

**Results of Proficiency Test
Fuel Oil
June 2017**

Organised by: Institute for Interlaboratory Studies (iis)
Spijkenisse, the Netherlands

Authors: ing. A.S. Noordman – de Neef
Correctors: dr. R.G. Visser & ing R. J. Starink
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1 INTRODUCTION

Since 1994 the Institute for Interlaboratory Studies (iis) organizes a proficiency test for Fuel Oil every year. During the annual proficiency testing program of 2016/2017, it was decided to continue the round robin for the analyses of Fuel Oil twice per year. The scope for this interlaboratory study is according to the latest applicable version of the specifications ISO 8217 and ASTM D396.

In the round robin with regular Fuel Oil 170 laboratories in 65 different countries registered for participation. In the round robin for Metals in Fuel Oil 100 laboratories in 48 different countries registered for participation. See appendix 2 for the number of participants per country for both rounds.

In this report, the test results of the June 2017 interlaboratory study on Fuel Oil are presented and discussed. This report is also electronically available through the iis website www.iisnl.com.

2 SET-UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, the Netherlands, was the organiser of this proficiency test (PT). Sample analyses for fit-for-use and homogeneity testing were subcontracted to an ISO/IEC 17025 accredited laboratory. Depending on the registration it was decided to send one bottle of 1L Fuel Oil (labelled #17105) and/or one bottle of 0.1L Fuel Oil (labelled #17106) specifically prepared for metal determinations.

Participants were requested to report rounded and unrounded test results. The unrounded test results were preferably used for statistical evaluation.

2.1 ACCREDITATION

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, is accredited in agreement with ISO/IEC 17043:2010 (R007), since January 2000, by the Dutch Accreditation Council (Raad voor Accreditatie). This PT falls under the accredited scope.

This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentiality of participant's data. Feedback from the participants on the reported data is encouraged and customer's satisfaction is measured on regular basis by means of questionnaires.

2.2 PROTOCOL

The protocol followed in the organisation of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of March 2017 (iis-protocol, version 3.4). This protocol is electronically available through the iis website www.iisnl.com, from the FAQ page.

2.3 CONFIDENTIALITY STATEMENT

All data presented in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

2.4 SAMPLES

For this proficiency test a regular Fuel Oil and a Fuel Oil positive on metals were prepared. Approximately 200 litre Fuel Oil was obtained from a supplier in Germany. After heating to 60°C and homogenisation of this batch 200 amber glass bottles of 1L were filled and labelled #17105. The homogeneity of these subsamples was checked by determination of Density at 15°C in accordance with ISO12185 on 8 stratified randomly selected samples.

| | Density at 15°C in kg/m ³ |
|-----------------|--------------------------------------|
| Sample #17105-1 | 982.7 |
| Sample #17105-2 | 982.7 |
| Sample #17105-3 | 982.7 |
| Sample #17105-4 | 982.7 |
| Sample #17105-5 | 982.7 |
| Sample #17105-6 | 982.7 |
| Sample #17105-7 | 982.7 |
| Sample #17105-8 | 982.7 |

Table 1: homogeneity test results of subsamples #17105

From the above test results the repeatability was calculated and compared with 0.3 times the corresponding reproducibility of the reference test method in agreement with the procedure of ISO 13528, Annex B2 in the next table:

| | Density at 15°C in kg/m ³ |
|----------------------------|--------------------------------------|
| r (observed) | 0.00 |
| reference test method | ISO12185:96 |
| 0.3 * R (ref. test method) | 0.45 |

Table 2: evaluation of the repeatability of test results of subsamples #17105

The calculated repeatability for Density was in agreement with 0.3 times the corresponding reproducibility of the reference test method. Therefore, homogeneity of the subsamples of #17105 was assumed.

For the preparation of the subsamples for the PT on Fuel Oil Metals approx. 18 litre of a batch of Fuel Oil obtained from a local supplier was spiked with Calcium (approx. 19 mg/kg), Phosphorus (approx. 15 mg/kg) and Zinc (approx. 17 mg/kg). After heating to 60°C and homogenisation of the batch 128 plastic PE bottles of 0.1L were filled and labelled #17106. The homogeneity of the subsamples was checked by determination of Phosphorus and Silicon in accordance with IP501 on 8 stratified randomly selected samples.

| | Phosphorus in mg/kg | Silicon in mg/kg |
|-----------------|---------------------|------------------|
| Sample #17106-1 | 17.1 | 11.7 |
| Sample #17106-2 | 17.2 | 11.9 |
| Sample #17106-3 | 16.8 | 11.7 |
| Sample #17106-4 | 17.2 | 11.9 |
| Sample #17106-5 | 16.7 | 11.5 |
| Sample #17106-6 | 17.4 | 11.8 |
| Sample #17106-7 | 17.1 | 11.5 |
| Sample #17106-8 | 17.0 | 11.6 |

Table 3: homogeneity test results of subsamples #17106

From above test results the repeatabilities were calculated and compared with 0.3 times the corresponding reproducibilities of the reference test methods in agreement with the procedure of ISO 13528, Annex B2 in the next table:

| | Phosphorus in mg/kg | Silicon in mg/kg |
|----------------------------|---------------------|------------------|
| r (observed) | 0.6 | 0.4 |
| reference test method | IP501:05 | IP470:05 |
| 0.3 * R (ref. test method) | 1.8 | 2.2 |

Table 4: evaluation of the repeatabilities of subsamples #17106

The calculated repeatabilities for Phosphorus and Silicon were in agreement with 0.3 times the corresponding reproducibilities of the reference test methods. Therefore, homogeneity of the subsamples of #17106 was assumed.

Depending on the registration of the participant; one bottle of 1L, labelled #17105 and/or one bottle of 0.1L, labelled #17106 were sent to the participating laboratories on May 31, 2017. An SDS was added to the sample package.

2.5 STABILITY OF THE SAMPLES

The stability of Fuel Oil, packed in the amber glass and plastic PE bottles was checked. The material has been found sufficiently stable for the period of the proficiency test.

2.6 ANALYSES

The participants were requested to determine one to all of the following parameters:

On sample #17105: Acid Number (total), API Gravity, Ash Content, Asphaltenes, Calculated Carbon Aromaticity Index (CCAI), Carbon Residue – Micro Method, Conradson Carbon Residue, Density at 15°C, Flash Point PMcc, Heat of Combustion (Gross and Net), Kinematic Viscosity (at 50°C and 100°C), Viscosity Stabinger (at 50°C and 100°C), Nitrogen, Pour Point (Lower, Upper and Automated), Sediment by Extraction, Total Sediment (by Hot filtration, Accelerated and Potential), Total Sulphur, Water by Distillation, Water and Sediment, Distillation (IPB, 5% - 50% recovered and FBP) and Total Carbon, Hydrogen and Nitrogen (CHN-analyzer).

On sample #17106: Aluminium, Silicon, Sum of Aluminium and Silicon, Iron, Nickel, Sodium, Vanadium, Calcium, Phosphorus and Zinc content.

It was explicitly requested to treat the sample as if it was a routine sample. Therefore, each laboratory is advised to perform only those analyses that normally are done in daily routine (but the laboratories are allowed to do all analyses). Furthermore, it was requested to report the test results using the indicated units on the report form and not to round the test results more, but report as much significant figures as possible. It was also requested not to report 'less than' test results, which are above the detection limit, because such test results cannot be used for meaningful statistical evaluations.

To get comparable test results, a detailed report form and a letter of instructions are prepared. On the report form the reporting units are given as well as the reference test methods that will be used during the evaluation. The detailed report form and the letter of instructions are both made available on the data entry portal www.kpmd.co.uk/sgs-iis/. The participating laboratories are also requested to confirm the sample receipt on this data entry portal. The letter of instructions can also be downloaded from the iis website www.iisnl.com.

3 RESULTS

During five weeks after sample dispatch, the test results of the individual laboratories were gathered via the data entry portal www.kpmd.co.uk/sgs-iis/. The reported test results are tabulated per determination in appendix 1 of this report. The laboratories are presented by their code numbers.

Directly after the deadline, a reminder was sent to those laboratories that had not reported test results at that moment. Shortly after the deadline, the available test results were screened for suspect data. A test result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the reported test results (no reanalysis). Additional or corrected test results are used for data analysis and original test results are placed under 'Remarks' in the test result tables in appendix 1. Test results that came in after the deadline were not taken into account in this screening for suspect data and thus these participants were not requested for checks.

3.1 STATISTICS

The protocol followed in the organization of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of March 2017 (iis-protocol, version 3.4).

For the statistical evaluation the *unrounded* (when available) figures were used instead of the rounded test results. Test results reported as '<...' or '>...' were not used in the statistical evaluation.

First, the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test a variant of the Kolmogorov-Smirnov test and by the calculation of skewness and kurtosis. Evaluation of the three normality indicators in combination with the visual evaluation of the graphic Kernel density plot, lead to judgement of the normality being either 'unknown', 'OK', 'suspect' or 'not OK'. After removal of outliers, this check was repeated. If a data set does not have a normal distribution, the results of the statistical evaluation should be used with due care.

According to ISO 5725 the original test results per determination were submitted to Dixon's, Grubbs' and/or Rosner's outlier tests. Outliers are marked by D(0.01) for the Dixon's test, by G(0.01) or DG(0.01) for the Grubbs' test and by R(0.01) for the Rosner's test. Stragglers are marked by D(0.05) for the Dixon's test, by G(0.05) or DG(0.05) for the Grubbs' test and by R(0.05) for the Rosner's test. Both outliers and stragglers were not included in the calculations of averages and standard deviations.

For each assigned value the uncertainty was determined in accordance with ISO13528.

Subsequently the calculated uncertainty was evaluated against the respective requirements based on the target reproducibility in accordance with ISO13528. When the uncertainty passed the evaluation, no remarks are made in the report. However, when the uncertainty failed the evaluation it is mentioned in the report and it will have consequences for the evaluation of the test results.

Finally, the reproducibilities were calculated from the standard deviations by multiplying them with a factor of 2.8.

3.2 GRAPHICS

In order to visualise the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported test results are plotted. The corresponding laboratory numbers are on the X-axis. The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected reference test method. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle. Furthermore, Kernel Density Graphs were made. This is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. Also, a normal Gauss curve was projected over the Kernel Density Graph for reference.

3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements, e.g. ASTM, ISO or EN reproducibilities, the z-scores were calculated using a target standard deviation. This results in an evaluation independent of the variation of this interlaboratory study.

The target standard deviation was calculated from the literature reproducibility by division with 2.8. In case no literature reproducibility was available, other targets values were used. In some cases, a reproducibility based on former iis proficiency tests could be used.

When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate whether the reported test result is fit-for-use.

The z-scores were calculated according to:

$$z_{(\text{target})} = (\text{test result} - \text{average of PT}) / \text{target standard deviation}$$

The $z_{(\text{target})}$ scores are listed in the test result tables in appendix 1.

Absolute values for $z < 2$ are very common and absolute values for $z > 3$ are very rare.

The usual interpretation of z-scores is as follows:

| | |
|---------------|----------------|
| $ z < 1$ | good |
| $1 < z < 2$ | satisfactory |
| $2 < z < 3$ | questionable |
| $3 < z $ | unsatisfactory |

4 EVALUATION

In this proficiency test major problems were encountered with the dispatch of the samples. Several laboratories in Egypt, India, Indonesia, Iran, Malaysia, Saudi Arabia and Sudan received the samples late or not at all. For the main round (sample #17105) three participants did not report any test results and five participants reported the test results after the final reporting date. For the metals round (sample #17106) ten participants did not report any test results. Three of these ten reported that the equipment was down. Nine participants reported the test results after the final reporting date. Not all laboratories were able to report all analyses requested.

Finally over the main and metal PTs, 169 participants reported in total 3119 numerical test results. Observed were 102 statistically outlying test results, which is 3.3% of the numerical test results. In proficiency studies, outlier percentages of 3% - 7.5% are quite normal.

Not all original data sets proved to have a normal Gaussian distribution. These are referred to as "not OK" or "suspect". The statistical evaluation of these data sets should be used with due care, see also paragraph 3.1.

4.1 EVALUATION PER SAMPLE AND PER TEST

In this section, the reported test results are discussed per sample and per test. The test methods, which are used by the different laboratories, are taken into account for explaining the observed differences when possible and applicable. These test methods are also listed in the tables together with the reported test results. The abbreviations, used in these tables, are listed in appendix 3.

In the iis PT reports, ASTM test methods are referred to with a number (e.g. D189) and an added designation for the year that the test method was adopted or revised (e.g. D189:06). If applicable, a designation in parentheses is added to designate the year of reapproval (e.g. D189:06(2014)). In the test results tables of appendix 1 only the test method number and year of adoption or revision (e.g. D189:06) are used.

Sample #17105

Acid Number: This determination was not problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D664-A:11ae1(2017).

API Gravity: This determination was not problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ASTM D1298:12b(2017).

Ash: This determination was very problematic at an ash content of 0.024 %M/M. Three statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not at all in agreement with requirements of ISO6245:01.

Asphaltenes: This determination was problematic. No statistical outliers were observed. However, the calculated reproducibility is not in agreement with the requirements of IP143:04(2016).

Calculated Carbon Aromaticity Index: This determination was not problematic. No statistical outliers and no calculation errors were observed. The calculated reproducibility is in agreement with the requirements of ISO8217:12.

Carbon Residue Micro Method: This determination was not problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in full agreement with the requirements of ISO10370:14.

Conradson Carbon Residue: This determination was not problematic. One statistical outlier was observed. However, the calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ASTM D189:06(2014).

Remarkably, three participants reported to use ASTM D4530 which is the micro method thata was evaluated seperately.

Density at 15°C: This determination was problematic for a number of participants. Six statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in full agreement with the requirements of ISO12185:96.

Flash Point PMcc: This determination was not problematic. Four statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ISO2719-B:16.

HOC Gross: This determination of the Gross Heat of Combustion was not problematic. One statistical outlier was observed. However, the calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ASTM D240:17.

HOC Net: This determination of the Net Heat of Combustion was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D240:17.

Kin. Visc. At 50°C: This determination was not problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in full agreement with the requirements of ISO3104:94.

Kin. Visc. At 100°C: This determination was not problematic. Three statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ISO3104:94.

Vis Stab.at 50°C: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D7042:16e3.

Vis Stab.at 100°C: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D7042:16e3.

Nitrogen: This determination was problematic. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ASTM D5762:12(2017). When the test results of ASTM D5762 volumetric and gravimetric test methods were evaluated separately, the calculated reproducibility of the volumetric test results was much smaller than the calculated reproducibility of the gravimetric test results. This finding is the same as found in the two Fuel Oil PTs of 2016 (iis16F01&iis16F03). The calculated reproducibility of the Volumetric test method is in agreement with the requirements of ASTM D5762:12(2017).

Pour Point Lower: This determination was problematic. No statistical outliers were observed. However, the calculated reproducibility is not in agreement with the requirements of ISO3016:94. Rounding to 3 degrees acc. ISO3016:94 may (partly) explain the large variation.

Pour Point Upper: This determination was problematic. One statistical outlier was observed. The calculated reproducibility after rejection of the statistical outlier is not in agreement with ISO3016:94. Rounding to 3 degrees acc. ISO3016:94 may (partly) explain the large variation.

Pour Point Automated: This determination was problematic. One statistical outlier was observed. However, the calculated reproducibility after rejection of the statistical outlier is not in agreement with ASTM D5950:14. The large variation may (partly) be explained by possible problems with the detector sensitivity or by not following the test method properly (see Note 8 in ASTM D5950:14). Rounding to 3 degrees may also (partly) explain the large variation.

Sediment by Extraction: This determination was not problematic. One statistical outlier was observed. However, the calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ASTM D473:07(2017).

Total Sediment (Hot filtration): This determination was not problematic. Three statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of IP375:11.

Total Sediment (Accelerated): This determination was not problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with IP390:11. IP390:11 is identical to ISO10307-2:09 and technically equivalent to ASTM D4870 (see appendix X1).

Total Sediment (Potential): This determination was not problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in good agreement with IP390:11. IP390:11 is identical to ISO10307-2:09 and technically equivalent to ASTM D4870 (see appendix X1).

Total Sulphur: This determination may be problematic dependent on the test method used. Two statistical outliers were observed. The calculated reproducibility after rejection of the statistical outliers is in agreement with the requirements of ISO 8754:03 but not with the more strict requirements of ASTM D4294:16e1.

Water by distillation: This determination was not problematic. One statistical outlier was observed. However, the calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ISO3733:99 or ASTM D95:13e1.

Water and Sediment: This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in full agreement with the requirements of ASTM D1796:11(2016).

Vacuum Distillation: This determination may be problematic for 50% recovered and FBP. In total ten statistical outliers were observed over eight parameters. Four other test results were excluded as the other reported test results of this participant were marked as statistical outliers. However, the calculated reproducibility after rejection of the suspect data is in agreement for IBP, 5%, 10%, 20%, 30% and 40% recovered with the requirements of ASTM D1160:15. The calculated reproducibilities for 50% recovered and FBP are not in agreement with the requirements of ASTM D1160:15.

CHN-Analyzer: This determination was not problematic for Carbon, Hydrogen and Nitrogen. One statistical outlier was observed for Carbon and two statistical outliers for Hydrogen. The calculated reproducibilities after rejection of the statistical outliers are all in agreement with the respective requirements of ASTM D5291-ABC:16.

Sample #17106:

Aluminium: This determination may be problematic for a number of participants. Six statistical outliers were observed and one other test result was excluded as 50% of the other metal tests results were marked as statistical outliers. However, the calculated reproducibility after rejection of the suspect data is in full agreement with the reproducibility of IP470:05 and IP501:05.

Silicon: This determination may be problematic depending on the test method used. Two statistical outliers were observed and two other test results were excluded as about 50% of the other metal tests results were marked as statistical outliers. However, the calculated reproducibility after rejection of the suspect data is in full agreement with the reproducibility of IP470:05 but not in agreement with the more strict requirements of IP501:05.

Total Al/Si: This determination may be problematic depending on the test method used. Three statistical outliers were observed and three other test results were excluded. One test result because about 50% of the other metal tests results were marked as statistical outliers and the other two because of a statistical outlier in the Al determination. However, the calculated reproducibility after rejection of the suspect data is in full agreement with the reproducibility of IP470:05 but not in agreement with the more strict requirements of IP501:05.

Iron: This determination may be problematic depending on the test method used. Two statistical outliers were observed and two other test results were excluded as about 50% of the other metal tests results were marked as statistical outliers. However, the calculated reproducibility after rejection of the suspect data is in agreement with the reproducibility of IP470:05, but not in agreement with the more strict requirements of IP501:05.

- Nickel: This determination may not be problematic. Nine statistical outliers were observed and one other test result was excluded as about 50% of the other metal tests results were marked as statistical outliers. However, the calculated reproducibility after rejection of the suspect data is in agreement with the reproducibilities of IP470:05 and IP501:05.
- Sodium: This determination was not problematic. Four statistical outliers were observed and two other test results were excluded as about 50% of the other metal tests results were marked as statistical outliers. However, the calculated reproducibility after rejection of the suspect data is in agreement with the reproducibilities of IP470:05 and IP501:05.
- Vanadium: This determination was not problematic. Five statistical outliers were observed and one other test result was excluded as about 50% of the other metal tests results were marked as statistical outliers. However, the calculated reproducibility after rejection of the suspect data is in good agreement with the reproducibilities of IP470:05 and IP501:05.
- Calcium: This determination was problematic for a number of laboratories. Six statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in full agreement with the requirements of IP470:05 and IP501:05.
The average recovery of Calcium (theoretical increment of 19.4 mg Calcium/kg) may be sufficient: “< 135%” (the actual blank Calcium content is unknown).
- Zinc: This determination may be problematic dependent on the test method used. Six statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in full agreement with the reproducibilities of IP470:05 but not in agreement with the more strict requirements of IP501:05.
The average recovery of Zinc (theoretical increment of 16.9 mg Zinc/kg) may be good: “< 108%” (the actual blank Zinc content is unknown).
- Phosphorus: This determination was problematic for a number of participants. Five statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in agreement with the reproducibility of IP501:05 but not in agreement with the more strict requirements of IP500:03.
The average recovery of Phosphorus (theoretical increment of 14.6 mg Phosphorus/kg) may be good: “< 117%” (the actual blank Phosphorus content is unknown).

Finally it should be noted that proper attention for homogenisation is crucial for a material such as Fuel Oil. Due to the nature of the material it is very susceptible to problems when not handled correctly. Practically most test methods for the determination of metals in Fuel Oil have similar statements regarding homogenization. Recommended is the use of a quality control fuel oil with known amounts of metals like Al, Fe, Si and V. This control standard may be of use to detect deviations in metals with respect to the preparation steps.

