDAN
- 1 lab in KAZAKHSTAN
- 1 lab in MALAYSIA
- 2 labs in NETHERLANDS
- 1 lab in NIGERIA
- 1 lab in PERU
- 1 lab in POLAND
- 1 lab in PORTUGAL
- 1 lab in RUSSIAN FEDERATION
- 2 labs in SAUDI ARABIA
- 1 lab in SERBIA
- 1 lab in SLOVENIA
- 2 labs in SPAIN
- 1 lab in SUDAN
- 1 lab in TAIWAN (R.O.C.)
- 1 lab in TANZANIA
- 1 lab in THAILAND
- 2 labs in TURKEY
- 1 lab in UNITED KINGDOM
- 3 labs in UNITED STATES OF AMERICA

### **APPENDIX 4**

### Abbreviations:

DG(0.05)

C = final test result after checking of first reported suspect test result

 $\begin{array}{ll} D(0.01) & = \text{outlier in Dixon's outlier test} \\ D(0.05) & = \text{straggler in Dixon's outlier test} \\ G(0.01) & = \text{outlier in Grubbs' outlier test} \\ G(0.05) & = \text{straggler in Grubbs' outlier test} \\ DG(0.01) & = \text{outlier in Double Grubbs' outlier test} \\ \end{array}$ 

R(0.01) = outlier in Rosner's outlier test R(0.05) = straggler in Rosner's outlier test E = probably an error in calculations

U = test result probably reported in a different unit
W = test result withdrawn on request of participant
ex = test result excluded from statistical evaluation

= straggler in Double Grubbs' outlier test

n.a. = not applicable
n.e. = not evaluated
n.d. = not detected
fr. = first reported

SDS = Safety Data Sheet

### Literature:

- 1 iis Interlaboratory Studies, Protocol for the Organization, Statistics and Evaluation, March 2017
- 2 ASTM E178:16a
- 3 ASTM E1301:95(2003)
- 4 ISO 5725:86
- 5 ISO 5725, parts 1-6, 1994
- 6 ISO 13528:05
- 7 M. Thompson and R. Wood, J. AOAC Int, <u>76</u>, 926, (1993)
- 8 W.J. Youden and E.H. Steiner, Statistical Manual of the AOAC, (1975)
- 9 IP 367:84
- 10 DIN 38402 T41/42
- 11 P.L. Davies, Fr. Z. Anal. Chem, <u>331</u>, 513, (1988)
- 12 J.N. Miller, Analyst, <u>118</u>, 455, (1993)
- 13 Analytical Methods Committee Technical Brief, No 4 January 2001
- 14 P.J. Lowthian and M. Thompson, The Royal Society of Chemistry, Analyst, <u>127</u>, 1359-1364 (2002)
- Bernard Rosner, Percentage Points for a Generalized ESD Many-Outlier Procedure, Technometrics, <u>25(2)</u>, 165-172, (1983)
- 16 Horwitz, R. Albert, J. AOAC Int, <u>79, 3</u>, 589, (1996)