4.2 PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES

A comparison has been made between the reproducibility ($2.8 * \text{sd}$) as declared by the relevant reference test methods and the reproducibility ($R (\text{lit})$) as found for the group of participating laboratories. The average test results of the evaluated parameters, calculated reproducibilities and reproducibilities, derived from reference test methods (in casu ASTM, EN, ISO and IP reference methods) are compared in the next table.

| Parameters | unit | n | average | $2.8 * \text{sd}$ | $R (\text{lit})$ |
|--|--------------------|-----|---------|-------------------|------------------|
| Acid Number | mg KOH/g | 85 | 0.29 | 0.14 | 0.18 |
| API Gravity | | 91 | 12.3 | 0.3 | 0.5 |
| Ash Content | %M/M | 111 | 0.024 | 0.010 | 0.005 |
| Asphaltenes | %M/M | 75 | 4.25 | 1.28 | 0.85 |
| Calc. Carbon Aromaticity Index | | 71 | 845.2 | 1.6 | 2.4 |
| Carbon Residue, Micro Method | %M/M | 102 | 11.2 | 1.1 | 1.2 |
| Conradson Carbon Residue | %M/M | 43 | 11.4 | 1.3 | 1.8 |
| Density at 15°C | kg/m ³ | 148 | 983.0 | 1.4 | 1.5 |
| Flash Point PMcc | °C | 134 | 117.7 | 6.5 | 6 |
| Heat of Combustion, Gross | MJ/kg | 72 | 43.09 | 0.30 | 0.40 |
| Heat of Combustion, Net | MJ/kg | 60 | 40.78 | 0.35 | 0.40 |
| Kinematic Viscosity at 50°C | mm ² /s | 126 | 342.9 | 24.2 | 25.4 |
| Kinematic Viscosity at 100°C | mm ² /s | 99 | 31.63 | 1.21 | 1.59 |
| Stabinger Viscosity at 50°C | mm ² /s | 12 | 347.5 | 23.5 | 35.8 |
| Stabinger Viscosity at 100°C | mm ² /s | 11 | 31.58 | 0.61 | 2.27 |
| Nitrogen Content | mg/kg | 24 | 3104 | 917 | 826 |
| Pour Point, Lower | °C | 64 | 0.8 | 9.7 | 6.6 |
| Pour Point, Upper | °C | 101 | 2.2 | 9.6 | 6.6 |
| Pour Point (automated), Δ3°C | °C | 24 | -0.3 | 9.2 | 6.1 |
| Sediment by Extraction | %M/M | 83 | 0.019 | 0.025 | 0.038 |
| Total Sediment (Hot Filtration) | %M/M | 71 | 0.019 | 0.014 | 0.040 |
| Total Sediment (Accelerated) | %M/M | 61 | 0.021 | 0.019 | 0.043 |
| Total Sediment (Potential) | %M/M | 59 | 0.019 | 0.014 | 0.041 |
| Total Sulphur Content | %M/M | 154 | 1.07 | 0.08 | 0.10 |
| Water by Distillation | %V/V | 88 | 0.04 | 0.07 | 0.2 |
| Water and Sediment | %V/V | 37 | 0.06 | 0.09 | 0.1 |
| Distillation at 10 mmHg calculated to 760 mmHg | | | | | |
| Initial Boiling Point | °C | 30 | 216.2 | 26.8 | 49 |
| 5% recovered | °C | 30 | 262.6 | 17.8 | 22.1 |
| 10% recovered | °C | 29 | 299.4 | 20.4 | 20.7 |
| 20% recovered | °C | 31 | 368.5 | 20.5 | 20.0 |
| 30% recovered | °C | 31 | 428.5 | 18.0 | 19.0 |
| 40% recovered | °C | 30 | 483.0 | 18.1 | 18.5 |
| 50% recovered | °C | 11 | 536.0 | 20.4 | 18.4 |

| Parameters | unit | n | average | 2.8 * sd | R (lit) |
|---------------------|------|----|---------|----------|---------|
| Final Boiling Point | °C | 23 | 522.6 | 43.1 | 27 |
| CHN analyser | | | | | |
| Total Carbon | %M/M | 26 | 87.6 | 2.0 | 2.4 |
| Total Hydrogen | %M/M | 24 | 10.7 | 0.5 | 0.8 |
| Total Nitrogen | %M/M | 21 | 0.36 | 0.18 | 0.45 |

Table 5: summary of test results on Fuel Oil sample #17105

| Parameters | unit | n | average | 2.8 * sd | R (lit) |
|-------------------------|-------|----|---------|----------|---------|
| Aluminium as Al | mg/kg | 73 | 10.7 | 3.7 | 3.9 |
| Silicon as Si | mg/kg | 73 | 11.7 | 6.6 | 7.2 |
| Total Aluminium+Silicon | mg/kg | 67 | 22.5 | 8.3 | 8.2 |
| Iron as Fe | mg/kg | 74 | 19.9 | 7.7 | 11.3 |
| Nickel as Ni | mg/kg | 72 | 18.3 | 5.1 | 11.5 |
| Sodium as Na | mg/kg | 75 | 10.3 | 4.0 | 5.3 |
| Vanadium as V | mg/kg | 79 | 39.5 | 11.8 | 20.5 |
| Calcium as Ca | mg/kg | 69 | 26.1 | 5.7 | 6.8 |
| Phosphorus as P | mg/kg | 58 | 17.0 | 4.6 | 6.1 |
| Zinc as Zn | mg/kg | 69 | 18.3 | 4.6 | 5.1 |

Table 6: summary of test results on Fuel Oil sample #17106

Without further statistical calculations it can be concluded that for a number tests there is a good compliance of the group of participating laboratories with the relevant reference test method. The problematic tests have been discussed in paragraph 4.1.

4.3 COMPARISON OF THE PROFICIENCY TEST OF JUNE 2017 WITH PREVIOUS PTS

| | June 2017 | December 2016 | January 2016 | January 2015 | January 2014 |
|----------------------------|--------------|------------------|-----------------|-----------------|-----------------|
| Number of reporting labs | 169 | 83 | 226 | 207 | 200 |
| Number of results reported | 3119 | 1936 | 4787 | 4048 | 3835 |
| Statistical outliers | 102 | 72 | 115 | 130 | 112 |
| Percentage outliers | 3.3% | 3.7% | 2.4% | 3.2% | 2.9% |

Table 7: comparison with previous proficiency tests

In proficiency tests, outlier percentages of 3% - 7.5% are quite normal.

The performance of the determinations of the proficiency tests was compared against the requirements of the respective reference methods. The conclusions are given the following table:

| Determination | June 2017 | December 2016 | January 2016 | January 2015 | January 2014 |
|---------------------------------|--------------|------------------|-----------------|-----------------|-----------------|
| Acid Number | + | ++ | + | ++ | + |
| API Gravity | ++ | ++ | ++ | ++ | ++ |
| Ash Content | -- | -- | - | -- | -- |
| Asphaltenes | - | -- | +/- | - | + |
| Calc. Carbon Aromaticity Index | + | + | + | + | + |
| Carbon Residue, Micro Method | +/- | + | + | ++ | +/- |
| Conradson Carbon Residue | + | +/- | + | + | + |
| Density at 15 °C | +/- | + | +/- | +/- | + |
| Flash Point PMcc | +/- | +/- | - | - | +/- |
| Heat of Combustion Gross | + | ++ | - | -- | + |
| Heat of Combustion Net | + | ++ | - | -- | + |
| Kinematic Viscosity at 50°C | +/- | ++ | + | ++ | + |
| Kinematic Viscosity at 100°C | + | - | +/- | - | - |
| Stabinger Viscosity at 50°C | + | + | n.e. | n.e. | n.e. |
| Stabinger Viscosity at 100°C | ++ | ++ | n.e. | n.e. | n.e. |
| Nitrogen | - | - | - | -- | - |
| Pour Point Lower | - | - | - | - | - |
| Pour Point Upper | - | - | - | - | - |
| Pour Point (automated), Δ3°C | - | -- | - | -- | - |
| Sediments by Extraction | + | ++ | ++ | ++ | + |
| Total Sediment (Hot Filtration) | ++ | ++ | ++ | ++ | + |
| Total Sediment (Accelerated) | ++ | ++ | ++ | ++ | ++ |
| Total Sediment (Potential) | ++ | ++ | ++ | ++ | ++ |
| Total Sulphur | + | +/- | + | -- | +/- |
| Water by Distillation | ++ | ++ | ++ | ++ | ++ |
| Water and Sediment | +/- | ++ | + | +/- | + |
| Distillation at 10mmHg to AET | +/- | - | +/- | +/- | +/- |
| Total Carbon | + | + | + | + | + |
| Total Hydrogen | + | + | + | ++ | + |
| Total Nitrogen | ++ | +/- | - | -- | - |
| Aluminium as Al | +/- | n.e. | n.e. | +/- | - |
| Silicon as Si | + | n.e. | n.e. | + | - |
| Total Aluminium/Silicon | +/- | n.e. | n.e. | + | - |
| Iron as Fe | + | + | + | ++ | - |
| Nickel as Ni | ++ | + | + | ++ | + |
| Sodium as Na | + | +/- | +/- | + | - |
| Vanadium as V | ++ | + | + | ++ | ++ |
| Calcium as Ca | + | +/- | - | -- | - |
| Phosphorus as P | + | + | + | ++ | + |
| Zinc as Zn | + | + | - | - | +/- |
| Bromine Number | n.e. | + | - | +/- | n.e. |
| p-Value | n.e. | +/- | ++ | +/- | n.e. |
| Compatibility | n.e. | +/- | n.e. | n.e. | n.e. |

Table 8: comparison determinations against the reference test method

The performance of the determinations against the requirements of the respective reference method is listed in the above table. The following performance categories were used:

- ++: group performed much better than the reference test method
- + : group performed better than the reference test method
- +/-: group performance equals the reference test method
- : group performed worse than the reference test method
- : group performed much worse than the reference test method
- n.e.: not evaluated

APPENDIX 1

Determination of Acid Number (total) on sample #17105; results in mg KOH/g

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|----------|-------|-----------|---------|------|---------|--------|------|---------|
| 62 | D664-A | 0.24 | | -0.80 | 870 | D664-A | 0.30 | | 0.12 |
| 90 | | ----- | | ----- | 886 | | ----- | | ----- |
| 92 | | ----- | | ----- | 902 | D664-A | 0.278 | | -0.22 |
| 120 | D664-A | 0.19 | | -1.57 | 904 | D664-A | 0.28 | | -0.19 |
| 131 | | ----- | | ----- | 912 | | ----- | | ----- |
| 140 | D664-A | 0.08 | R(0.01) | -3.26 | 913 | D664-A | 0.322 | | 0.46 |
| 150 | D664-A | 0.25 | | -0.65 | 922 | D664-A | 0.338 | | 0.71 |
| 158 | | ----- | | ----- | 962 | | ----- | | ----- |
| 159 | D664-A | 0.29 | | -0.03 | 963 | D664 | 0.30 | | 0.12 |
| 168 | | ----- | | ----- | 971 | D664-A | 0.31 | | 0.28 |
| 169 | | ----- | | ----- | 974 | D664-A | 0.33 | | 0.58 |
| 171 | D664-A | 0.29 | | -0.03 | 982 | | ----- | | ----- |
| 175 | | ----- | | ----- | 997 | | ----- | | ----- |
| 194 | D664-A | 0.34 | | 0.74 | 1006 | | ----- | | ----- |
| 212 | D664-A | 0.32 | | 0.43 | 1011 | D664-A | 0.280 | | -0.19 |
| 221 | | ----- | | ----- | 1059 | ISO6619 | 0.28 | | -0.19 |
| 224 | D974 | 0.023 | C,R(0.01) | -4.14 | 1065 | D664-A | 0.273 | | -0.29 |
| 225 | D664-A | 0.27 | | -0.34 | 1082 | | ----- | | ----- |
| 237 | D664-A | 0.19 | | -1.57 | 1095 | D664-A | 0.274 | | -0.28 |
| 238 | D664-A | 0.149 | | -2.20 | 1099 | | ----- | | ----- |
| 252 | | ----- | | ----- | 1109 | D664-A | 0.29 | | -0.03 |
| 253 | | ----- | | ----- | 1126 | | ----- | | ----- |
| 254 | | ----- | | ----- | 1134 | D664-A | 0.25 | | -0.65 |
| 273 | D974 | 0.44 | C | 2.27 | 1135 | D664-A | 0.2635 | | -0.44 |
| 311 | D664-A | 0.31 | | 0.28 | 1161 | | ----- | | ----- |
| 313 | | ----- | | ----- | 1167 | | ----- | | ----- |
| 323 | D664-A | 0.26 | | -0.49 | 1177 | | ----- | | ----- |
| 331 | D664Mod. | 0.325 | | 0.51 | 1191 | | ----- | | ----- |
| 333 | | ----- | | ----- | 1213 | | ----- | | ----- |
| 334 | | ----- | | ----- | 1229 | | ----- | | ----- |
| 336 | | ----- | | ----- | 1233 | D664-A | 0.38 | | 1.35 |
| 337 | | ----- | | ----- | 1254 | D664-A | 0.325 | | 0.51 |
| 342 | D664-A | 0.32 | | 0.43 | 1259 | D664-A | 0.313 | | 0.32 |
| 343 | | ----- | | ----- | 1275 | | ----- | | ----- |
| 349 | | ----- | | ----- | 1299 | D664-A | 0.290 | | -0.03 |
| 351 | | ----- | | ----- | 1345 | D664-A | 0.301 | | 0.14 |
| 371 | | ----- | | ----- | 1356 | D664-A | 0.325 | | 0.51 |
| 391 | D664-A | 0.287 | | -0.08 | 1367 | IP177 | 0.37 | | 1.20 |
| 398 | D664-A | 0.291 | | -0.02 | 1389 | D664-A | 0.29 | | -0.03 |
| 399 | | ----- | | ----- | 1402 | IP177 | 0.262 | | -0.46 |
| 440 | | ----- | | ----- | 1404 | D664-A | 0.295 | | 0.05 |
| 444 | | ----- | | ----- | 1412 | D664-A | 0.28 | | -0.19 |
| 445 | D664-A | 0.311 | | 0.29 | 1428 | | ----- | | ----- |
| 447 | D664-A | 0.305 | | 0.20 | 1431 | | ----- | | ----- |
| 463 | D664-A | 0.434 | | 2.18 | 1459 | | ----- | | ----- |
| 511 | | ----- | | ----- | 1488 | | ----- | | ----- |
| 541 | | ----- | | ----- | 1510 | | ----- | | ----- |
| 562 | | ----- | | ----- | 1539 | D664-A | 0.30 | | 0.12 |
| 575 | D664-A | 0.35 | | 0.89 | 1556 | D664-A | 0.24 | | -0.80 |
| 603 | | ----- | | ----- | 1569 | D664-A | 0.27 | | -0.34 |
| 604 | | ----- | | ----- | 1584 | | ----- | | ----- |
| 605 | D664-A | 0.29 | | -0.03 | 1586 | D664-A | 0.276 | | -0.25 |
| 608 | D664-A | 0.135 | | -2.41 | 1613 | D664-A | 0.157 | | -2.08 |
| 621 | | ----- | | ----- | 1622 | D664-A | 0.3241 | | 0.49 |
| 631 | | ----- | | ----- | 1631 | | ----- | | ----- |
| 663 | D664-A | 0.313 | | 0.32 | 1643 | D664-A | 0.327 | | 0.54 |
| 671 | | ----- | | ----- | 1710 | D664-A | 0.276 | | -0.25 |
| 750 | D664-A | 0.23 | | -0.95 | 1720 | D664-A | 0.33 | C | 0.58 |
| 753 | D664-A | 0.26 | | -0.49 | 1724 | D664-A | 0.331 | | 0.60 |
| 759 | | ----- | | ----- | 1728 | | ----- | | ----- |
| 824 | D664-A | 0.30 | C | 0.12 | 1740 | D664-A | 0.23 | | -0.95 |
| 825 | | ----- | | ----- | 1741 | ISO6619 | 0.270 | | -0.34 |
| 851 | | ----- | | ----- | 1796 | D664-A | 0.2853 | | -0.10 |
| 855 | D664-A | 0.31 | | 0.28 | 1807 | | ----- | | ----- |
| 857 | D664-A | 0.30 | | 0.12 | 1832 | | ----- | | ----- |
| 858 | D664-A | 0.32 | | 0.43 | 1833 | | ----- | | ----- |
| 859 | D664-A | 0.30 | | 0.12 | 1849 | | ----- | | ----- |
| 862 | D664-A | 0.253 | | -0.60 | 1857 | D664-A | 0.30 | | 0.12 |
| 863 | D664-A | 0.28 | | -0.19 | 1862 | D664-A | 0.278 | | -0.22 |
| 864 | D664-A | 0.30 | | 0.12 | 1881 | | ----- | | ----- |
| 865 | D664-A | 0.311 | | 0.29 | 1906 | | ----- | | ----- |
| 866 | D664-A | 0.28 | | -0.19 | 1936 | | ----- | | ----- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|--------|--------|------|---------|------|--------|-------|------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | D664-A | 0.287 | | -0.08 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | D664-A | 0.29 | | -0.03 |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | D664-A | 0.285 | | -0.11 | 6057 | D664-A | 0.344 | | 0.80 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | D664-A | 0.29 | | -0.03 | 6092 | | ---- | | ---- |
| 1995 | D664-A | 0.3965 | C | 1.61 | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | | ---- | | ---- | 6114 | D664-A | 0.300 | | 0.12 |
| 6021 | D664-A | 0.295 | | 0.05 | 6122 | | ---- | | ---- |

| | |
|-----------------|--------|
| normality | not OK |
| n | 85 |
| outliers | 2 |
| mean (n) | 0.2921 |
| std.dev. (n) | 0.0492 |
| R(calc.) | 0.1380 |
| R(D664-A:11ae1) | 0.1822 |

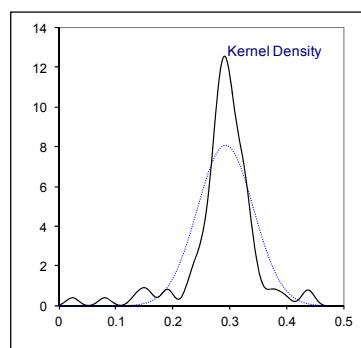
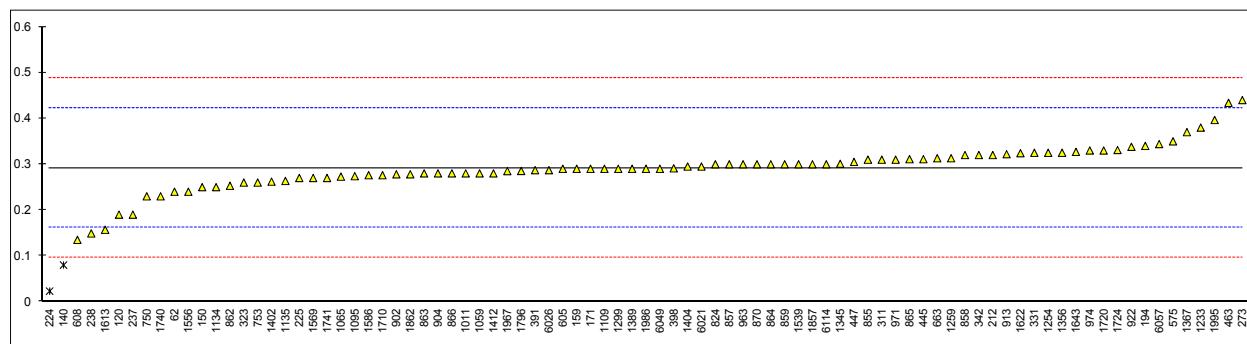
Lab 224 first reported: 0.0445

Lab 273 first reported: 0.942

Lab 824 first reported: 0.033

Lab 1720 first reported: 0.65

Lab 1995 first reported: 0.4965



Determination of API Gravity on sample #17105

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|----------|--------|-----------|---------|------|----------|--------|-----------|---------|
| 62 | D4052 | 12.3 | | -0.25 | 870 | D1298 | 12.33 | | -0.09 |
| 90 | D4052 | 12.39 | | 0.25 | 886 | | ---- | | ---- |
| 92 | D4052 | 12.41 | | 0.36 | 902 | D4052 | 12.32 | | -0.14 |
| 120 | ISO12185 | 12.3 | | -0.25 | 904 | D4052 | 12.3 | | -0.25 |
| 131 | D4052 | 12.35 | | 0.03 | 912 | D1298 | 12.32 | | -0.14 |
| 140 | D4052 | 12.3 | | -0.25 | 913 | D1298 | 12.37 | | 0.14 |
| 150 | | ---- | | ---- | 922 | D1298 | 12.37 | | 0.14 |
| 158 | | ---- | | ---- | 962 | D1298 | 12.34 | | -0.03 |
| 159 | D4052 | 12.4 | | 0.31 | 963 | D1298 | 12.36 | | 0.08 |
| 168 | D287 | 12.2 | | -0.81 | 971 | ISO12185 | 12.41 | | 0.36 |
| 169 | D1298 | 12.0 | | -1.93 | 974 | Calc. | 12.42 | | 0.42 |
| 171 | D4052 | 12.3 | | -0.25 | 982 | D1298 | 12.35 | | 0.03 |
| 175 | D4052 | 12.33 | | -0.09 | 997 | D1250 | 12.05 | | -1.65 |
| 194 | D4052 | 12.3 | | -0.25 | 1006 | | ---- | | ---- |
| 212 | ISO12185 | 12.31 | | -0.20 | 1011 | | ---- | | ---- |
| 221 | | ---- | | ---- | 1059 | D4052 | 12.62 | | 1.54 |
| 224 | D1298 | 11.62 | C,R(0.01) | -4.06 | 1065 | | ---- | | ---- |
| 225 | | 12.45 | | 0.59 | 1082 | | ---- | | ---- |
| 237 | D4052 | 12.29 | | -0.31 | 1095 | | ---- | | ---- |
| 238 | D4052 | 12.32 | | -0.14 | 1099 | | ---- | | ---- |
| 252 | | ---- | | ---- | 1109 | D287 | 12.30 | | -0.25 |
| 253 | D4052 | 12.42 | | 0.42 | 1126 | | ---- | | ---- |
| 254 | | ---- | | ---- | 1134 | D1298 | 12.35 | | 0.03 |
| 273 | D4052 | 12.2 | C | -0.81 | 1135 | D4052 | 12.41 | | 0.36 |
| 311 | | ---- | | ---- | 1161 | | ---- | | ---- |
| 313 | | ---- | | ---- | 1167 | | ---- | | ---- |
| 323 | D1298 | 12.3 | | -0.25 | 1177 | | ---- | | ---- |
| 331 | ISO12185 | 12.35 | | 0.03 | 1191 | | ---- | | ---- |
| 333 | | ---- | | ---- | 1213 | | ---- | | ---- |
| 334 | | ---- | | ---- | 1229 | | ---- | | ---- |
| 336 | | ---- | | ---- | 1233 | | ---- | | ---- |
| 337 | | ---- | | ---- | 1254 | ISO12185 | 12.35 | | 0.03 |
| 342 | | ---- | | ---- | 1259 | ISO12185 | 12.15 | | -1.09 |
| 343 | D4052 | 12.38 | | 0.19 | 1275 | | ---- | | ---- |
| 349 | | ---- | | ---- | 1299 | | ---- | | ---- |
| 351 | | ---- | | ---- | 1345 | D1298 | 12.41 | | 0.36 |
| 371 | D1298 | 12.38 | | 0.19 | 1356 | | ---- | | ---- |
| 391 | D1298 | 12.39 | | 0.25 | 1367 | | ---- | | ---- |
| 398 | D1298 | 12.44 | | 0.53 | 1389 | | ---- | | ---- |
| 399 | D1298 | 12.4 | | 0.31 | 1402 | D4052 | 12.30 | | -0.25 |
| 440 | | ---- | | ---- | 1404 | | ---- | | ---- |
| 444 | | ---- | | ---- | 1412 | D4052 | 12.41 | | 0.36 |
| 445 | | ---- | | ---- | 1428 | | ---- | | ---- |
| 447 | D1250 | 12.52 | | 0.98 | 1431 | ISO12185 | 12.28 | | -0.37 |
| 463 | D1298 | 12.36 | | 0.08 | 1459 | | ---- | | ---- |
| 511 | | ---- | | ---- | 1488 | Calc. | 11.65 | C,R(0.01) | -3.89 |
| 541 | D4052 | 12.24 | | -0.59 | 1510 | | ---- | | ---- |
| 562 | D1298 | 12.5 | | 0.87 | 1539 | | ---- | | ---- |
| 575 | D1298 | 12.6 | | 1.43 | 1556 | | ---- | | ---- |
| 603 | | ---- | | ---- | 1569 | | ---- | | ---- |
| 604 | D4052 | 12.18 | | -0.93 | 1584 | ISO12185 | 12.345 | | 0.00 |
| 605 | D4052 | 12.25 | | -0.53 | 1586 | D1298 | 12.38 | | 0.19 |
| 608 | | ---- | | ---- | 1613 | D4052 | 12.33 | | -0.09 |
| 621 | | ---- | | ---- | 1622 | D4052 | 12.4 | | 0.31 |
| 631 | D1298 | 12.08 | | -1.49 | 1631 | | ---- | | ---- |
| 663 | | ---- | | ---- | 1643 | | ---- | | ---- |
| 671 | D287 | 12.4 | C | 0.31 | 1710 | | ---- | | ---- |
| 750 | D1298 | 12.4 | | 0.31 | 1720 | | ---- | | ---- |
| 753 | D1298 | 12.33 | | -0.09 | 1724 | D1298 | 12.5 | | 0.87 |
| 759 | D1298 | 12.375 | | 0.17 | 1728 | D287 | 12.530 | | 1.03 |
| 824 | D4052 | 12.38 | | 0.19 | 1740 | | ---- | | ---- |
| 825 | D4052 | 12.39 | | 0.25 | 1741 | | ---- | | ---- |
| 851 | | ---- | | ---- | 1796 | D1250 | 12.276 | | -0.39 |
| 855 | D1298 | 12.34 | | -0.03 | 1807 | | ---- | | ---- |
| 857 | | ---- | | ---- | 1832 | | ---- | | ---- |
| 858 | D1298 | 12.35 | | 0.03 | 1833 | | ---- | | ---- |
| 859 | D1298 | 12.32 | | -0.14 | 1849 | | ---- | | ---- |
| 862 | D287 | 12.28 | | -0.37 | 1857 | D1298 | 12.287 | | -0.33 |
| 863 | ISO12185 | 12.42 | | 0.42 | 1862 | D1250 | 12.35 | | 0.03 |
| 864 | ISO12185 | 12.4 | | 0.31 | 1881 | D4052 | 12.35 | | 0.03 |
| 865 | ISO12185 | 12.37 | | 0.14 | 1906 | | ---- | | ---- |
| 866 | ISO12185 | 12.32 | | -0.14 | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|----------|--------|------|---------|------|----------|--------|------|---------|
| 1937 | | ---- | | ---- | 6024 | D1250 | 12.29 | | -0.31 |
| 1938 | | ---- | | ---- | 6026 | D1298 | 12.33 | | -0.09 |
| 1943 | | ---- | | ---- | 6028 | D1298 | 12.49 | | 0.81 |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | D4052 | 12.405 | | 0.33 |
| 1964 | | ---- | | ---- | 6051 | D1250 | 12.35 | | 0.03 |
| 1967 | D1298 | 12.375 | | 0.17 | 6057 | ISO12185 | 12.41 | | 0.36 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | D4052 | 12.30 | | -0.25 | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | D1298 | 12.30 | | -0.25 | 6112 | | ---- | | ---- |
| 6016 | D4052 | 12.2 | | -0.81 | 6114 | D4052 | 12.329 | | -0.09 |
| 6021 | ISO12185 | 12.360 | | 0.08 | 6122 | | ---- | | ---- |

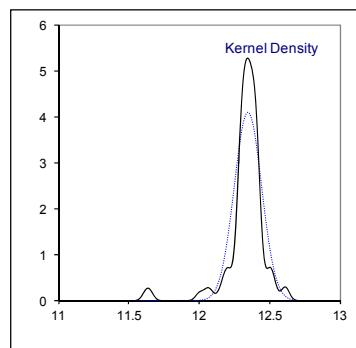
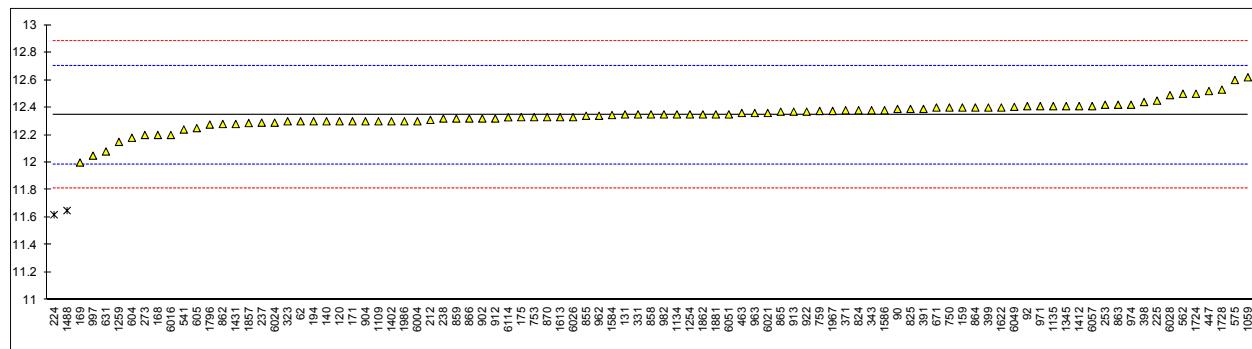
normality not OK
n 91
outliers 2
mean (n) 12.345
st.dev. (n) 0.0972
R(calc.) 0.272
R(D1298:12b) 0.5

Lab 224 first reported: 12.06

Lab 273 first reported: 11.7

Lab 671 first reported: 14.46

Lab 1488 first reported: 11.73



Determination of Ash Content on sample #17105; results in %M/M

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|---------|---------|---------|---------|------|---------|----------|---------|---------|
| 62 | D482 | 0.032 | | 4.41 | 870 | ISO6245 | 0.029 | | 2.73 |
| 90 | D482 | 0.0278 | | 2.06 | 886 | | ----- | | ----- |
| 92 | D482 | 0.030 | | 3.29 | 902 | ISO6245 | 0.027 | | 1.61 |
| 120 | D482 | 0.021 | | -1.75 | 904 | D482 | 0.022 | | -1.19 |
| 131 | | ----- | | ----- | 912 | D482 | 0.0295 | | 3.01 |
| 140 | ISO6245 | 0.017 | | -3.99 | 913 | ISO6245 | 0.0292 | | 2.85 |
| 150 | D482 | 0.026 | | 1.05 | 922 | D482 | 0.0206 | | -1.97 |
| 158 | | ----- | | ----- | 962 | ISO6245 | 0.01977 | | -2.43 |
| 159 | D482 | 0.022 | | -1.19 | 963 | ISO6245 | 0.025 | | 0.49 |
| 168 | | ----- | | ----- | 971 | D482 | 0.0245 | | 0.21 |
| 169 | D482 | 0.02068 | | -1.92 | 974 | D482 | 0.025 | | 0.49 |
| 171 | ISO6245 | 0.018 | | -3.43 | 982 | D482 | 0.021 | | -1.75 |
| 175 | D482 | 0.023 | | -0.63 | 997 | | ----- | | ----- |
| 194 | ISO6245 | 0.0242 | | 0.05 | 1006 | | ----- | | ----- |
| 212 | ISO6245 | 0.02 | | -2.31 | 1011 | ISO6245 | 0.025 | | 0.49 |
| 221 | D482 | 0.0278 | | 2.06 | 1059 | | ----- | | ----- |
| 224 | D482 | 0.0276 | | 1.95 | 1065 | D482 | 0.023625 | | -0.28 |
| 225 | D482 | 0.023 | | -0.63 | 1082 | | ----- | | ----- |
| 237 | D482 | 0.023 | C | -0.63 | 1095 | ISO6245 | 0.023 | | -0.63 |
| 238 | | ----- | | ----- | 1099 | | ----- | | ----- |
| 252 | D482 | 0.0249 | | 0.44 | 1109 | D482 | 0.0232 | | -0.51 |
| 253 | D482 | 0.025 | | 0.49 | 1126 | | ----- | | ----- |
| 254 | D482 | 0.024 | | -0.07 | 1134 | | ----- | | ----- |
| 273 | | ----- | | ----- | 1135 | ISO6245 | 0.02655 | | 1.36 |
| 311 | | ----- | | ----- | 1161 | | ----- | | ----- |
| 313 | | ----- | | ----- | 1167 | ISO6245 | 0.02393 | | -0.10 |
| 323 | ISO6245 | 0.018 | | -3.43 | 1177 | | ----- | | ----- |
| 331 | ISO6245 | 0.0250 | | 0.49 | 1191 | ISO6245 | 0.0248 | | 0.38 |
| 333 | | ----- | | ----- | 1213 | D482 | 0.0225 | | -0.91 |
| 334 | | ----- | | ----- | 1229 | | ----- | | ----- |
| 336 | | ----- | | ----- | 1233 | ISO6245 | 0.025 | | 0.49 |
| 337 | | ----- | | ----- | 1254 | D482 | 0.0215 | | -1.47 |
| 342 | ISO6245 | 0.025 | | 0.49 | 1259 | ISO6245 | 0.0269 | | 1.56 |
| 343 | ISO6245 | 0.021 | | -1.75 | 1275 | IP4 | 0.022 | | -1.19 |
| 349 | | ----- | | ----- | 1299 | D482 | <0.001 | C, f-? | <-12.79 |
| 351 | ISO6245 | 0.0234 | | -0.40 | 1345 | D482 | 0.0274 | | 1.84 |
| 371 | ISO6245 | 0.0222 | | -1.07 | 1356 | ISO6245 | 0.031 | | 3.85 |
| 391 | | ----- | | ----- | 1367 | IP4 | 0.024 | | -0.07 |
| 398 | | ----- | | ----- | 1389 | D482 | 0.022 | | -1.19 |
| 399 | | ----- | | ----- | 1402 | IP4 | 0.027 | | 1.61 |
| 440 | | ----- | | ----- | 1404 | ISO6245 | 0.020 | | -2.31 |
| 444 | D482 | 0.0168 | | -4.10 | 1412 | D482 | 0.027 | | 1.61 |
| 445 | IP4 | 0.015 | | -5.11 | 1428 | ISO6245 | 0.028 | | 2.17 |
| 447 | IP4 | 0.010 | R(0.05) | -7.91 | 1431 | D482 | 0.02452 | | 0.23 |
| 463 | ISO6245 | 0.0225 | | -0.91 | 1459 | | ----- | | ----- |
| 511 | | ----- | | ----- | 1488 | ISO6245 | 0.0224 | C | -0.96 |
| 541 | D482 | 0.0223 | | -1.02 | 1510 | | ----- | | ----- |
| 562 | D482 | 0.031 | | 3.85 | 1539 | ISO6245 | 0.025 | | 0.49 |
| 575 | | ----- | | ----- | 1556 | ISO6245 | 0.0249 | | 0.44 |
| 603 | | ----- | | ----- | 1569 | ISO6245 | 0.024 | | -0.07 |
| 604 | | ----- | | ----- | 1584 | | ----- | | ----- |
| 605 | D482 | 0.023 | | -0.63 | 1586 | ISO6245 | 0.020 | | -2.31 |
| 608 | | ----- | | ----- | 1613 | D482 | 0.022 | | -1.19 |
| 621 | | ----- | | ----- | 1622 | | ----- | | ----- |
| 631 | D482 | 0.0291 | | 2.79 | 1631 | | ----- | | ----- |
| 663 | D482 | 0.0228 | | -0.74 | 1643 | D482 | 0.0258 | | 0.94 |
| 671 | D482 | 0.016 | | -4.55 | 1710 | ISO6245 | 0.021 | | -1.75 |
| 750 | | ----- | | ----- | 1720 | | ----- | | ----- |
| 753 | D482 | 0.026 | | 1.05 | 1724 | D482 | 0.022 | | -1.19 |
| 759 | | ----- | | ----- | 1728 | ISO6245 | 0.024 | | -0.07 |
| 824 | ISO6245 | 0.025 | | 0.49 | 1740 | ISO6245 | 0.026 | | 1.05 |
| 825 | D482 | 0.025 | | 0.49 | 1741 | ISO6245 | 0.020 | | -2.31 |
| 851 | ISO6245 | 0.025 | | 0.49 | 1796 | ISO6245 | 0.02723 | | 1.74 |
| 855 | ISO6245 | 0.026 | | 1.05 | 1807 | ISO6245 | 0.0394 | R(0.01) | 8.56 |
| 857 | ISO6245 | 0.0259 | | 1.00 | 1832 | ISO6245 | 0.0220 | | -1.19 |
| 858 | D482 | 0.027 | | 1.61 | 1833 | | ----- | | ----- |
| 859 | D482 | 0.025 | | 0.49 | 1849 | ISO6245 | 0.026 | | 1.05 |
| 862 | ISO6245 | 0.0234 | | -0.40 | 1857 | D482 | 0.028 | | 2.17 |
| 863 | D482 | 0.0235 | | -0.35 | 1862 | ISO6245 | 0.0282 | | 2.29 |
| 864 | D482 | 0.025 | | 0.49 | 1881 | D482 | 0.0164 | | -4.32 |
| 865 | ISO6245 | 0.026 | | 1.05 | 1906 | | ----- | | ----- |
| 866 | D482 | 0.025 | | 0.49 | 1936 | | ----- | | ----- |

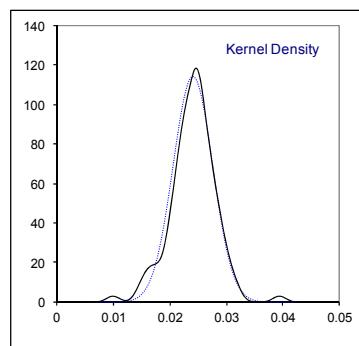
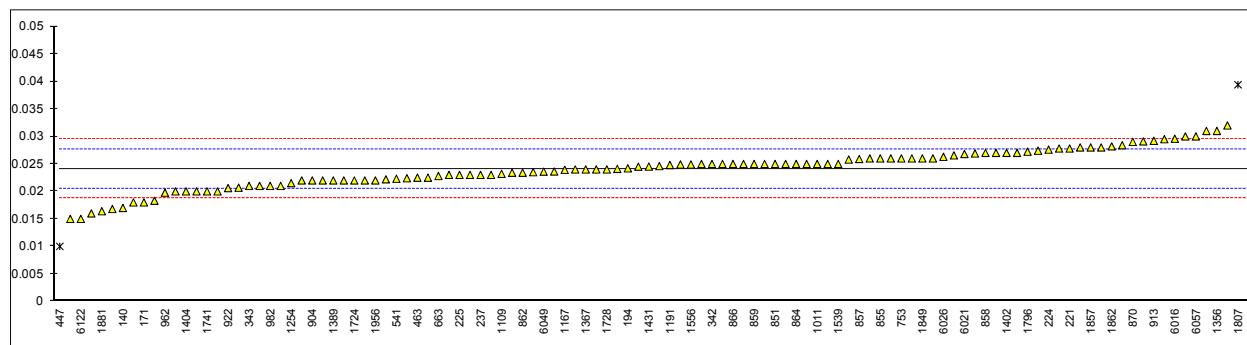
| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|---------|----------|------|---------|------|---------|--------|---------|---------|
| 1937 | | ---- | | ---- | 6024 | ISO6245 | 0.0284 | | 2.40 |
| 1938 | | ---- | | ---- | 6026 | D482 | 0.0263 | | 1.22 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | ISO6245 | 0.022 | | -1.19 | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | ISO6245 | 0.0236 | | -0.29 |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | D482 | 0.0246 | | 0.27 | 6057 | ISO6245 | 0.03 | | 3.29 |
| 1971 | | ---- | | ---- | 6075 | ISO6245 | 0.0183 | | -3.26 |
| 1986 | ISO6245 | 0.026 | | 1.05 | 6092 | ISO6245 | 0.028 | | 2.17 |
| 1995 | D482 | 0.02 | | -2.31 | 6109 | D482 | 4.780 | R(0.01) | 2663.29 |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | D482 | 0.029579 | | 3.06 | 6114 | D482 | 0.0241 | | -0.01 |
| 6021 | D482 | 0.0268 | | 1.50 | 6122 | ISO6245 | 0.0150 | | -5.11 |

normality OK
n 111
outliers 3
mean (n) 0.0241
st.dev. (n) 0.00349
R(calc.) 0.0098
R(ISO6245:01) 0.005

Lab 237 first reported: 0.002

Lab 1299 first reported: 0.00019/ possibly a false negative test result?

Lab 1488 first reported: 0.0022



Determination of Asphaltenes on sample #17105; results in %M/M

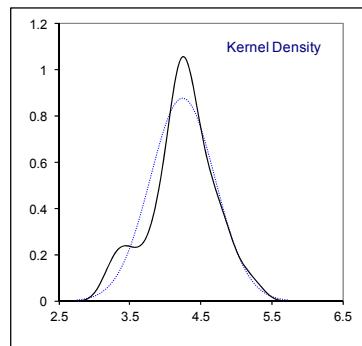
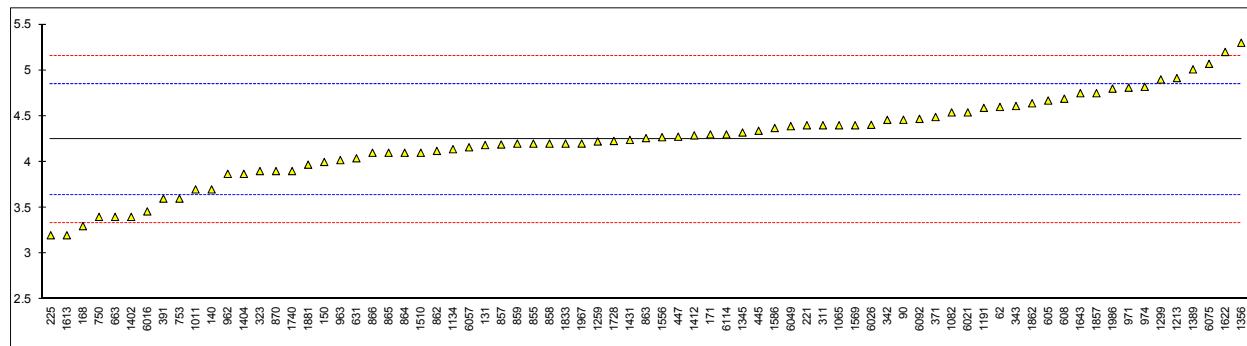
| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|--------|-------|------|---------|------|--------|--------|------|---------|
| 62 | IP143 | 4.6 | | 1.16 | 870 | IP143 | 3.90 | | -1.14 |
| 90 | IP143 | 4.46 | | 0.70 | 886 | | ---- | | ---- |
| 92 | | ---- | | ---- | 902 | | ---- | | ---- |
| 120 | | ---- | | ---- | 904 | | ---- | | ---- |
| 131 | D6560 | 4.184 | | -0.21 | 912 | | ---- | | ---- |
| 140 | IP143 | 3.7 | | -1.80 | 913 | | ---- | | ---- |
| 150 | IP143 | 4.0 | | -0.81 | 922 | | ---- | | ---- |
| 158 | | ---- | | ---- | 962 | IP143 | 3.87 | | -1.24 |
| 159 | | ---- | | ---- | 963 | IP143 | 4.02 | | -0.75 |
| 168 | D3279 | 3.3 | | -3.12 | 971 | IP143 | 4.81 | | 1.86 |
| 169 | | ---- | | ---- | 974 | IP143 | 4.82 | | 1.89 |
| 171 | IP143 | 4.3 | | 0.17 | 982 | | ---- | | ---- |
| 175 | | ---- | | ---- | 997 | | ---- | | ---- |
| 194 | | ---- | | ---- | 1006 | | ---- | | ---- |
| 212 | | ---- | | ---- | 1011 | IP143 | 3.7 | | -1.80 |
| 221 | D6560 | 4.4 | | 0.50 | 1059 | | ---- | | ---- |
| 224 | | ---- | | ---- | 1065 | IP143 | 4.40 | | 0.50 |
| 225 | D6560 | 3.2 | | -3.45 | 1082 | IP143 | 4.54 | | 0.97 |
| 237 | | ---- | | ---- | 1095 | | ---- | | ---- |
| 238 | | ---- | | ---- | 1099 | | ---- | | ---- |
| 252 | | ---- | | ---- | 1109 | | ---- | | ---- |
| 253 | | ---- | | ---- | 1126 | | ---- | | ---- |
| 254 | | ---- | | ---- | 1134 | IP143 | 4.1387 | | -0.36 |
| 273 | | ---- | | ---- | 1135 | | ---- | | ---- |
| 311 | IP143 | 4.4 | | 0.50 | 1161 | | ---- | | ---- |
| 313 | | ---- | | ---- | 1167 | | ---- | | ---- |
| 323 | IP143 | 3.9 | | -1.14 | 1177 | | ---- | | ---- |
| 331 | | ---- | | ---- | 1191 | IP143 | 4.59 | | 1.13 |
| 333 | | ---- | | ---- | 1213 | D6560 | 4.915 | | 2.20 |
| 334 | | ---- | | ---- | 1229 | | ---- | | ---- |
| 336 | | ---- | | ---- | 1233 | | ---- | | ---- |
| 337 | | ---- | | ---- | 1254 | | ---- | | ---- |
| 342 | IP143 | 4.459 | | 0.70 | 1259 | D6560 | 4.223 | | -0.08 |
| 343 | IP143 | 4.61 | | 1.20 | 1275 | | ---- | | ---- |
| 349 | | ---- | | ---- | 1299 | IP143 | 4.90 | | 2.15 |
| 351 | | ---- | | ---- | 1345 | IP143 | 4.321 | | 0.24 |
| 371 | IP143 | 4.49 | | 0.80 | 1356 | D6560 | 5.3 | | 3.47 |
| 391 | IP143 | 3.6 | | -2.13 | 1367 | | ---- | | ---- |
| 398 | | ---- | | ---- | 1389 | IP143 | 5.01 | | 2.52 |
| 399 | | ---- | | ---- | 1402 | IP143 | 3.4 | | -2.79 |
| 440 | | ---- | | ---- | 1404 | IP143 | 3.87 | | -1.24 |
| 444 | | ---- | | ---- | 1412 | D6560 | 4.29 | | 0.14 |
| 445 | IP143 | 4.34 | | 0.31 | 1428 | | ---- | | ---- |
| 447 | IP143 | 4.275 | | 0.09 | 1431 | D6560 | 4.24 | | -0.02 |
| 463 | | ---- | | ---- | 1459 | | ---- | | ---- |
| 511 | | ---- | | ---- | 1488 | | ---- | | ---- |
| 541 | | ---- | | ---- | 1510 | IP143 | 4.1 | | -0.48 |
| 562 | | ---- | | ---- | 1539 | | ---- | | ---- |
| 575 | | ---- | | ---- | 1556 | IP143 | 4.27 | | 0.08 |
| 603 | | ---- | | ---- | 1569 | IP143 | 4.4 | | 0.50 |
| 604 | | ---- | | ---- | 1584 | | ---- | | ---- |
| 605 | IP143 | 4.67 | | 1.39 | 1586 | IP143 | 4.37 | | 0.41 |
| 608 | IP143 | 4.69 | | 1.46 | 1613 | IP143 | 3.2 | | -3.45 |
| 621 | | ---- | | ---- | 1622 | IP143 | 5.2 | C | 3.14 |
| 631 | D6560 | 4.04 | | -0.68 | 1631 | | ---- | | ---- |
| 663 | IP143 | 3.40 | | -2.79 | 1643 | D6560 | 4.75 | | 1.66 |
| 671 | | ---- | | ---- | 1710 | | ---- | W | ---- |
| 750 | IP143 | 3.4 | | -2.79 | 1720 | | ---- | | ---- |
| 753 | IP143 | 3.60 | | -2.13 | 1724 | | ---- | | ---- |
| 759 | | ---- | | ---- | 1728 | IP143 | 4.229 | | -0.06 |
| 824 | | ---- | | ---- | 1740 | IP143 | 3.9 | | -1.14 |
| 825 | | ---- | | ---- | 1741 | | ---- | | ---- |
| 851 | | ---- | | ---- | 1796 | | ---- | | ---- |
| 855 | IP143 | 4.20 | | -0.15 | 1807 | | ---- | | ---- |
| 857 | IP143 | 4.19 | | -0.19 | 1832 | | ---- | | ---- |
| 858 | IP143 | 4.2 | | -0.15 | 1833 | IP143 | 4.2 | | -0.15 |
| 859 | IP143 | 4.2 | | -0.15 | 1849 | | ---- | | ---- |
| 862 | IP143 | 4.12 | | -0.42 | 1857 | IP143 | 4.75 | | 1.66 |
| 863 | IP143 | 4.26 | | 0.04 | 1862 | IP143 | 4.64 | | 1.30 |
| 864 | IP143 | 4.1 | | -0.48 | 1881 | IP143 | 3.97 | C | -0.91 |
| 865 | IP143 | 4.10 | | -0.48 | 1906 | | ---- | | ---- |
| 866 | IP143 | 4.1 | | -0.48 | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-------------|--------|--------|------|---------|------|-------------|-------|------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | IP143 | 4.405 | | 0.52 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | IP143 | 4.39 | | 0.47 |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | IP143 | 4.2005 | | -0.15 | 6057 | IP143 | 4.16 | | -0.29 |
| 1971 | | ---- | | ---- | 6075 | NF T 60-115 | 5.07 | | 2.71 |
| 1986 | IP143 | 4.8 | | 1.82 | 6092 | IP143 | 4.47 | | 0.74 |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | IP143 | 3.46 | | -2.59 | 6114 | IP143 | 4.30 | | 0.17 |
| 6021 | IP143 | 4.54 | | 0.97 | 6122 | | ---- | | ---- |
| normality | | OK | | | | | | | |
| n | | 75 | | | | | | | |
| outliers | | 0 | | | | | | | |
| mean (n) | | 4.247 | | | | | | | |
| st.dev. (n) | | 0.4558 | | | | | | | |
| R(calc.) | | 1.276 | | | | | | | |
| R(IP143:04) | | 0.849 | | | | | | | |

Lab 1622 first reported: 10.5357

Lab 1710 first reported: 2.85

Lab 1881 first reported: 5.53



Determination of Calculated Carbon Aromaticity Index on sample #17105

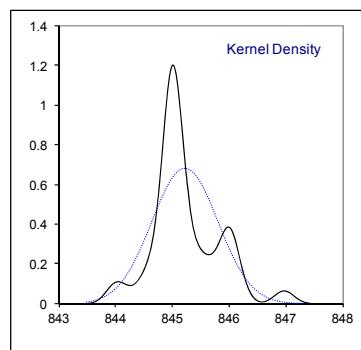
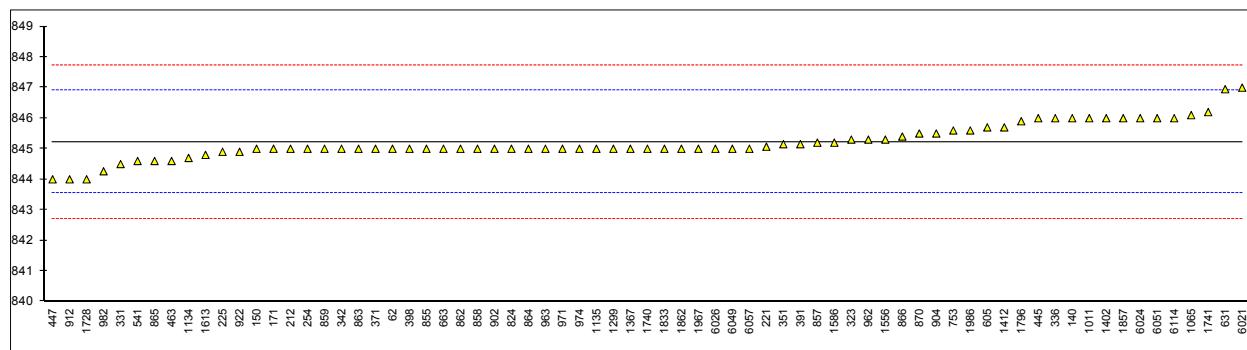
| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|---------|---------|------|---------|------|---------|---------|------|---------|
| 62 | ISO8217 | 845 | | -0.26 | 870 | ISO8217 | 845.5 | | 0.33 |
| 90 | | ----- | | ----- | 886 | | ----- | | ----- |
| 92 | | ----- | | ----- | 902 | ISO8217 | 845 | | -0.26 |
| 120 | | ----- | | ----- | 904 | ISO8217 | 845.5 | | 0.33 |
| 131 | | ----- | | ----- | 912 | ISO8217 | 844 | | -1.45 |
| 140 | ISO8217 | 846 | | 0.93 | 913 | | ----- | | ----- |
| 150 | ISO8217 | 845 | | -0.26 | 922 | ISO8217 | 844.9 | | -0.38 |
| 158 | | ----- | | ----- | 962 | ISO8217 | 845.3 | | 0.09 |
| 159 | | ----- | | ----- | 963 | ISO8217 | 845 | | -0.26 |
| 168 | | ----- | | ----- | 971 | ISO8217 | 845 | | -0.26 |
| 169 | | ----- | | ----- | 974 | ISO8217 | 845 | | -0.26 |
| 171 | ISO8217 | 845 | | -0.26 | 982 | ISO8217 | 844.263 | | -1.14 |
| 175 | | ----- | | ----- | 997 | | ----- | | ----- |
| 194 | | ----- | | ----- | 1006 | | ----- | | ----- |
| 212 | ISO8217 | 845 | | -0.26 | 1011 | ISO8217 | 846 | | 0.93 |
| 221 | ISO8217 | 845.067 | | -0.18 | 1059 | | ----- | | ----- |
| 224 | | ----- | | ----- | 1065 | ISO8217 | 846.1 | | 1.05 |
| 225 | ISO8217 | 844.9 | | -0.38 | 1082 | | ----- | | ----- |
| 237 | | ----- | | ----- | 1095 | | ----- | | ----- |
| 238 | | ----- | | ----- | 1099 | | ----- | | ----- |
| 252 | | ----- | | ----- | 1109 | | ----- | | ----- |
| 253 | | ----- | | ----- | 1126 | | ----- | | ----- |
| 254 | ISO8217 | 845 | | -0.26 | 1134 | ISO8217 | 844.7 | | -0.62 |
| 273 | | ----- | | ----- | 1135 | ISO8217 | 845 | | -0.26 |
| 311 | | ----- | | ----- | 1161 | | ----- | | ----- |
| 313 | | ----- | | ----- | 1167 | | ----- | | ----- |
| 323 | ISO8217 | 845.3 | C | 0.09 | 1177 | | ----- | | ----- |
| 331 | ISO8217 | 844.5 | | -0.86 | 1191 | | ----- | | ----- |
| 333 | | ----- | | ----- | 1213 | | ----- | | ----- |
| 334 | | ----- | | ----- | 1229 | | ----- | | ----- |
| 336 | ISO8217 | 846 | | 0.93 | 1233 | | ----- | | ----- |
| 337 | | ----- | | ----- | 1254 | | ----- | | ----- |
| 342 | ISO8217 | 845 | | -0.26 | 1259 | | ----- | | ----- |
| 343 | | ----- | | ----- | 1275 | | ----- | | ----- |
| 349 | | ----- | | ----- | 1299 | ISO8217 | 845 | | -0.26 |
| 351 | ISO8217 | 845.15 | | -0.08 | 1345 | | ----- | | ----- |
| 371 | ISO8217 | 845 | C | -0.26 | 1356 | | ----- | | ----- |
| 391 | ISO8217 | 845.15 | | -0.08 | 1367 | ISO8217 | 845.0 | | -0.26 |
| 398 | ISO8217 | 845 | | -0.26 | 1389 | | ----- | | ----- |
| 399 | | ----- | | ----- | 1402 | ISO8217 | 846 | | 0.93 |
| 440 | | ----- | | ----- | 1404 | | ----- | | ----- |
| 444 | | ----- | | ----- | 1412 | ISO8217 | 845.7 | | 0.57 |
| 445 | ISO8217 | 846 | | 0.93 | 1428 | | ----- | | ----- |
| 447 | ISO8217 | 844 | | -1.45 | 1431 | | ----- | | ----- |
| 463 | ISO8217 | 844.6 | | -0.74 | 1459 | | ----- | | ----- |
| 511 | | ----- | | ----- | 1488 | | ----- | | ----- |
| 541 | ISO8217 | 844.6 | | -0.74 | 1510 | | ----- | | ----- |
| 562 | | ----- | | ----- | 1539 | | ----- | | ----- |
| 575 | | ----- | | ----- | 1556 | ISO8217 | 845.3 | | 0.09 |
| 603 | | ----- | | ----- | 1569 | | ----- | | ----- |
| 604 | | ----- | | ----- | 1584 | | ----- | | ----- |
| 605 | ISO8217 | 845.7 | | 0.57 | 1586 | ISO8217 | 845.2 | | -0.02 |
| 608 | | ----- | | ----- | 1613 | ISO8217 | 844.8 | | -0.50 |
| 621 | | ----- | | ----- | 1622 | | ----- | | ----- |
| 631 | ISO8217 | 846.95 | | 2.06 | 1631 | | ----- | | ----- |
| 663 | ISO8217 | 845 | | -0.26 | 1643 | | ----- | | ----- |
| 671 | | ----- | | ----- | 1710 | | ----- | | ----- |
| 750 | | ----- | | ----- | 1720 | | ----- | | ----- |
| 753 | ISO8217 | 845.6 | | 0.45 | 1724 | | ----- | | ----- |
| 759 | | ----- | | ----- | 1728 | ISO8217 | 844 | | -1.45 |
| 824 | ISO8217 | 845 | | -0.26 | 1740 | ISO8217 | 845 | | -0.26 |
| 825 | | ----- | | ----- | 1741 | ISO8217 | 846.20 | | 1.17 |
| 851 | | ----- | | ----- | 1796 | ISO8217 | 845.9 | | 0.81 |
| 855 | ISO8217 | 845 | | -0.26 | 1807 | | ----- | | ----- |
| 857 | ISO8217 | 845.2 | | -0.02 | 1832 | | ----- | | ----- |
| 858 | ISO8217 | 845 | | -0.26 | 1833 | ISO8217 | 845 | | -0.26 |
| 859 | ISO8217 | 845 | | -0.26 | 1849 | | ----- | | ----- |
| 862 | ISO8217 | 845 | | -0.26 | 1857 | ISO8217 | 846 | | 0.93 |
| 863 | ISO8217 | 845 | | -0.26 | 1862 | ISO8217 | 845 | | -0.26 |
| 864 | ISO8217 | 845 | | -0.26 | 1881 | | ----- | | ----- |
| 865 | ISO8217 | 844.6 | | -0.74 | 1906 | | ----- | | ----- |
| 866 | ISO8217 | 845.4 | | 0.21 | 1936 | | ----- | | ----- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|---------|-------|------|---------|------|---------|-------|------|---------|
| 1937 | | ---- | | ---- | 6024 | ISO8217 | 846 | | 0.93 |
| 1938 | | ---- | | ---- | 6026 | ISO8217 | 845 | | -0.26 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | ISO8217 | 845 | | -0.26 |
| 1964 | | ---- | | ---- | 6051 | ISO8217 | 846 | | 0.93 |
| 1967 | ISO8217 | 845 | | -0.26 | 6057 | ISO8217 | 845 | | -0.26 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | ISO8217 | 845.6 | | 0.45 | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | | ---- | | ---- | 6114 | ISO8217 | 846 | | 0.93 |
| 6021 | ISO8217 | 847 | | 2.12 | 6122 | | ---- | | ---- |

normality suspect
n 71
outliers 0
mean (n) 845.221
st.dev. (n) 0.5853
R(calc.) 1.639
R(ISO8217:12) 2.35

Lab 323 first reported: 848

Lab 371 first reported: 35.3

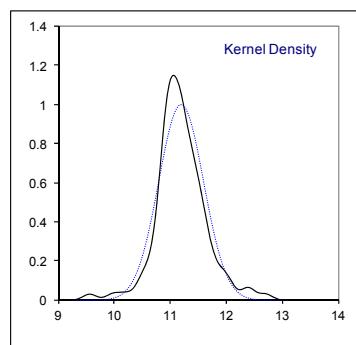
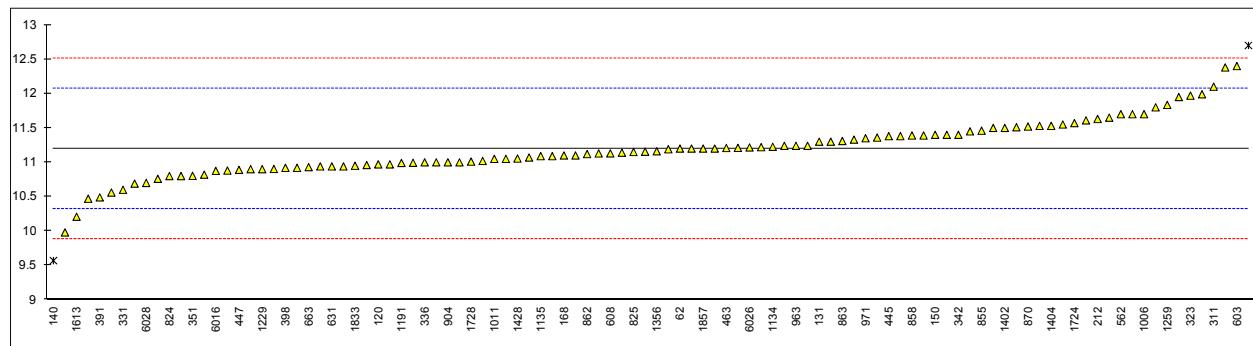


Determination of Carbon Residue - micro method on sample #17105; results in %M/M

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|----------|--------|---------|---------|------|----------|---------|------|---------|
| 62 | D4530 | 11.2 | | 0.01 | 870 | ISO10370 | 11.52 | | 0.74 |
| 90 | ---- | ---- | | ---- | 886 | D4530 | 11.8 | | 1.38 |
| 92 | D4530 | 10.47 | | -1.66 | 902 | ISO10370 | 11.0 | | -0.45 |
| 120 | D4530 | 10.97 | | -0.52 | 904 | D4530 | 11.0 | | -0.45 |
| 131 | D4530 | 11.30 | | 0.24 | 912 | ISO10370 | 11.61 | | 0.94 |
| 140 | ISO10370 | 9.57 | R(0.05) | -3.71 | 913 | D4530 | 11.95 | | 1.72 |
| 150 | D4530 | 11.4 | | 0.46 | 922 | | ---- | | ---- |
| 158 | ---- | ---- | | ---- | 962 | | ---- | | ---- |
| 159 | D4530 | 12.7 | R(0.05) | 3.43 | 963 | ISO10370 | 11.24 | | 0.10 |
| 168 | D4530 | 11.1 | | -0.22 | 971 | D4530 | 11.35 | | 0.35 |
| 169 | ---- | ---- | | ---- | 974 | D4530 | 11.33 | | 0.30 |
| 171 | ISO10370 | 10.76 | | -1.00 | 982 | | ---- | | ---- |
| 175 | ---- | ---- | | ---- | 997 | | ---- | | ---- |
| 194 | D4530 | 10.903 | | -0.67 | 1006 | D4530 | 11.7 | | 1.15 |
| 212 | ISO10370 | 11.63 | | 0.99 | 1011 | ISO10370 | 11.05 | | -0.34 |
| 221 | ---- | ---- | | ---- | 1059 | ISO10370 | 11.19 | | -0.02 |
| 224 | ---- | ---- | | ---- | 1065 | | ---- | | ---- |
| 225 | ---- | ---- | | ---- | 1082 | | ---- | | ---- |
| 237 | ---- | ---- | | ---- | 1095 | ISO10370 | 10.88 | | -0.72 |
| 238 | ---- | ---- | | ---- | 1099 | | ---- | | ---- |
| 252 | D4530 | 10.94 | | -0.59 | 1109 | D4530 | 10.97 | | -0.52 |
| 253 | ---- | ---- | | ---- | 1126 | | ---- | | ---- |
| 254 | ---- | ---- | | ---- | 1134 | D4530 | 11.226 | | 0.07 |
| 273 | ---- | ---- | | ---- | 1135 | ISO10370 | 11.09 | | -0.24 |
| 311 | D4530 | 12.1 | | 2.06 | 1161 | | ---- | | ---- |
| 313 | ---- | ---- | | ---- | 1167 | | ---- | | ---- |
| 323 | ISO10370 | 11.97 | | 1.76 | 1177 | | ---- | | ---- |
| 331 | ISO10370 | 10.60 | | -1.36 | 1191 | ISO10370 | 10.99 | | -0.47 |
| 333 | ---- | ---- | | ---- | 1213 | D4530 | 11.07 | | -0.29 |
| 334 | ISO10370 | 10.69 | | -1.16 | 1229 | ISO10370 | 10.9 | | -0.68 |
| 336 | ISO10370 | 11.00 | | -0.45 | 1233 | ISO10370 | 11.36 | | 0.37 |
| 337 | ---- | ---- | | ---- | 1254 | D4530 | 11.129 | | -0.15 |
| 342 | ISO10370 | 11.40 | C | 0.46 | 1259 | ISO10370 | 11.8346 | | 1.46 |
| 343 | ISO10370 | 11.24 | | 0.10 | 1275 | | ---- | | ---- |
| 349 | ---- | ---- | | ---- | 1299 | D4530 | 11.02 | | -0.40 |
| 351 | ISO10370 | 10.803 | | -0.90 | 1345 | | ---- | | ---- |
| 371 | ---- | ---- | | ---- | 1356 | ISO10370 | 11.16 | | -0.08 |
| 391 | ISO10370 | 10.49 | | -1.61 | 1367 | IP398 | 11.53 | | 0.76 |
| 398 | ISO10370 | 10.92 | | -0.63 | 1389 | | ---- | | ---- |
| 399 | ---- | ---- | | ---- | 1402 | IP398 | 11.5 | | 0.69 |
| 440 | ---- | ---- | | ---- | 1404 | ISO10370 | 11.53 | | 0.76 |
| 444 | ---- | ---- | | ---- | 1412 | | ---- | | ---- |
| 445 | IP398 | 11.38 | | 0.42 | 1428 | ISO10370 | 11.055 | | -0.32 |
| 447 | IP398 | 10.89 | | -0.70 | 1431 | D4530 | 11.14 | | -0.13 |
| 463 | ISO10370 | 11.208 | | 0.03 | 1459 | | ---- | | ---- |
| 511 | ---- | ---- | | ---- | 1488 | | ---- | | ---- |
| 541 | ---- | ---- | | ---- | 1510 | D4530 | 11.2 | | 0.01 |
| 562 | D4530 | 11.7 | | 1.15 | 1539 | ISO10370 | 11.45 | | 0.58 |
| 575 | ---- | ---- | | ---- | 1556 | ISO10370 | 10.96 | | -0.54 |
| 603 | D4530 | 12.4 | | 2.75 | 1569 | ISO10370 | 11.39 | | 0.44 |
| 604 | ---- | ---- | | ---- | 1584 | | ---- | | ---- |
| 605 | D4530 | 10.9 | | -0.68 | 1586 | ISO10370 | 11.09 | | -0.24 |
| 608 | D4530 | 11.13 | | -0.15 | 1613 | D4530 | 10.208 | | -2.26 |
| 621 | ---- | ---- | | ---- | 1622 | D4530 | 10.9925 | | -0.47 |
| 631 | D4530 | 10.94 | | -0.59 | 1631 | | ---- | | ---- |
| 663 | D4530 | 10.93 | | -0.61 | 1643 | | ---- | | ---- |
| 671 | ---- | ---- | | ---- | 1710 | ISO10370 | 11.55 | | 0.81 |
| 750 | ISO10370 | 11.99 | | 1.81 | 1720 | D4530 | 9.98 | | -2.78 |
| 753 | ---- | ---- | | ---- | 1724 | D4530 | 11.57 | | 0.85 |
| 759 | ---- | ---- | | ---- | 1728 | ISO10370 | 11.01 | | -0.43 |
| 824 | ISO10370 | 10.80 | | -0.91 | 1740 | ISO10370 | 11 | | -0.45 |
| 825 | D4530 | 11.15 | | -0.11 | 1741 | ISO10370 | 11.380 | | 0.42 |
| 851 | ISO10370 | 10.94 | | -0.59 | 1796 | | ---- | | ---- |
| 855 | D4530 | 11.46 | | 0.60 | 1807 | ISO10370 | 10.80 | | -0.91 |
| 857 | ISO10370 | 11.50 | | 0.69 | 1832 | | ---- | | ---- |
| 858 | D4530 | 11.39 | | 0.44 | 1833 | ISO10370 | 10.95 | | -0.56 |
| 859 | D4530 | 11.7 | | 1.15 | 1849 | | ---- | | ---- |
| 862 | ISO10370 | 11.12 | | -0.18 | 1857 | ISO10370 | 11.2 | | 0.01 |
| 863 | D4530 | 11.31 | | 0.26 | 1862 | ISO10370 | 11.1 | | -0.22 |
| 864 | D4530 | 11.24 | | 0.10 | 1881 | ISO10370 | 12.38 | | 2.70 |
| 865 | ISO10370 | 11.21 | | 0.03 | 1906 | | ---- | | ---- |
| 866 | D4530 | 11.4 | | 0.46 | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|----------------|----------|---------|------|---------|------|----------|--------|------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | D4530 | 11.216 | | 0.04 |
| 1943 | | ---- | | ---- | 6028 | ISO10370 | 10.7 | | -1.13 |
| 1956 | ISO10370 | 11.51 | | 0.71 | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | ISO10370 | 11.22 | | 0.05 |
| 1964 | | ---- | | ---- | 6051 | D4530 | 11.3 | | 0.24 |
| 1967 | D4530 | 11.154 | | -0.10 | 6057 | ISO10370 | 10.82 | | -0.86 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | ISO10370 | 11.2 | | 0.01 | 6092 | | ---- | | ---- |
| 1995 | D4530 | 11.65 | | 1.03 | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | D4530 | 10.8751 | | -0.73 | 6114 | ISO10370 | 10.920 | | -0.63 |
| 6021 | ISO10370 | 11.05 | | -0.34 | 6122 | ISO10370 | 10.56 | | -1.45 |
| normality | | suspect | | | | | | | |
| n | | 102 | | | | | | | |
| outliers | | 2 | | | | | | | |
| mean (n) | | 11.1969 | | | | | | | |
| st.dev. (n) | | 0.39975 | | | | | | | |
| R(calc.) | | 1.1193 | | | | | | | |
| R(ISO10370:14) | | 1.2267 | | | | | | | |

Lab 342 first reported: 13.07



Determination of Conradson Carbon Residue on sample #17105; results in %M/M

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|---------|-------|-----------|---------|---------|---------|-------|-------|---------|
| 62 | | ---- | | ---- | 870 | D189 | 11.50 | | 0.09 |
| 90 | | ---- | | ---- | 886 | | ---- | | ---- |
| 92 | | ---- | | ---- | 902 | | ---- | | ---- |
| 120 | | ---- | | ---- | 904 | D189 | 11.5 | | 0.09 |
| 131 | | ---- | | ---- | 912 | D189 | 11.04 | | -0.61 |
| 140 | | ---- | | ---- | 913 | D189 | 11.15 | | -0.44 |
| 150 | | ---- | | ---- | 922 | D189 | 11.75 | | 0.48 |
| 158 | | ---- | | ---- | 962 | D189 | 11.56 | | 0.19 |
| 159 | | ---- | | ---- | 963 | D189 | 11.42 | | -0.03 |
| 168 | | ---- | | ---- | 971 | D189 | 11.45 | | 0.02 |
| 169 | | ---- | | ---- | 974 | D189 | 11.35 | | -0.14 |
| 171 | D189 | 11.0 | | -0.68 | 982 | D189 | 11.11 | | -0.51 |
| 175 | | ---- | | ---- | 997 | D189 | 11.58 | C | 0.22 |
| 194 | | ---- | | 1006 | | ---- | | ---- | ---- |
| 212 | | 11.56 | | 0.19 | 1011 | | ---- | | ---- |
| 221 | | ---- | | 1059 | | ---- | | ---- | ---- |
| 224 | D189 | 11.95 | | 0.79 | 1065 | | ---- | | ---- |
| 225 | D4530 | 11.1 | | -0.52 | 1082 | | ---- | | ---- |
| 237 | D189 | 10.62 | | -1.26 | 1095 | | ---- | | ---- |
| 238 | | ---- | | 1099 | | ---- | | ---- | ---- |
| 252 | | ---- | | 1109 | | ---- | | ---- | ---- |
| 253 | D189 | 12.00 | | 0.86 | 1126 | | ---- | | ---- |
| 254 | D189 | 10.96 | | -0.74 | 1134 | | ---- | | ---- |
| 273 | D4530 | 10.66 | | -1.20 | 1135 | | ---- | | ---- |
| 311 | | ---- | | 1161 | | ---- | | ---- | ---- |
| 313 | | ---- | | 1167 | | ---- | | ---- | ---- |
| 323 | | ---- | | 1177 | | ---- | | ---- | ---- |
| 331 | | ---- | | 1191 | | ---- | | ---- | ---- |
| 333 | | ---- | | 1213 | | ---- | | ---- | ---- |
| 334 | | ---- | | 1229 | | ---- | | ---- | ---- |
| 336 | | ---- | | 1233 | | ---- | | ---- | ---- |
| 337 | | ---- | | 1254 | D189 | 11.682 | | 0.37 | 0.37 |
| 342 | | ---- | | 1259 | | ---- | | ---- | ---- |
| 343 | | ---- | | 1275 | | ---- | | ---- | ---- |
| 349 | | ---- | | 1299 | | ---- | | ---- | ---- |
| 351 | | ---- | | 1345 | D189 | 11.662 | | 0.34 | 0.34 |
| 371 | D189 | 11.63 | | 0.29 | 1356 | | ---- | | ---- |
| 391 | | ---- | | 1367 | | ---- | | ---- | ---- |
| 398 | | ---- | | 1389 | D4530 | 11.04 | | -0.61 | 0.00 |
| 399 | | ---- | | 1402 | D189 | 12.20 | | 1.17 | 0.00 |
| 440 | | ---- | | 1404 | | ---- | | ---- | ---- |
| 444 | | ---- | | 1412 | D189 | 11.52 | | 0.13 | 0.00 |
| 445 | IP13 | 11.27 | | -0.26 | 1428 | | ---- | | ---- |
| 447 | | ---- | | 1431 | | ---- | | ---- | ---- |
| 463 | | ---- | | 1459 | | ---- | | ---- | ---- |
| 511 | | ---- | | 1488 | ISO6615 | 11.60 | | 0.25 | 0.00 |
| 541 | D189 | 10.63 | C | -1.24 | 1510 | | ---- | | 0.00 |
| 562 | D189 | 12.1 | | 1.02 | 1539 | ISO6615 | 12.26 | | 1.26 |
| 575 | D189 | 13.11 | C,R(0.05) | 2.57 | 1556 | | ---- | | 0.00 |
| 603 | | ---- | | 1569 | | ---- | | ---- | ---- |
| 604 | | ---- | | 1584 | | ---- | | ---- | ---- |
| 605 | | ---- | | 1586 | D189 | 11.53 | | 0.14 | 0.00 |
| 608 | | ---- | | 1613 | D189 | 10.51 | | -1.43 | 0.00 |
| 621 | | ---- | | 1622 | D189 | 12.6463 | | 1.86 | 0.00 |
| 631 | | ---- | | 1631 | | ---- | | ---- | ---- |
| 663 | | ---- | | 1643 | D189 | 11.577 | | 0.21 | 0.00 |
| 671 | | ---- | | 1710 | | ---- | | ---- | ---- |
| 750 | | ---- | | 1720 | | ---- | | ---- | ---- |
| 753 | | ---- | | 1724 | | ---- | | ---- | ---- |
| 759 | | ---- | | 1728 | D189 | 10.89 | | -0.84 | 0.00 |
| 824 | | ---- | | 1740 | D189 | 11.1 | | -0.52 | 0.00 |
| 825 | | ---- | | 1741 | | ---- | | ---- | ---- |
| 851 | | ---- | | 1796 | | ---- | | ---- | ---- |
| 855 | | ---- | | 1807 | | ---- | | ---- | ---- |
| 857 | | ---- | | 1832 | ISO6615 | 11.452 | | 0.02 | 0.00 |
| 858 | | ---- | | 1833 | | ---- | | ---- | ---- |
| 859 | | ---- | | 1849 | | ---- | | ---- | ---- |
| 862 | D189 | 11.37 | | -0.11 | 1857 | | ---- | | 0.00 |
| 863 | | ---- | | 1862 | D189 | 11.6 | | 0.25 | 0.00 |
| 864 | | ---- | | 1881 | | ---- | | ---- | ---- |
| 865 | ISO6615 | 11.24 | | -0.31 | 1906 | | ---- | | 0.00 |
| 866 | | ---- | | 1936 | | ---- | | ---- | ---- |

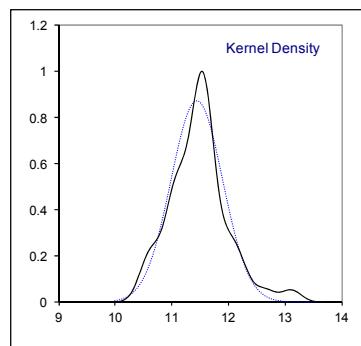
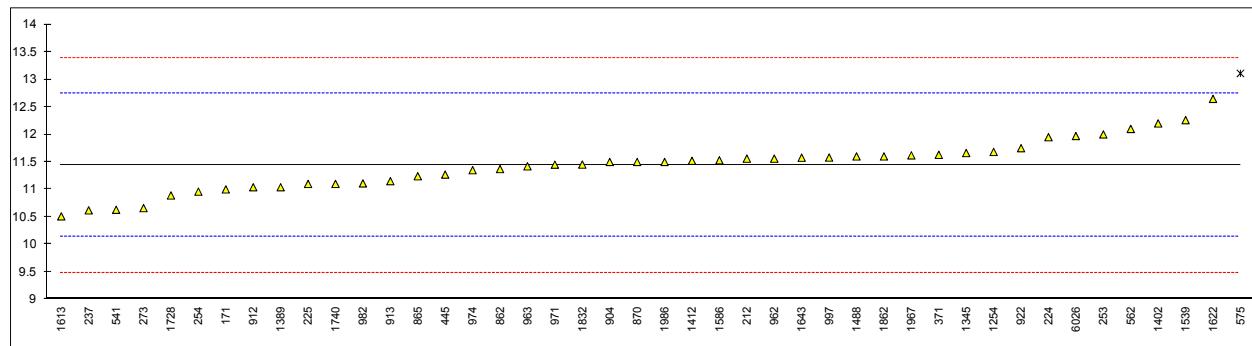
| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|--------|---------|------|---------|------|--------|--------|------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | D189 | 11.971 | | 0.82 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | | ---- | | ---- |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | D189 | 11.6194 | | 0.28 | 6057 | | ---- | | ---- |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | D189 | 11.5 | | 0.09 | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | | ---- | | ---- | 6114 | | ---- | | ---- |
| 6021 | | ---- | | ---- | 6122 | | ---- | | ---- |

normality OK
n 43
outliers 1
mean (n) 11.4386
st.dev. (n) 0.45689
R(calc.) 1.2793
R(D189:06) 1.8189

Lab 541 first reported: 9.634

Lab 575 first reported: 13.32

Lab 997 first reported: 13.8



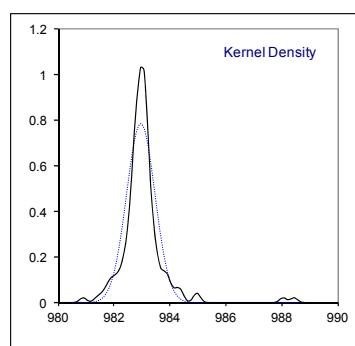
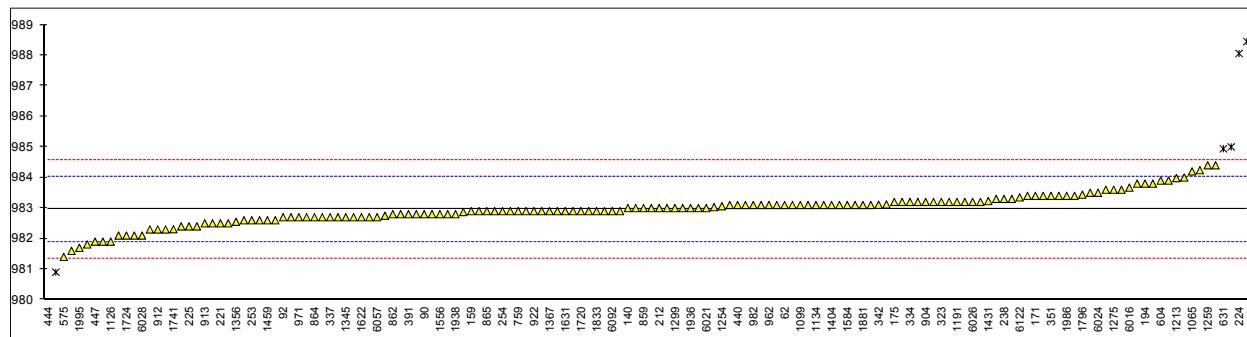
Determination of Density at 15°C on sample #17105; results in kg/m³

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|----------|--------|-----------|---------|------|----------|--------|-----------|---------|
| 62 | D4052 | 983.1 | | 0.25 | 870 | D1298 | 983.2 | | 0.44 |
| 90 | D4052 | 982.8 | | -0.31 | 886 | | ---- | | ---- |
| 92 | D4052 | 982.7 | | -0.49 | 902 | ISO12185 | 982.9 | | -0.12 |
| 120 | ISO12185 | 983.4 | | 0.81 | 904 | D4052 | 983.2 | | 0.44 |
| 131 | D4052 | 983.10 | | 0.25 | 912 | D1298 | 982.3 | | -1.24 |
| 140 | D4052 | 983.0 | | 0.07 | 913 | D1298 | 982.5 | | -0.87 |
| 150 | | ---- | | ---- | 922 | D1298 | 982.9 | | -0.12 |
| 158 | | ---- | | ---- | 962 | ISO12185 | 983.1 | | 0.25 |
| 159 | D4052 | 982.9 | | -0.12 | 963 | ISO12185 | 983.0 | | 0.07 |
| 168 | | ---- | | ---- | 971 | IP365 | 982.7 | | -0.49 |
| 169 | | ---- | | ---- | 974 | D1298 | 982.6 | | -0.68 |
| 171 | ISO12185 | 983.4 | | 0.81 | 982 | D1298 | 983.1 | C | 0.25 |
| 175 | D4052 | 983.2 | | 0.44 | 997 | ISO12185 | 981.9 | | -1.99 |
| 194 | D4052 | 983.8 | | 1.56 | 1006 | D1298 | 982.7 | | -0.49 |
| 212 | ISO12185 | 983.0 | | 0.07 | 1011 | ISO12185 | 983.8 | | 1.56 |
| 221 | D4052 | 982.5 | | -0.87 | 1059 | ISO12185 | 980.9 | R(0.05) | -3.85 |
| 224 | D1298 | 988.06 | C,R(0.01) | 9.51 | 1065 | D4052 | 984.2 | | 2.31 |
| 225 | D4052 | 982.4 | | -1.05 | 1082 | ISO12185 | 983.1 | | 0.25 |
| 237 | D4052 | 983.1 | | 0.25 | 1095 | ISO12185 | 983.3 | | 0.63 |
| 238 | D4052 | 983.3 | | 0.63 | 1099 | ISO12185 | 983.1 | | 0.25 |
| 252 | | ---- | | ---- | 1109 | D4052 | 983.1 | | 0.25 |
| 253 | D4052 | 982.6 | | -0.68 | 1126 | ISO12185 | 981.9 | | -1.99 |
| 254 | D1298 | 982.9 | | -0.12 | 1134 | D1298 | 983.1 | | 0.25 |
| 273 | D4052 | 984.0 | | 1.93 | 1135 | ISO12185 | 982.7 | | -0.49 |
| 311 | ISO12185 | 982.7 | | -0.49 | 1161 | | ---- | | ---- |
| 313 | ISO12185 | 982.5 | | -0.87 | 1167 | ISO12185 | 983.10 | | 0.25 |
| 323 | ISO12185 | 983.2 | | 0.44 | 1177 | | ---- | | ---- |
| 331 | ISO12185 | 982.75 | | -0.40 | 1191 | ISO12185 | 983.2 | | 0.44 |
| 333 | ISO12185 | 982.3 | | -1.24 | 1213 | D4052 | 983.98 | | 1.90 |
| 334 | ISO12185 | 983.2 | | 0.44 | 1229 | ISO12185 | 983.2 | | 0.44 |
| 336 | ISO12185 | 983.6 | | 1.19 | 1233 | ISO12185 | 982.87 | | -0.18 |
| 337 | ISO12185 | 982.7 | | -0.49 | 1254 | ISO12185 | 983.06 | | 0.18 |
| 342 | D4052 | 983.11 | | 0.27 | 1259 | ISO12185 | 984.4 | | 2.68 |
| 343 | D4052 | 982.9 | | -0.12 | 1275 | IP365 | 983.6 | | 1.19 |
| 349 | | ---- | | ---- | 1299 | ISO12185 | 983.0 | | 0.07 |
| 351 | ISO3675 | 983.40 | | 0.81 | 1345 | ISO12185 | 982.7 | | -0.49 |
| 371 | D4052 | 982.9 | | -0.12 | 1356 | ISO12185 | 982.55 | | -0.77 |
| 391 | ISO12185 | 982.8 | | -0.31 | 1367 | D1298 | 982.9 | | -0.12 |
| 398 | ISO3675 | 983.0 | | 0.07 | 1389 | ISO12185 | 982.4 | | -1.05 |
| 399 | ISO12185 | 981.6 | | -2.55 | 1402 | IP365 | 983.4 | | 0.81 |
| 440 | D4052 | 983.1 | | 0.25 | 1404 | ISO12185 | 983.1 | | 0.25 |
| 444 | D4052 | 958.7 | R(0.01) | -45.29 | 1412 | D4052 | 982.7 | | -0.49 |
| 445 | IP365 | 983.8 | | 1.56 | 1428 | ISO12185 | 983.9 | | 1.75 |
| 447 | IP365 | 981.9 | | -1.99 | 1431 | ISO12185 | 983.23 | | 0.50 |
| 463 | ISO12185 | 982.70 | | -0.49 | 1459 | ISO12185 | 982.6 | | -0.68 |
| 511 | | ---- | | ---- | 1488 | ISO3675 | 988.45 | C,R(0.01) | 10.24 |
| 541 | ISO12185 | 982.4 | | -1.05 | 1510 | IP365 | 982.3 | | -1.24 |
| 562 | D1298 | 982.1 | | -1.61 | 1539 | ISO12185 | 983.1 | | 0.25 |
| 575 | D1298 | 981.4 | | -2.92 | 1556 | ISO12185 | 982.8 | | -0.31 |
| 603 | D1298 | 983.2 | | 0.44 | 1569 | ISO12185 | 982.8 | | -0.31 |
| 604 | D4052 | 983.9 | | 1.75 | 1584 | ISO12185 | 983.1 | | 0.25 |
| 605 | D1298 | 983.4 | | 0.81 | 1586 | ISO12185 | 982.9 | | -0.12 |
| 608 | D4052 | 983.1 | | 0.25 | 1613 | D4052 | 982.5 | | -0.87 |
| 621 | | ---- | | ---- | 1622 | D4052 | 982.7 | | -0.49 |
| 631 | D1298 | 984.94 | R(0.05) | 3.69 | 1631 | ISO12185 | 982.9 | | -0.12 |
| 663 | D4052 | 983.3 | | 0.63 | 1643 | D4052 | 982.9 | | -0.12 |
| 671 | D1298 | 982.8 | C | -0.31 | 1710 | ISO12185 | 983.6 | | 1.19 |
| 750 | D1298 | 983.0 | | 0.07 | 1720 | D4052 | 982.9 | | -0.12 |
| 753 | D1298 | 983.2 | | 0.44 | 1724 | D1298 | 982.1 | | -1.61 |
| 759 | D1298 | 982.9 | | -0.12 | 1728 | ISO12185 | 981.81 | | -2.15 |
| 824 | ISO12185 | 982.9 | | -0.12 | 1740 | ISO12185 | 982.9 | | -0.12 |
| 825 | D4052 | 982.8 | | -0.31 | 1741 | ISO12185 | 982.31 | | -1.22 |
| 851 | ISO12185 | 982.8 | | -0.31 | 1796 | ISO12185 | 983.44 | | 0.89 |
| 855 | ISO12185 | 983.12 | | 0.29 | 1807 | ISO3675 | 982.6 | | -0.68 |
| 857 | ISO3675 | 983.1 | | 0.25 | 1832 | ISO12185 | 983.0 | | 0.07 |
| 858 | ISO12185 | 982.9 | | -0.12 | 1833 | ISO12185 | 982.9 | | -0.12 |
| 859 | D4052 | 983.0 | | 0.07 | 1849 | ISO12185 | 982.1 | | -1.61 |
| 862 | ISO12185 | 982.8 | | -0.31 | 1857 | ISO12185 | 983.5 | | 1.00 |
| 863 | ISO12185 | 982.6 | | -0.68 | 1862 | ISO12185 | 983.1 | | 0.25 |
| 864 | ISO12185 | 982.7 | | -0.49 | 1881 | D4052 | 983.1 | | 0.25 |
| 865 | ISO12185 | 982.9 | | -0.12 | 1906 | | ---- | | ---- |
| 866 | ISO12185 | 983.2 | | 0.44 | 1936 | ISO12185 | 983.0 | | 0.07 |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|----------|--------|-----------|---------|------|----------|--------|------|---------|
| 1937 | ISO12185 | 983.0 | | 0.07 | 6024 | ISO12185 | 983.5 | | 1.00 |
| 1938 | ISO12185 | 982.8 | | -0.31 | 6026 | D1298 | 983.2 | | 0.44 |
| 1943 | | ----- | | ----- | 6028 | ISO12185 | 982.1 | | -1.61 |
| 1956 | ISO12185 | 984.4 | | 2.68 | 6039 | | ----- | | ----- |
| 1962 | D1298 | 985 | C,R(0.05) | 3.80 | 6049 | ISO12185 | 982.7 | | -0.49 |
| 1964 | | ----- | | ----- | 6051 | D4052 | 983.1 | | 0.25 |
| 1967 | D1298 | 982.9 | | -0.12 | 6057 | ISO12185 | 982.7 | | -0.49 |
| 1971 | ISO12185 | 983.03 | | 0.12 | 6075 | ISO12185 | 984.24 | | 2.38 |
| 1986 | D4052 | 983.4 | | 0.81 | 6092 | D4052 | 982.9 | | -0.12 |
| 1995 | D4052 | 981.7 | | -2.36 | 6109 | | ----- | | ----- |
| 6004 | D1298 | 983.4 | | 0.81 | 6112 | ISO12185 | 982.9 | | -0.12 |
| 6016 | D4052 | 983.67 | | 1.32 | 6114 | ISO12185 | 983.2 | | 0.44 |
| 6021 | ISO12185 | 983.0 | | 0.07 | 6122 | ISO3675 | 983.35 | | 0.72 |

normality suspect
n 148
outliers 6
mean (n) 982.964
st.dev. (n) 0.5087
R(calc.) 1.424
R(ISO12185:96) 1.5

Lab 224 first reported: 985.11
Lab 671 first reported: 968.5
Lab 982 reported: 983.1 kg/L
Lab 1488 first reported: 987.15
Lab 1962 first reported: 1002



Determination of Flash Point PMcc on sample #17105; results in °C

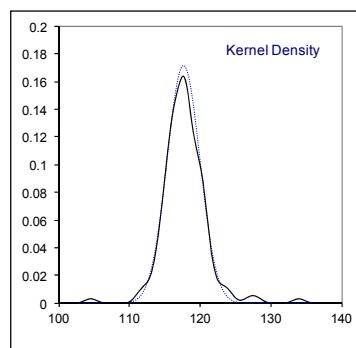
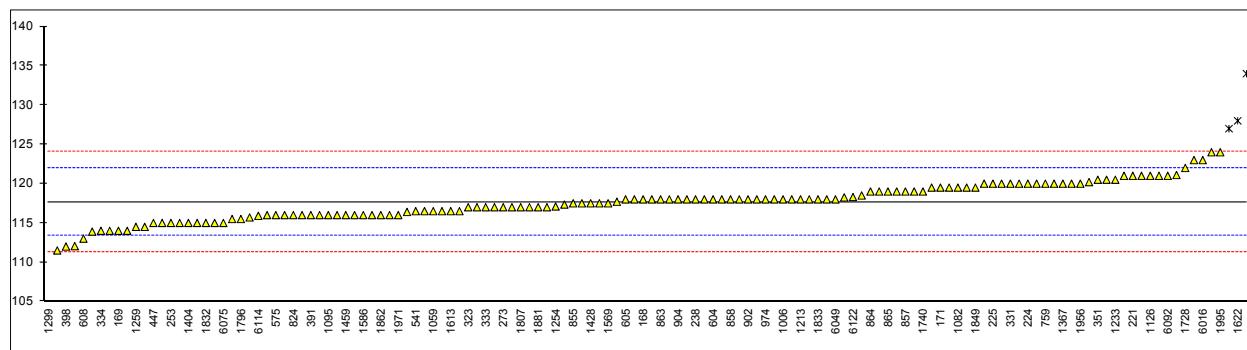
| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|-----------|--------|------|---------|------|-----------|--------|---------|---------|
| 62 | D93-A | 115.5 | C | -1.01 | 870 | D93-B | 118 | | 0.16 |
| 90 | D93-B | >110 | | ----- | 886 | D93-A | 118 | | 0.16 |
| 92 | D93-B | 118 | | 0.16 | 902 | D93-B | 118.0 | | 0.16 |
| 120 | D93-B | 117.0 | | -0.31 | 904 | D93-B | 118 | | 0.16 |
| 131 | D93-B | 118 | | 0.16 | 912 | D93-B | 118 | | 0.16 |
| 140 | D93-B | >230 | U | ----- | 913 | D93-A | 120 | | 1.09 |
| 150 | D93-B | >110 | | ----- | 922 | D93-B | 119 | | 0.63 |
| 158 | | ----- | | ----- | 962 | ISO2719-B | 116 | | -0.77 |
| 159 | D93-B | >110 | | ----- | 963 | ISO2719-B | 117.5 | | -0.07 |
| 168 | D93-B | 118.0 | | 0.16 | 971 | D93-B | 118.0 | | 0.16 |
| 169 | D93-B | 114 | | -1.71 | 974 | D93-B | 118.0 | | 0.16 |
| 171 | ISO2719-A | 119.5 | | 0.86 | 982 | | ----- | | ----- |
| 175 | D93-B | 116 | | -0.77 | 997 | D93-B | 118.0 | | 0.16 |
| 194 | D93-B | 115 | | -1.24 | 1006 | D93-B | 118.0 | | 0.16 |
| 212 | | 114.0 | | -1.71 | 1011 | ISO2719-B | 120 | | 1.09 |
| 221 | D93-B | 121.0 | | 1.56 | 1059 | ISO2719-B | 116.5 | | -0.54 |
| 224 | D93-B | 120 | | 1.09 | 1065 | D93-A | 121 | | 1.56 |
| 225 | D93-B | 120.0 | | 1.09 | 1082 | ISO2719-A | 119.5 | | 0.86 |
| 237 | D93-A | 120 | | 1.09 | 1095 | D93-B | 116.0 | | -0.77 |
| 238 | D93-B | 118.0 | | 0.16 | 1099 | ISO2719-A | 119.5 | | 0.86 |
| 252 | | ----- | | ----- | 1109 | D93-B | >100 | | ----- |
| 253 | D93-B | 115 | | -1.24 | 1126 | ISO2719-A | 121 | | 1.56 |
| 254 | D93-B | 116.0 | | -0.77 | 1134 | D93-B | 121.0 | | 1.56 |
| 273 | D93-B | 117 | | -0.31 | 1135 | ISO2719-B | 118.0 | | 0.16 |
| 311 | | ----- | | ----- | 1161 | | ----- | | ----- |
| 313 | ISO2719-B | 123.0 | | 2.49 | 1167 | ISO2719-B | 118.25 | | 0.28 |
| 323 | ISO2719-A | 117.0 | | -0.31 | 1177 | | ----- | | ----- |
| 331 | D93-B | 120.0 | | 1.09 | 1191 | ISO2719-A | 120.5 | | 1.33 |
| 333 | ISO2719-B | 117.0 | | -0.31 | 1213 | D93-A | 118 | | 0.16 |
| 334 | D93-B | 114.0 | | -1.71 | 1229 | ISO2719-A | 115.0 | | -1.24 |
| 336 | | ----- | | ----- | 1233 | ISO2719-B | 120.5 | | 1.33 |
| 337 | | ----- | | ----- | 1254 | D93-B | 117.1 | | -0.26 |
| 342 | ISO2719-B | 111.5 | | -2.87 | 1259 | ISO2719-A | 114.5 | | -1.47 |
| 343 | ISO2719-B | 119.5 | | 0.86 | 1275 | | ----- | | ----- |
| 349 | | ----- | | ----- | 1299 | D93-B | 104.5 | R(0.01) | -6.14 |
| 351 | ISO2719-B | 120.50 | | 1.33 | 1345 | | ----- | | ----- |
| 371 | ISO2719-B | 116.0 | | -0.77 | 1356 | ISO2719-B | 134 | R(0.01) | 7.63 |
| 391 | ISO2719-B | 116 | | -0.77 | 1367 | D93-A | 120 | | 1.09 |
| 398 | ISO2719-B | 112 | | -2.64 | 1389 | D93-B | 120.0 | | 1.09 |
| 399 | | ----- | | ----- | 1402 | IP34-B | 117.0 | | -0.31 |
| 440 | IP34-A | 115.7 | | -0.91 | 1404 | ISO2719-B | 115.0 | | -1.24 |
| 444 | D93-B | 119.5 | | 0.86 | 1412 | D93-B | 116.0 | | -0.77 |
| 445 | IP34-B | 118.0 | | 0.16 | 1428 | ISO2719-B | 117.5 | | -0.07 |
| 447 | D93-B | 115 | | -1.24 | 1431 | D93-B | 117.7 | | 0.02 |
| 463 | D93-B | 118.5 | | 0.39 | 1459 | ISO2719-A | 116.0 | | -0.77 |
| 511 | D93-B | 112.05 | | -2.62 | 1488 | ISO2719-B | 120.2 | | 1.19 |
| 541 | D93-B | 116.5 | | -0.54 | 1510 | D93-B | 118 | | 0.16 |
| 562 | D93-B | 116.5 | | -0.54 | 1539 | ISO2719-B | 116.5 | | -0.54 |
| 575 | D93-B | 116 | | -0.77 | 1556 | ISO2719-B | 117.5 | | -0.07 |
| 603 | D93-B | 121.0 | | 1.56 | 1569 | D93-A | 117.5 | | -0.07 |
| 604 | D93-B | 118 | | 0.16 | 1584 | ISO2719-B | 116.0 | | -0.77 |
| 605 | D93-B | 118.0 | | 0.16 | 1586 | ISO2719-B | 116.0 | | -0.77 |
| 608 | D93-B | 113.0 | | -2.17 | 1613 | D93-B | 116.5 | | -0.54 |
| 621 | | ----- | | ----- | 1622 | D93-B | 128.0 | R(0.01) | 4.83 |
| 631 | D93-B | 117.34 | | -0.15 | 1631 | ISO2719-B | 116 | | -0.77 |
| 663 | D93-B | 116.4 | | -0.59 | 1643 | D93-B | 121.1 | | 1.61 |
| 671 | D93-A | >110 | | ----- | 1710 | | ----- | | ----- |
| 750 | | ----- | | ----- | 1720 | | ----- | | ----- |
| 753 | D93-B | 124.0 | | 2.96 | 1724 | D93-B | 119 | | 0.63 |
| 759 | ISO2719-B | 120.0 | | 1.09 | 1728 | ISO2719-A | 122 | | 2.03 |
| 824 | ISO2719-B | 116.0 | | -0.77 | 1740 | ISO2719-B | 119 | | 0.63 |
| 825 | D93-B | 120.0 | | 1.09 | 1741 | ISO2719-B | 115 | | -1.24 |
| 851 | ISO2719-B | 120.0 | | 1.09 | 1796 | ISO2719-B | 115.5 | | -1.01 |
| 855 | ISO2719-B | 117.5 | | -0.07 | 1807 | ISO2719-B | 117 | | -0.31 |
| 857 | ISO2719-B | 119.0 | | 0.63 | 1832 | ISO2719-B | 115.0 | | -1.24 |
| 858 | D93-B | 118.0 | | 0.16 | 1833 | ISO2719-B | 118 | | 0.16 |
| 859 | D93-B | 117 | | -0.31 | 1849 | ISO2719-B | 119.5 | | 0.86 |
| 862 | ISO2719-B | 118.0 | | 0.16 | 1857 | ISO2719-B | 117.0 | | -0.31 |
| 863 | D93-B | 118.0 | | 0.16 | 1862 | ISO2719-B | 116.0 | | -0.77 |
| 864 | D93-B | 119.0 | | 0.63 | 1881 | D93-B | 117.0 | | -0.31 |
| 865 | ISO2719-B | 119.0 | | 0.63 | 1906 | | ----- | | ----- |
| 866 | D93-B | 119 | | 0.63 | 1936 | | ----- | | ----- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|-----------|-------|------|---------|------|-----------|--------|---------|---------|
| 1937 | ISO2719-B | 116 | | -0.77 | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | D93-B | 114.5 | | -1.47 |
| 1943 | | ---- | | ---- | 6028 | ISO2719-A | 115 | | -1.24 |
| 1956 | ISO2719-B | 120 | | 1.09 | 6039 | | ---- | | ---- |
| 1962 | D93-B | 113.9 | | -1.75 | 6049 | ISO2719-B | 118.0 | | 0.16 |
| 1964 | | ---- | | ---- | 6051 | D93-B | 114.0 | | -1.71 |
| 1967 | D93-B | 116.5 | | -0.54 | 6057 | ISO2719-B | 127.0 | R(0.05) | 4.36 |
| 1971 | ISO2719-B | 116.0 | | -0.77 | 6075 | ISO2719-B | 115.0 | | -1.24 |
| 1986 | ISO2719-B | 118.0 | | 0.16 | 6092 | D93-B | 121 | | 1.56 |
| 1995 | D93-B | 124 | | 2.96 | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | D93-B | 123.0 | | 2.49 | 6114 | D93-B | 115.91 | | -0.81 |
| 6021 | ISO2719-B | 117.0 | | -0.31 | 6122 | ISO2719-B | 118.3 | | 0.30 |

normality OK
n 134
outliers 4
mean (n) 117.656
st.dev. (n) 2.3235
R(calc.) 6.506
R(ISO2719-B:16) 6

Lab 62 first reported: 135.5

Lab 140: reported possibly a unit error? 230F = 110°C



Determination of Heat of Combustion Gross on sample #17105; results in MJ/kg

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|--------------|---------|------|---------|------|--------------|----------|------|---------|
| 62 | | ---- | | | 870 | | ---- | | ---- |
| 90 | D240 | 43.151 | | 0.44 | 886 | | ---- | | ---- |
| 92 | | 42.772 | | -2.21 | 902 | D4868 | 43.02 | | -0.48 |
| 120 | | ---- | | | 904 | D4868 | 43 | | -0.62 |
| 131 | | ---- | | | 912 | | ---- | | ---- |
| 140 | | ---- | | | 913 | D4868 | 43.01 | C | -0.55 |
| 150 | D240 | 43.324 | | 1.65 | 922 | D240 | 42.9158 | | -1.21 |
| 158 | | ---- | | | 962 | | ---- | | ---- |
| 159 | | ---- | | | 963 | | ---- | | ---- |
| 168 | | ---- | | | 971 | | ---- | | ---- |
| 169 | | ---- | | | 974 | D4868 | 43.06 | | -0.20 |
| 171 | D240 | 42.895 | | -1.35 | 982 | D4868 | 43.04 | | -0.34 |
| 175 | | ---- | | | 997 | | ---- | | ---- |
| 194 | | ---- | | | 1006 | | ---- | | ---- |
| 212 | | ---- | | | 1011 | D240 | 43.065 | | -0.16 |
| 221 | | ---- | | | 1059 | | ---- | | ---- |
| 224 | | ---- | | | 1065 | | ---- | | ---- |
| 225 | D4868 | 43.04 | | -0.34 | 1082 | D240 | 43.1540 | | 0.46 |
| 237 | D4868 | 43.037 | | -0.36 | 1095 | | ---- | | ---- |
| 238 | | ---- | | | 1099 | PN-C-04062 | 43.281 | | 1.35 |
| 252 | | ---- | | | 1109 | D4868 | 43.03 | | -0.41 |
| 253 | | ---- | | | 1126 | | ---- | | ---- |
| 254 | | ---- | | | 1134 | | 43.21255 | | 0.87 |
| 273 | | ---- | | | 1135 | D240 | 43.08 | | -0.06 |
| 311 | | 43.235 | | 1.03 | 1161 | | ---- | | ---- |
| 313 | | ---- | | | 1167 | DIN51900-2 | 43.181 | | 0.65 |
| 323 | D240 | 43.080 | | -0.06 | 1177 | DIN51900 1/2 | 43.228 | | 0.98 |
| 331 | | 43.30 | | 1.48 | 1191 | | ---- | | ---- |
| 333 | D240 | 43.215 | | 0.89 | 1213 | | 43.00 | C | -0.62 |
| 334 | | ---- | | | 1229 | | ---- | | ---- |
| 336 | | ---- | | | 1233 | | ---- | | ---- |
| 337 | | ---- | | | 1254 | | ---- | | ---- |
| 342 | | ---- | | | 1259 | D4868 | 42.971 | | -0.82 |
| 343 | D240 | 43.071 | | -0.12 | 1275 | | ---- | | ---- |
| 349 | | ---- | | | 1299 | D240 | 43.061 | | -0.19 |
| 351 | ISO8217Calc. | 43.284 | | 1.37 | 1345 | D4868 | 43.03 | | -0.41 |
| 371 | D4868 | 43.035 | | -0.37 | 1356 | | ---- | | ---- |
| 391 | | ---- | | | 1367 | | 43.072 | | -0.11 |
| 398 | | ---- | | | 1389 | | ---- | | ---- |
| 399 | | ---- | | | 1402 | IP12 | 43.02 | | -0.48 |
| 440 | | ---- | | | 1404 | | ---- | | ---- |
| 444 | | ---- | | | 1412 | D4868 | 43.02 | | -0.48 |
| 445 | D240 | 43.028 | | -0.42 | 1428 | | ---- | | ---- |
| 447 | D240 | 43.200 | | 0.78 | 1431 | D240 | 43.044 | | -0.31 |
| 463 | | ---- | | | 1459 | | ---- | | ---- |
| 511 | | ---- | | | 1488 | D240 | 43.1599 | | 0.50 |
| 541 | | ---- | | | 1510 | | 42.82 | | -1.88 |
| 562 | | ---- | | | 1539 | | 42.938 | | -1.05 |
| 575 | | ---- | | | 1556 | D4868 | 43.04 | | -0.34 |
| 603 | | ---- | | | 1569 | D240 | 43.033 | | -0.39 |
| 604 | | ---- | | | 1584 | | ---- | | ---- |
| 605 | | ---- | | | 1586 | D240 | 43.01 | | -0.55 |
| 608 | | 43.2101 | | 0.85 | 1613 | | ---- | | ---- |
| 621 | | ---- | | | 1622 | D240 | 43.15 | C | 0.43 |
| 631 | D240 | 43.0647 | | -0.16 | 1631 | | ---- | | ---- |
| 663 | | ---- | | | 1643 | D240 | 43.12 | | 0.22 |
| 671 | | ---- | | | 1710 | D4809 | 43.140 | | 0.36 |
| 750 | | ---- | | | 1720 | | ---- | | ---- |
| 753 | | ---- | | | 1724 | | ---- | | ---- |
| 759 | | ---- | | | 1728 | D4868 | 43.0469 | | -0.29 |
| 824 | D240 | 43.095 | | 0.05 | 1740 | | 42.970 | | -0.83 |
| 825 | | 43.157 | | 0.48 | 1741 | | ---- | | ---- |
| 851 | | ---- | | | 1796 | | ---- | | ---- |
| 855 | GB/T 384 | 43.080 | | -0.06 | 1807 | D240 | 43.164 | | 0.53 |
| 857 | GB/T 384 | 43.126 | | 0.27 | 1832 | | ---- | | ---- |
| 858 | D4868 | 43.04 | | -0.34 | 1833 | | ---- | | ---- |
| 859 | D4868 | 43.05 | | -0.27 | 1849 | | ---- | | ---- |
| 862 | D240 | 43.185 | | 0.68 | 1857 | D4868 | 43.02 | | -0.48 |
| 863 | D4868 | 43.050 | | -0.27 | 1862 | D4868 | 43.02 | | -0.48 |
| 864 | D4868 | 43.06 | | -0.20 | 1881 | | ---- | | ---- |
| 865 | GB/T 384 | 43.05 | | -0.27 | 1906 | | 43.169 | | 0.57 |
| 866 | D4868 | 43.30 | | 1.48 | 1936 | | ---- | | ---- |

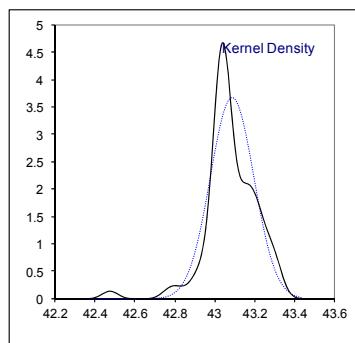
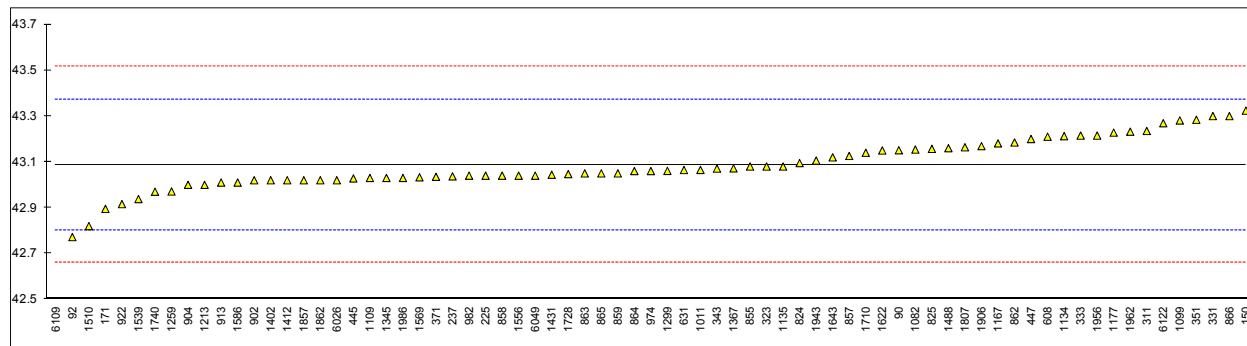
| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|------------|--------|------|---------|------|--------|---------|---------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | D4868 | 43.02 | | -0.48 |
| 1943 | DIN51900-1 | 43.106 | | 0.13 | 6028 | | ---- | | ---- |
| 1956 | | 43.215 | | 0.89 | 6039 | | ---- | | ---- |
| 1962 | D240 | 43.232 | | 1.01 | 6049 | D4868 | 43.04 | | -0.34 |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | | ---- | | ---- | 6057 | | ---- | | ---- |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | D4868 | 43.030 | | -0.41 | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | D240 | 42.4774 | R(0.01) | -4.27 |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | | ---- | | ---- | 6114 | | ---- | | ---- |
| 6021 | | ---- | | ---- | 6122 | D240 | 43.269 | | 1.27 |

normality OK
n 72
outliers 1
mean (n) 43.0881
st.dev. (n) 0.10871
R(calc.) 0.3044
R(D240:17) 0.40

Lab 913 reported: 10272 kcal/kg: iis calc to MJ/kg

Lab 1213 first reported: 10270 cal/g

Lab 1622 first reported: 43.578

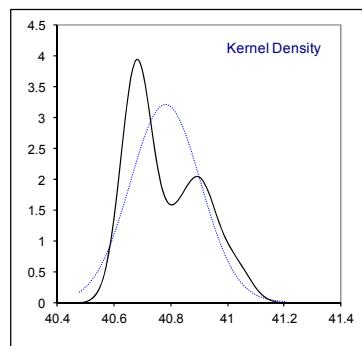
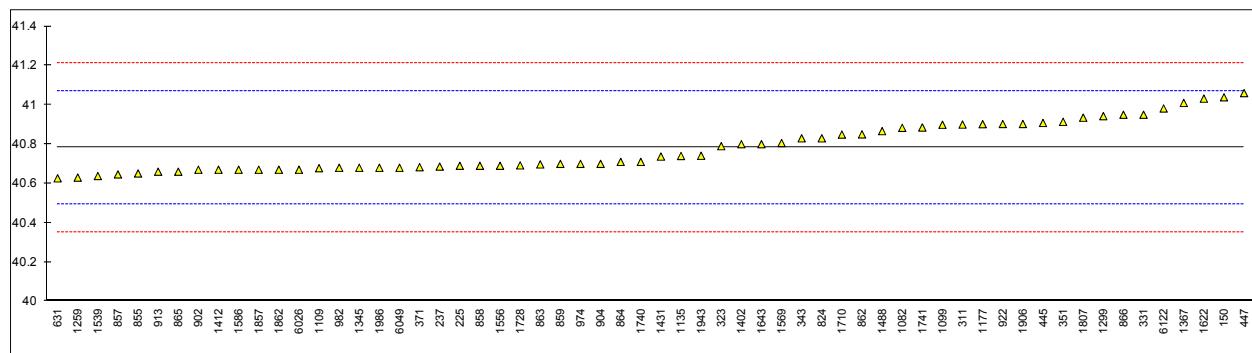


Determination of Heat of Combustion Net on sample #17105; results in MJ/kg

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|--------------|---------|------|---------|------|--------------|---------|------|---------|
| 62 | | ---- | | | 870 | | ---- | | ---- |
| 90 | | ---- | | | 886 | | ---- | | ---- |
| 92 | | ---- | | | 902 | D4868 | 40.67 | | -0.78 |
| 120 | | ---- | | | 904 | D4868 | 40.7 | | -0.57 |
| 131 | | ---- | | | 912 | | ---- | | ---- |
| 140 | | ---- | | | 913 | D4868 | 40.66 | | -0.85 |
| 150 | D240 | 41.039 | | 1.80 | 922 | D240 | 40.9029 | | 0.85 |
| 158 | | ---- | | | 962 | | ---- | | ---- |
| 159 | | ---- | | | 963 | | ---- | | ---- |
| 168 | | ---- | | | 971 | | ---- | | ---- |
| 169 | | ---- | | | 974 | D4868 | 40.70 | | -0.57 |
| 171 | | ---- | | | 982 | D4868 | 40.68 | | -0.71 |
| 175 | | ---- | | | 997 | | ---- | | ---- |
| 194 | | ---- | | | 1006 | | ---- | | ---- |
| 212 | | ---- | | | 1011 | | ---- | | ---- |
| 221 | | ---- | | | 1059 | | ---- | | ---- |
| 224 | | ---- | | | 1065 | | ---- | | ---- |
| 225 | D4868 | 40.69 | | -0.64 | 1082 | D240 | 40.8834 | | 0.71 |
| 237 | D4868 | 40.686 | | -0.67 | 1095 | | ---- | | ---- |
| 238 | | ---- | | | 1099 | PN-C-04062 | 40.899 | | 0.82 |
| 252 | | ---- | | | 1109 | D4868 | 40.678 | | -0.73 |
| 253 | | ---- | | | 1126 | | ---- | | ---- |
| 254 | | ---- | | | 1134 | | ---- | | ---- |
| 273 | | ---- | | | 1135 | D240 | 40.74 | | -0.29 |
| 311 | | 40.900 | | 0.83 | 1161 | | ---- | | ---- |
| 313 | | ---- | | | 1167 | | ---- | | ---- |
| 323 | D240 | 40.790 | | 0.06 | 1177 | DIN51900 1/2 | 40.902 | | 0.84 |
| 331 | | 40.95 | | 1.18 | 1191 | | ---- | | ---- |
| 333 | | ---- | | | 1213 | | ---- | | ---- |
| 334 | | ---- | | | 1229 | | ---- | | ---- |
| 336 | | ---- | | | 1233 | | ---- | | ---- |
| 337 | | ---- | | | 1254 | | ---- | | ---- |
| 342 | | ---- | | | 1259 | D4868 | 40.63 | | -1.06 |
| 343 | D240 | 40.830 | | 0.34 | 1275 | | ---- | | ---- |
| 349 | | ---- | | | 1299 | D240 | 40.943 | | 1.13 |
| 351 | ISO8217Calc. | 40.914 | | 0.92 | 1345 | D4868 | 40.68 | | -0.71 |
| 371 | D4868 | 40.683 | | -0.69 | 1356 | | ---- | | ---- |
| 391 | | ---- | | | 1367 | | 41.01 | | 1.60 |
| 398 | | ---- | | | 1389 | | ---- | | ---- |
| 399 | | ---- | | | 1402 | IP12 | 40.80 | | 0.13 |
| 440 | | ---- | | | 1404 | | ---- | | ---- |
| 444 | | ---- | | | 1412 | D4868 | 40.67 | | -0.78 |
| 445 | D240 | 40.908 | | 0.88 | 1428 | | ---- | | ---- |
| 447 | D240 | 41.060 | | 1.95 | 1431 | D240 | 40.737 | | -0.31 |
| 463 | | ---- | | | 1459 | | ---- | | ---- |
| 511 | | ---- | | | 1488 | D240 | 40.8664 | | 0.59 |
| 541 | | ---- | | | 1510 | | ---- | | ---- |
| 562 | | ---- | | | 1539 | | 40.638 | | -1.01 |
| 575 | | ---- | | | 1556 | D4868 | 40.69 | | -0.64 |
| 603 | | ---- | | | 1569 | D240 | 40.806 | | 0.17 |
| 604 | | ---- | | | 1584 | | ---- | | ---- |
| 605 | | ---- | | | 1586 | D240 | 40.67 | | -0.78 |
| 608 | | ---- | | | 1613 | | ---- | | ---- |
| 621 | | ---- | | | 1622 | D240 | 41.032 | | 1.75 |
| 631 | D4868 | 40.6264 | | -1.09 | 1631 | | ---- | | ---- |
| 663 | | ---- | | | 1643 | D240 | 40.80 | | 0.13 |
| 671 | | ---- | | | 1710 | D4809 | 40.849 | | 0.47 |
| 750 | | ---- | | | 1720 | | ---- | | ---- |
| 753 | | ---- | | | 1724 | | ---- | | ---- |
| 759 | | ---- | | | 1728 | D4868 | 40.6921 | | -0.63 |
| 824 | D240 | 40.830 | | 0.34 | 1740 | | 40.710 | | -0.50 |
| 825 | | ---- | | | 1741 | D4868 | 40.8851 | | 0.72 |
| 851 | | ---- | | | 1796 | | ---- | | ---- |
| 855 | GB/T 384 | 40.651 | | -0.92 | 1807 | D240 | 40.935 | | 1.07 |
| 857 | GB/T 384 | 40.646 | | -0.95 | 1832 | | ---- | | ---- |
| 858 | D4868 | 40.69 | | -0.64 | 1833 | | ---- | | ---- |
| 859 | D4868 | 40.70 | | -0.57 | 1849 | | ---- | | ---- |
| 862 | D240 | 40.850 | | 0.48 | 1857 | D4868 | 40.67 | | -0.78 |
| 863 | D4868 | 40.697 | | -0.59 | 1862 | D4868 | 40.67 | | -0.78 |
| 864 | D4868 | 40.71 | | -0.50 | 1881 | | ---- | | ---- |
| 865 | GB/T 384 | 40.66 | | -0.85 | 1906 | | 40.903 | | 0.85 |
| 866 | D4868 | 40.95 | | 1.18 | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|------------|--------|------|---------|------|--------|--------|------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | D4868 | 40.67 | | -0.78 |
| 1943 | DIN51900-1 | 40.741 | | -0.29 | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | D4868 | 40.68 | | -0.71 |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | | ---- | | ---- | 6057 | | ---- | | ---- |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | D4868 | 40.680 | | -0.71 | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | | ---- | | ---- | 6114 | | ---- | | ---- |
| 6021 | | ---- | | ---- | 6122 | D240 | 40.982 | | 1.40 |

normality OK
n 60
outliers 0
mean (n) 40.7819
st.dev. (n) 0.12406
R(calc.) 0.3474
R(D240:17) 0.40

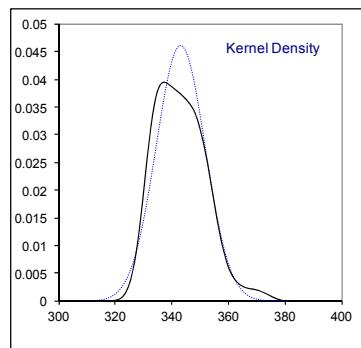
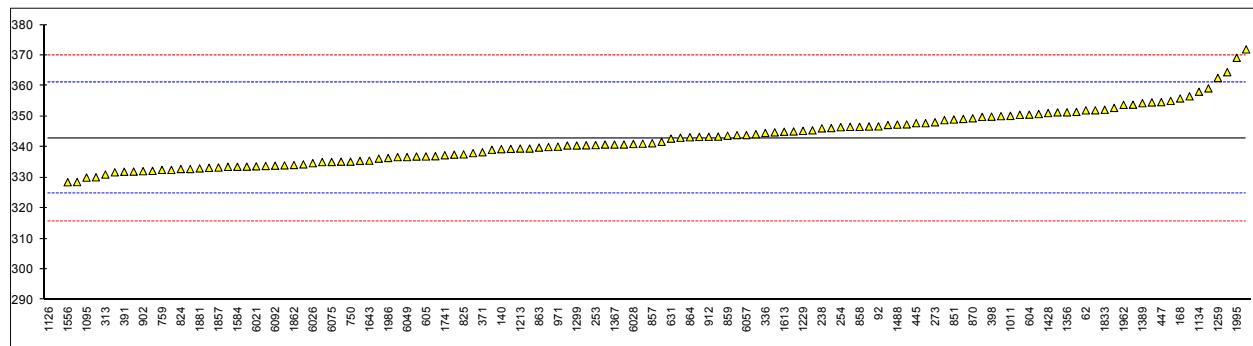


Determination of Kinematic Viscosity at 50°C on sample #17105; results in mm²/s

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|---------|---------|------|---------|------|---------|-----------|---------|---------|
| 62 | D445 | 352.0 | | 1.01 | 870 | ISO3104 | 349.4 | | 0.72 |
| 90 | D445 | 341.10 | | -0.20 | 886 | | ---- | | ---- |
| 92 | D445 | 346.75 | | 0.43 | 902 | ISO3104 | 332.1 | | -1.19 |
| 120 | D445 | 340.8 | | -0.23 | 904 | D445 | 332.8 | | -1.11 |
| 131 | D445 | 347.8 | | 0.54 | 912 | D445 | 343.34 | | 0.05 |
| 140 | ISO3104 | 339.3 | | -0.40 | 913 | | ---- | | ---- |
| 150 | D445 | 350.1 | | 0.80 | 922 | D445 | 343.9 | | 0.11 |
| 158 | | ---- | | ---- | 962 | ISO3104 | 338.0 | | -0.54 |
| 159 | D445 | 349.2 | | 0.70 | 963 | ISO3104 | 339.1 | | -0.42 |
| 168 | D445 | 355.9 | | 1.44 | 971 | D445 | 340.1 | | -0.31 |
| 169 | | ---- | | ---- | 974 | D445 | 339.4 | | -0.38 |
| 171 | ISO3104 | 352.8 | | 1.09 | 982 | D445 | 371.96 | | 3.21 |
| 175 | D445 | 333.2 | | -1.07 | 997 | D445 | 343.03 | | 0.02 |
| 194 | D445 | 332.19 | | -1.18 | 1006 | D445 | 354.6 | | 1.29 |
| 212 | ISO3104 | 353.85 | | 1.21 | 1011 | ISO3104 | 350.2 | | 0.81 |
| 221 | D445 | 341.7 | | -0.13 | 1059 | ISO3104 | 359.2 | | 1.80 |
| 224 | | ---- | | ---- | 1065 | D445 | 364.5 | | 2.38 |
| 225 | D445 | 343.3 | | 0.05 | 1082 | ISO3104 | 350.54 | | 0.84 |
| 237 | | ---- | | ---- | 1095 | ISO3104 | 330.0 | | -1.42 |
| 238 | D445 | 346.109 | | 0.36 | 1099 | | ---- | W | ---- |
| 252 | | ---- | | ---- | 1109 | D445 | 336.89 | | -0.66 |
| 253 | D445 | 340.62 | | -0.25 | 1126 | ISO3104 | 255.978 | R(0.01) | -9.59 |
| 254 | D445 | 346.5 | | 0.40 | 1134 | D445 | 358.1 | | 1.68 |
| 273 | D445 | 348.1 | | 0.58 | 1135 | ISO3104 | 331.95 | | -1.21 |
| 311 | ISO3104 | 333.5 | | -1.04 | 1161 | | ---- | | ---- |
| 313 | ISO3104 | 331.0 | | -1.31 | 1167 | | ---- | | ---- |
| 323 | ISO3104 | 340.0 | | -0.32 | 1177 | | ---- | | ---- |
| 331 | ISO3104 | 355.1 | | 1.35 | 1191 | ISO3104 | 340.82 | | -0.23 |
| 333 | ISO3104 | 346.6 | | 0.41 | 1213 | D445 | 339.5 | | -0.37 |
| 334 | ISO3104 | 344.2 | | 0.14 | 1229 | ISO3104 | 345.3 | | 0.27 |
| 336 | ISO3104 | 344.6 | | 0.19 | 1233 | ISO3104 | 352.02 | | 1.01 |
| 337 | | ---- | | ---- | 1254 | D445 | 345.47 | | 0.28 |
| 342 | ISO3104 | 346.7 | | 0.42 | 1259 | ISO3104 | 362.6148 | | 2.18 |
| 343 | ISO3104 | 334.320 | | -0.95 | 1275 | | ---- | | ---- |
| 349 | | ---- | | ---- | 1299 | D445 | 340.5 | | -0.26 |
| 351 | ISO3104 | 351.50 | | 0.95 | 1345 | D445 | 347.4036 | | 0.50 |
| 371 | D445 | 338.3 | | -0.51 | 1356 | ISO3104 | 351.35 | | 0.93 |
| 391 | ISO3104 | 331.9 | | -1.21 | 1367 | IP71 | 340.8 | | -0.23 |
| 398 | ISO3104 | 349.94 | | 0.78 | 1389 | D445 | 354.35 | | 1.26 |
| 399 | | ---- | | ---- | 1402 | ISO3104 | 334.0 | | -0.98 |
| 440 | | ---- | | ---- | 1404 | ISO3104 | 345.1 | | 0.24 |
| 444 | | ---- | | ---- | 1412 | | ---- | | ---- |
| 445 | IP71 | 347.8 | | 0.54 | 1428 | ISO3104 | 351.1 | | 0.91 |
| 447 | D445 | 354.7 | | 1.30 | 1431 | | ---- | | ---- |
| 463 | D445 | 346.196 | | 0.36 | 1459 | | ---- | | ---- |
| 511 | | ---- | | ---- | 1488 | ISO3104 | 347.34463 | | 0.49 |
| 541 | D445 | 335.47 | | -0.82 | 1510 | D445 | 337.5 | | -0.59 |
| 562 | | ---- | | ---- | 1539 | ISO3104 | 343.4 | | 0.06 |
| 575 | D445 | 356.6 | | 1.51 | 1556 | ISO3104 | 328.47 | | -1.59 |
| 603 | D445 | 351.33 | | 0.93 | 1569 | | ---- | | ---- |
| 604 | D445 | 350.61 | | 0.85 | 1584 | ISO3104 | 333.52 | | -1.03 |
| 605 | D445 | 336.91 | | -0.66 | 1586 | ISO3104 | 333.8 | | -1.00 |
| 608 | D445 | 335.2 | | -0.85 | 1613 | D445 | 345.0 | | 0.23 |
| 621 | | ---- | | ---- | 1622 | D445 | 336.2 | | -0.74 |
| 631 | D445 | 342.74 | | -0.02 | 1631 | | ---- | | ---- |
| 663 | D445 | 340.56 | | -0.26 | 1643 | D445 | 335.54 | | -0.81 |
| 671 | | ---- | | ---- | 1710 | | ---- | | ---- |
| 750 | D445 | 335.2 | | -0.85 | 1720 | | ---- | | ---- |
| 753 | D445 | 331.71 | | -1.23 | 1724 | D445 | 347.2 | | 0.48 |
| 759 | ISO3104 | 332.5 | | -1.15 | 1728 | ISO3104 | 336.7 | | -0.68 |
| 824 | ISO3104 | 332.8 | | -1.11 | 1740 | ISO3104 | 339.5 | | -0.37 |
| 825 | D445 | 337.6 | | -0.58 | 1741 | ISO3104 | 337.31 | | -0.62 |
| 851 | ISO3104 | 349.0 | | 0.67 | 1796 | ISO3104 | 333.57 | | -1.03 |
| 855 | ISO3104 | 344.8 | | 0.21 | 1807 | | ---- | | ---- |
| 857 | ISO3104 | 341.24 | | -0.18 | 1832 | ISO3104 | 349.853 | | 0.77 |
| 858 | D445 | 346.6 | | 0.41 | 1833 | ISO3104 | 352.2 | | 1.03 |
| 859 | D445 | 343.7 | | 0.09 | 1849 | | ---- | | ---- |
| 862 | D445 | 350.80 | | 0.87 | 1857 | ISO3104 | 333.3 | | -1.06 |
| 863 | D445 | 339.82 | | -0.34 | 1862 | ISO3104 | 334.1 | | -0.97 |
| 864 | D445 | 343.2 | | 0.03 | 1881 | D445 | 333.00 | | -1.09 |
| 865 | ISO3104 | 348.8 | | 0.65 | 1906 | | ---- | | ---- |
| 866 | D445 | 340.5 | | -0.26 | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|---------------|---------|----------|---------|---------|------|---------|---------|------|---------|
| 1937 | | ---- | | ---- | 6024 | ISO3104 | 332.5 | | -1.15 |
| 1938 | | ---- | | ---- | 6026 | D445 | 334.711 | | -0.90 |
| 1943 | | ---- | | ---- | 6028 | ISO3104 | 341 | | -0.21 |
| 1956 | ISO3104 | 261.5 | R(0.01) | -8.98 | 6039 | | ---- | | ---- |
| 1962 | D445 | 353.81 | | 1.21 | 6049 | ISO3104 | 336.7 | | -0.68 |
| 1964 | | ---- | | ---- | 6051 | D445 | 330.1 | | -1.41 |
| 1967 | D445 | 335.077 | | -0.86 | 6057 | ISO3104 | 343.9 | | 0.11 |
| 1971 | | ---- | | ---- | 6075 | ISO3104 | 335.1 | | -0.86 |
| 1986 | ISO3104 | 336.4 | | -0.72 | 6092 | D445 | 333.9 | | -0.99 |
| 1995 | D445 | 369.21 | | 2.90 | 6109 | | ---- | | ---- |
| 6004 | D445 | 328.535 | | -1.58 | 6112 | | ---- | | ---- |
| 6016 | | ---- | | ---- | 6114 | D445 | 337.00 | | -0.65 |
| 6021 | ISO3104 | 333.68 | | -1.02 | 6122 | | ---- | | ---- |
| | | | | | | | | | |
| normality | | OK | | | | | | | |
| n | | 126 | | | | | | | |
| outliers | | 2 | | | | | | | |
| mean (n) | | 342.8884 | | | | | | | |
| st.dev. (n) | | 8.65178 | | | | | | | |
| R(calc.) | | 24.2250 | | | | | | | |
| R(ISO3104:94) | | 25.3737 | | | | | | | |

Lab 1099 first reported: 293.91



Determination of Kinematic Viscosity at 100°C on sample #17105; results in mm²/s

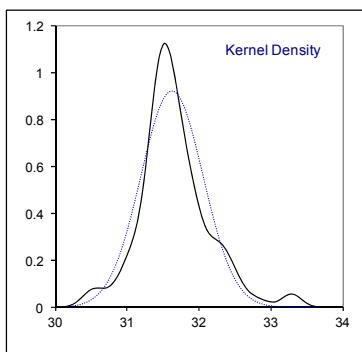
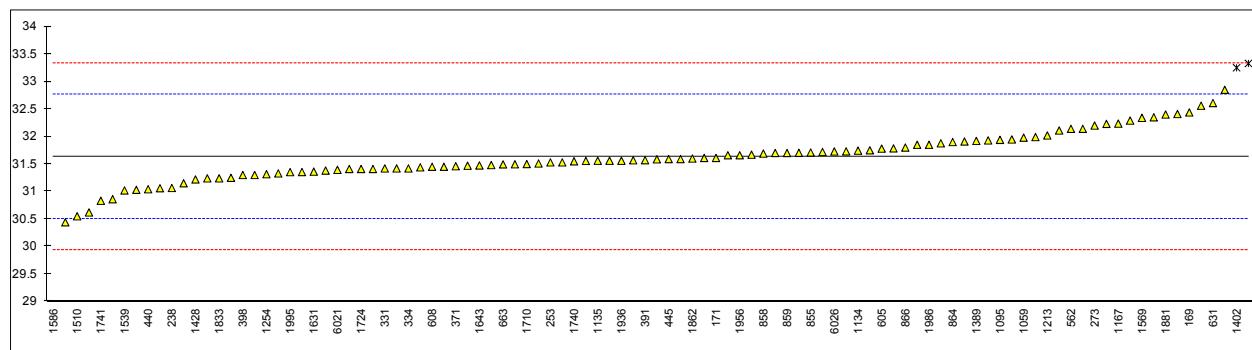
| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|---------|---------|---------|---------|------|---------|-----------|---------|---------|
| 62 | | ---- | | ----- | 870 | D445 | 31.72 | | 0.17 |
| 90 | | ---- | | ----- | 886 | | ---- | | ----- |
| 92 | | ---- | | ----- | 902 | | ---- | | ----- |
| 120 | | ---- | | ----- | 904 | D445 | 32.23 | | 1.07 |
| 131 | | ---- | | ----- | 912 | | ---- | | ----- |
| 140 | ISO3104 | 31.67 | | 0.08 | 913 | | ---- | | ----- |
| 150 | D445 | 31.42 | | -0.36 | 922 | | ---- | | ----- |
| 158 | | ---- | | ----- | 962 | ISO3104 | 31.47 | | -0.27 |
| 159 | | ---- | | ----- | 963 | ISO3104 | 31.70 | | 0.13 |
| 168 | | ---- | | ----- | 971 | | ---- | | ----- |
| 169 | D445 | 32.438 | | 1.44 | 974 | D445 | 32.41 | | 1.39 |
| 171 | ISO3104 | 31.61 | | -0.03 | 982 | D445 | 31.99 | | 0.64 |
| 175 | | ---- | | ----- | 997 | D445 | 31.61 | | -0.03 |
| 194 | | ---- | | ----- | 1006 | | ---- | | ----- |
| 212 | | ---- | | ----- | 1011 | ISO3104 | 30.62 | | -1.78 |
| 221 | | ---- | | ----- | 1059 | ISO3104 | 31.98 | | 0.63 |
| 224 | | ---- | | ----- | 1065 | D445 | 32.56 | | 1.65 |
| 225 | D445 | 32.29 | | 1.17 | 1082 | ISO3104 | 31.947 | | 0.57 |
| 237 | | ---- | | ----- | 1095 | ISO3104 | 31.94 | | 0.56 |
| 238 | D445 | 31.064 | | -0.99 | 1099 | | ---- | | ----- |
| 252 | | ---- | | ----- | 1109 | D445 | 31.568 | | -0.10 |
| 253 | D445 | 31.53 | C | -0.17 | 1126 | | ---- | | ----- |
| 254 | | ---- | | ----- | 1134 | D445 | 31.743506 | | 0.21 |
| 273 | D445 | 32.2 | | 1.01 | 1135 | ISO3104 | 31.56 | | -0.12 |
| 311 | ISO3104 | 31.73 | | 0.18 | 1161 | | ---- | | ----- |
| 313 | ISO3104 | 31.44 | | -0.33 | 1167 | ISO3104 | 32.235 | | 1.08 |
| 323 | ISO3104 | 31.30 | | -0.58 | 1177 | | ---- | | ----- |
| 331 | ISO3104 | 31.42 | | -0.36 | 1191 | ISO3104 | 31.381 | | -0.43 |
| 333 | ISO3104 | 31.41 | | -0.38 | 1213 | D445 | 32.02 | | 0.70 |
| 334 | ISO3104 | 31.42 | | -0.36 | 1229 | | ---- | | ----- |
| 336 | | ---- | | ----- | 1233 | | ---- | | ----- |
| 337 | | ---- | | ----- | 1254 | D445 | 31.315 | | -0.55 |
| 342 | | ---- | | ----- | 1259 | ISO3104 | 32.8503 | | 2.16 |
| 343 | ISO3104 | 33.329 | R(0.05) | 3.01 | 1275 | | ---- | | ----- |
| 349 | | ---- | | ----- | 1299 | D445 | 31.66 | | 0.06 |
| 351 | ISO3104 | 31.355 | | -0.48 | 1345 | | ---- | | ----- |
| 371 | D445 | 31.46 | | -0.29 | 1356 | | ---- | | ----- |
| 391 | ISO3104 | 31.57 | | -0.10 | 1367 | IP71 | 32.11 | | 0.86 |
| 398 | ISO3104 | 31.300 | | -0.58 | 1389 | D445 | 31.92 | | 0.52 |
| 399 | | ---- | | ----- | 1402 | ISO3104 | 33.25 | R(0.05) | 2.87 |
| 440 | D445 | 31.0417 | C | -1.03 | 1404 | ISO3104 | 31.59 | | -0.06 |
| 444 | | ---- | | ----- | 1412 | D445 | 32.35 | | 1.28 |
| 445 | IP71 | 31.59 | | -0.06 | 1428 | ISO3104 | 31.22 | | -0.72 |
| 447 | D445 | 32.14 | | 0.91 | 1431 | | ---- | | ----- |
| 463 | | ---- | | ----- | 1459 | | ---- | | ----- |
| 511 | | ---- | | ----- | 1488 | ISO3104 | 31.55628 | | -0.12 |
| 541 | D445 | 31.877 | | 0.44 | 1510 | D445 | 30.55 | | -1.90 |
| 562 | D445 | 32.14 | | 0.91 | 1539 | ISO3104 | 31.02 | | -1.07 |
| 575 | D445 | 31.51 | | -0.20 | 1556 | ISO3104 | 31.249 | | -0.67 |
| 603 | | ---- | | ----- | 1569 | D445 | 32.34 | | 1.26 |
| 604 | | ---- | | ----- | 1584 | ISO3104 | 31.481 | | -0.26 |
| 605 | D445 | 31.78 | | 0.27 | 1586 | ISO3104 | 17.07 | R(0.01) | -25.71 |
| 608 | D445 | 31.45 | | -0.31 | 1613 | D445 | 31.06 | | -1.00 |
| 621 | | ---- | | ----- | 1622 | D445 | 30.44 | | -2.09 |
| 631 | D445 | 32.609 | | 1.74 | 1631 | ISO3104 | 31.362 | | -0.47 |
| 663 | D445 | 31.494 | | -0.23 | 1643 | D445 | 31.474 | | -0.27 |
| 671 | | ---- | | ----- | 1710 | ISO3104 | 31.50 | | -0.22 |
| 750 | | ---- | | ----- | 1720 | | ---- | | ----- |
| 753 | D445 | 31.329 | | -0.52 | 1724 | D445 | 31.41 | | -0.38 |
| 759 | | ---- | | ----- | 1728 | ISO3104 | 31.56 | | -0.12 |
| 824 | ISO3104 | 31.75 | | 0.22 | 1740 | ISO3104 | 31.55 | | -0.13 |
| 825 | D445 | 31.15 | | -0.84 | 1741 | ISO3104 | 30.832 | | -1.40 |
| 851 | | ---- | | ----- | 1796 | | ---- | | ----- |
| 855 | ISO3104 | 31.71 | | 0.15 | 1807 | ISO3104 | 31.24 | | -0.68 |
| 857 | | ---- | | ----- | 1832 | | ---- | | ----- |
| 858 | D445 | 31.69 | | 0.11 | 1833 | ISO3104 | 31.24 | | -0.68 |
| 859 | D445 | 31.70 | | 0.13 | 1849 | ISO3104 | 31.41 | | -0.38 |
| 862 | D445 | 31.929 | | 0.54 | 1857 | ISO3104 | 31.45 | | -0.31 |
| 863 | D445 | 31.704 | | 0.14 | 1862 | ISO3104 | 31.60 | | -0.05 |
| 864 | D445 | 31.90 | | 0.48 | 1881 | D445 | 32.400 | | 1.37 |
| 865 | ISO3104 | 31.85 | | 0.40 | 1906 | | ---- | | ----- |
| 866 | D445 | 31.80 | | 0.31 | 1936 | ISO3104 | 31.56 | | -0.12 |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|---------|--------|------|---------|------|---------|--------|------|---------|
| 1937 | ISO3104 | 31.495 | | -0.23 | 6024 | ISO3104 | 31.53 | | -0.17 |
| 1938 | ISO3104 | 31.586 | | -0.07 | 6026 | D445 | 31.729 | | 0.18 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | ISO3104 | 31.66 | | 0.06 | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | | ---- | | ---- |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | | ---- | | ---- | 6057 | ISO3104 | 31.91 | | 0.50 |
| 1971 | ISO3104 | 31.031 | | -1.05 | 6075 | | ---- | | ---- |
| 1986 | ISO3104 | 31.85 | | 0.40 | 6092 | | ---- | | ---- |
| 1995 | D445 | 31.353 | | -0.48 | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | | ---- | | ---- | 6114 | D445 | 31.785 | | 0.28 |
| 6021 | ISO3104 | 31.394 | | -0.41 | 6122 | ISO3104 | 30.86 | | -1.35 |

normality OK
n 99
outliers 3
mean (n) 31.6256
st.dev. (n) 0.43363
R(calc.) 1.2142
R(ISO3104:94) 1.5850

Lab 253 first reported: 33.53

Lab 440 reported the test result 31.0417 mm²/s under 50°C instead of 100°C

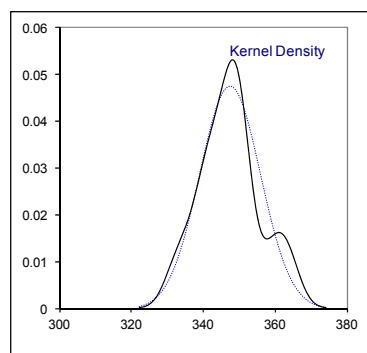
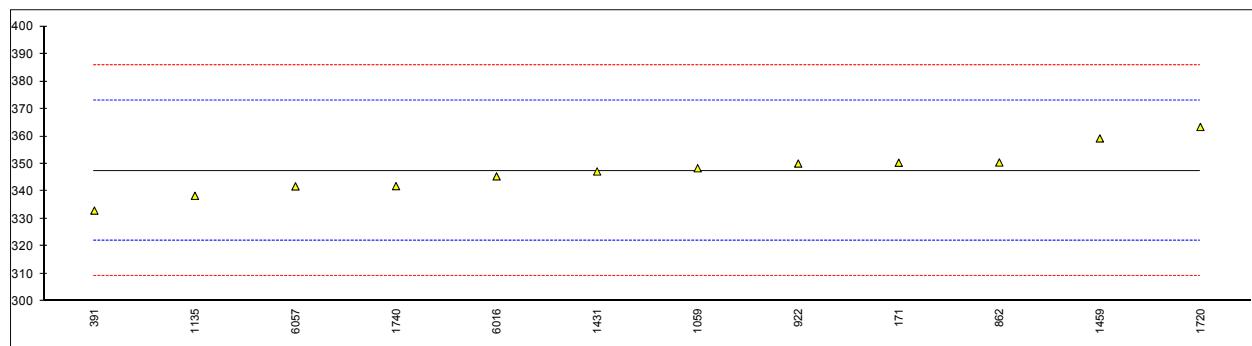


Determination of Viscosity Stabinger at 50°C on sample #17105; results in mm²/s

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|--------|--------|------|---------|------|--------|--------|------|---------|
| 62 | | ---- | | | 870 | | ---- | | ---- |
| 90 | | ---- | | | 886 | | ---- | | ---- |
| 92 | | ---- | | | 902 | | ---- | | ---- |
| 120 | | ---- | | | 904 | | ---- | | ---- |
| 131 | | ---- | | | 912 | | ---- | | ---- |
| 140 | | ---- | | | 913 | | ---- | | ---- |
| 150 | | ---- | | | 922 | D7042 | 350.1 | | 0.20 |
| 158 | | ---- | | | 962 | | ---- | | ---- |
| 159 | | ---- | | | 963 | | ---- | | ---- |
| 168 | | ---- | | | 971 | | ---- | | ---- |
| 169 | | ---- | | | 974 | | ---- | | ---- |
| 171 | D7042 | 350.4 | | 0.23 | 982 | | ---- | | ---- |
| 175 | | ---- | | | 997 | | ---- | | ---- |
| 194 | | ---- | | | 1006 | | ---- | | ---- |
| 212 | | ---- | | | 1011 | | ---- | | ---- |
| 221 | | ---- | | | 1059 | D7042 | 348.4 | | 0.07 |
| 224 | | ---- | | | 1065 | | ---- | | ---- |
| 225 | | ---- | | | 1082 | | ---- | | ---- |
| 237 | | ---- | | | 1095 | | ---- | | ---- |
| 238 | | ---- | | | 1099 | | ---- | | ---- |
| 252 | | ---- | | | 1109 | | ---- | | ---- |
| 253 | | ---- | | | 1126 | | ---- | | ---- |
| 254 | | ---- | | | 1134 | | ---- | | ---- |
| 273 | | ---- | | | 1135 | D7042 | 338.37 | | -0.71 |
| 311 | | ---- | | | 1161 | | ---- | | ---- |
| 313 | | ---- | | | 1167 | | ---- | | ---- |
| 323 | | ---- | | | 1177 | | ---- | | ---- |
| 331 | | ---- | | | 1191 | | ---- | | ---- |
| 333 | | ---- | | | 1213 | | ---- | | ---- |
| 334 | | ---- | | | 1229 | | ---- | | ---- |
| 336 | | ---- | | | 1233 | | ---- | | ---- |
| 337 | | ---- | | | 1254 | | ---- | | ---- |
| 342 | | ---- | | | 1259 | | ---- | | ---- |
| 343 | | ---- | | | 1275 | | ---- | | ---- |
| 349 | | ---- | | | 1299 | | ---- | | ---- |
| 351 | | ---- | | | 1345 | | ---- | | ---- |
| 371 | | ---- | | | 1356 | | ---- | | ---- |
| 391 | D7042 | 333.0 | | -1.13 | 1367 | | ---- | | ---- |
| 398 | | ---- | | | 1389 | | ---- | | ---- |
| 399 | | ---- | | | 1402 | | ---- | | ---- |
| 440 | | ---- | | | 1404 | | ---- | | ---- |
| 444 | | ---- | | | 1412 | | ---- | | ---- |
| 445 | | ---- | | | 1428 | | ---- | | ---- |
| 447 | | ---- | | | 1431 | D7042 | 347.23 | | -0.02 |
| 463 | | ---- | | | 1459 | D7042 | 359.25 | | 0.92 |
| 511 | | ---- | | | 1488 | | ---- | | ---- |
| 541 | | ---- | | | 1510 | | ---- | | ---- |
| 562 | | ---- | | | 1539 | | ---- | | ---- |
| 575 | | ---- | | | 1556 | | ---- | | ---- |
| 603 | | ---- | | | 1569 | | ---- | | ---- |
| 604 | | ---- | | | 1584 | | ---- | | ---- |
| 605 | | ---- | | | 1586 | | ---- | | ---- |
| 608 | | ---- | | | 1613 | | ---- | | ---- |
| 621 | | ---- | | | 1622 | | ---- | | ---- |
| 631 | | ---- | | | 1631 | | ---- | | ---- |
| 663 | | ---- | | | 1643 | | ---- | | ---- |
| 671 | | ---- | | | 1710 | | ---- | | ---- |
| 750 | | ---- | | | 1720 | D7042 | 363.4 | | 1.25 |
| 753 | | ---- | | | 1724 | | ---- | | ---- |
| 759 | | ---- | | | 1728 | | ---- | | ---- |
| 824 | | ---- | | | 1740 | D7042 | 341.9 | | -0.44 |
| 825 | | ---- | | | 1741 | | ---- | | ---- |
| 851 | | ---- | | | 1796 | | ---- | | ---- |
| 855 | | ---- | | | 1807 | | ---- | | ---- |
| 857 | | ---- | | | 1832 | | ---- | | ---- |
| 858 | | ---- | | | 1833 | | ---- | | ---- |
| 859 | | ---- | | | 1849 | | ---- | | ---- |
| 862 | D7042 | 350.49 | | 0.24 | 1857 | | ---- | | ---- |
| 863 | | ---- | | | 1862 | | ---- | | ---- |
| 864 | | ---- | | | 1881 | | ---- | | ---- |
| 865 | | ---- | | | 1906 | | ---- | | ---- |
| 866 | | ---- | | | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|--------|--------|------|---------|------|--------|-------|------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | | ---- | | ---- |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | | ---- | | ---- |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | | ---- | | ---- | 6057 | D7042 | 341.8 | | -0.44 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | | ---- | | ---- | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | D7042 | 345.45 | | -0.16 | 6114 | | ---- | | ---- |
| 6021 | | ---- | | ---- | 6122 | | ---- | | ---- |

normality OK
n 12
outliers 0
mean (n) 347.4825
st.dev. (n) 8.40736
R(calc.) 23.5406
R(D7042:16e3) 35.7560

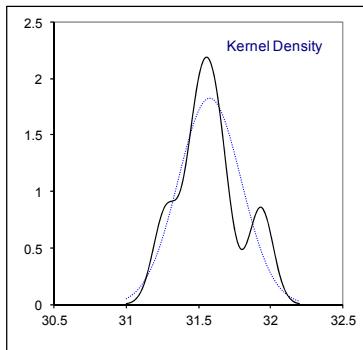
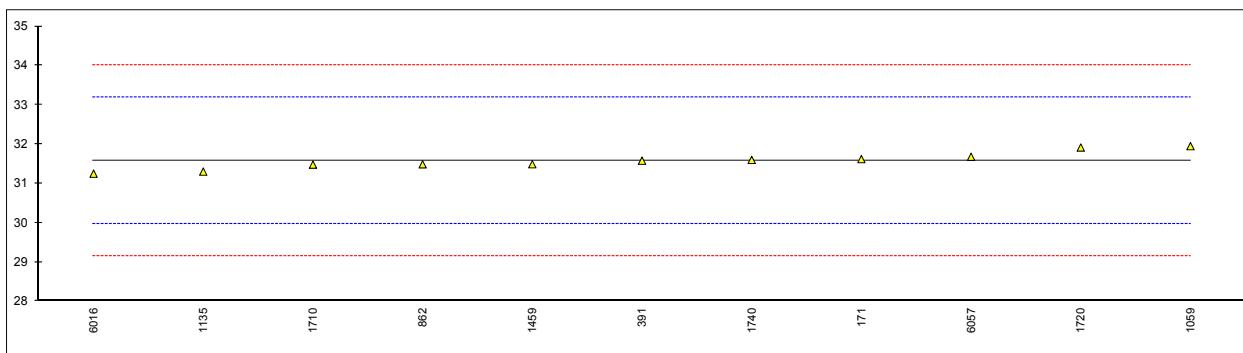


Determination of Viscosity Stabinger at 100°C on sample #17105; results in mm²/s

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|--------|--------|------|---------|------|--------|--------|------|---------|
| 62 | | ---- | | | 870 | | ---- | | ---- |
| 90 | | ---- | | | 886 | | ---- | | ---- |
| 92 | | ---- | | | 902 | | ---- | | ---- |
| 120 | | ---- | | | 904 | | ---- | | ---- |
| 131 | | ---- | | | 912 | | ---- | | ---- |
| 140 | | ---- | | | 913 | | ---- | | ---- |
| 150 | | ---- | | | 922 | | ---- | | ---- |
| 158 | | ---- | | | 962 | | ---- | | ---- |
| 159 | | ---- | | | 963 | | ---- | | ---- |
| 168 | | ---- | | | 971 | | ---- | | ---- |
| 169 | | ---- | | | 974 | | ---- | | ---- |
| 171 | D7042 | 31.62 | | 0.05 | 982 | | ---- | | ---- |
| 175 | | ---- | | | 997 | | ---- | | ---- |
| 194 | | ---- | | | 1006 | | ---- | | ---- |
| 212 | | ---- | | | 1011 | | ---- | | ---- |
| 221 | | ---- | | | 1059 | D7042 | 31.95 | | 0.46 |
| 224 | | ---- | | | 1065 | | ---- | | ---- |
| 225 | | ---- | | | 1082 | | ---- | | ---- |
| 237 | | ---- | | | 1095 | | ---- | | ---- |
| 238 | | ---- | | | 1099 | | ---- | | ---- |
| 252 | | ---- | | | 1109 | | ---- | | ---- |
| 253 | | ---- | | | 1126 | | ---- | | ---- |
| 254 | | ---- | | | 1134 | | ---- | | ---- |
| 273 | | ---- | | | 1135 | D7042 | 31.302 | | -0.34 |
| 311 | | ---- | | | 1161 | | ---- | | ---- |
| 313 | | ---- | | | 1167 | | ---- | | ---- |
| 323 | | ---- | | | 1177 | | ---- | | ---- |
| 331 | | ---- | | | 1191 | | ---- | | ---- |
| 333 | | ---- | | | 1213 | | ---- | | ---- |
| 334 | | ---- | | | 1229 | | ---- | | ---- |
| 336 | | ---- | | | 1233 | | ---- | | ---- |
| 337 | | ---- | | | 1254 | | ---- | | ---- |
| 342 | | ---- | | | 1259 | | ---- | | ---- |
| 343 | | ---- | | | 1275 | | ---- | | ---- |
| 349 | | ---- | | | 1299 | | ---- | | ---- |
| 351 | | ---- | | | 1345 | | ---- | | ---- |
| 371 | | ---- | | | 1356 | | ---- | | ---- |
| 391 | D7042 | 31.58 | | 0.00 | 1367 | | ---- | | ---- |
| 398 | | ---- | | | 1389 | | ---- | | ---- |
| 399 | | ---- | | | 1402 | | ---- | | ---- |
| 440 | | ---- | | | 1404 | | ---- | | ---- |
| 444 | | ---- | | | 1412 | | ---- | | ---- |
| 445 | | ---- | | | 1428 | | ---- | | ---- |
| 447 | | ---- | | | 1431 | | ---- | | ---- |
| 463 | | ---- | | | 1459 | D7042 | 31.49 | | -0.11 |
| 511 | | ---- | | | 1488 | | ---- | | ---- |
| 541 | | ---- | | | 1510 | | ---- | | ---- |
| 562 | | ---- | | | 1539 | | ---- | | ---- |
| 575 | | ---- | | | 1556 | | ---- | | ---- |
| 603 | | ---- | | | 1569 | | ---- | | ---- |
| 604 | | ---- | | | 1584 | | ---- | | ---- |
| 605 | | ---- | | | 1586 | | ---- | | ---- |
| 608 | | ---- | | | 1613 | | ---- | | ---- |
| 621 | | ---- | | | 1622 | | ---- | | ---- |
| 631 | | ---- | | | 1631 | | ---- | | ---- |
| 663 | | ---- | | | 1643 | | ---- | | ---- |
| 671 | | ---- | | | 1710 | D7042 | 31.48 | | -0.12 |
| 750 | | ---- | | | 1720 | D7042 | 31.916 | | 0.42 |
| 753 | | ---- | | | 1724 | | ---- | | ---- |
| 759 | | ---- | | | 1728 | | ---- | | ---- |
| 824 | | ---- | | | 1740 | D7042 | 31.60 | | 0.03 |
| 825 | | ---- | | | 1741 | | ---- | | ---- |
| 851 | | ---- | | | 1796 | | ---- | | ---- |
| 855 | | ---- | | | 1807 | | ---- | | ---- |
| 857 | | ---- | | | 1832 | | ---- | | ---- |
| 858 | | ---- | | | 1833 | | ---- | | ---- |
| 859 | | ---- | | | 1849 | | ---- | | ---- |
| 862 | D7042 | 31.488 | | -0.11 | 1857 | | ---- | | ---- |
| 863 | | ---- | | | 1862 | | ---- | | ---- |
| 864 | | ---- | | | 1881 | | ---- | | ---- |
| 865 | | ---- | | | 1906 | | ---- | | ---- |
| 866 | | ---- | | | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|--------|--------|------|---------|------|--------|-------|------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | | ---- | | ---- |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | | ---- | | ---- |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | | ---- | | ---- | 6057 | D7042 | 31.68 | | 0.13 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | | ---- | | ---- | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | D7042 | 31.249 | | -0.41 | 6114 | | ---- | | ---- |
| 6021 | | ---- | | ---- | 6122 | | ---- | | ---- |

normality OK
n 11
outliers 0
mean (n) 31.5777
st.dev. (n) 0.21798
R(calc.) 0.6103
R(D7042:16e3) 2.2692



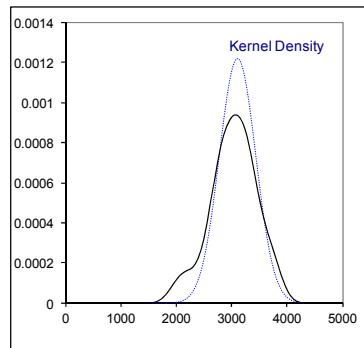
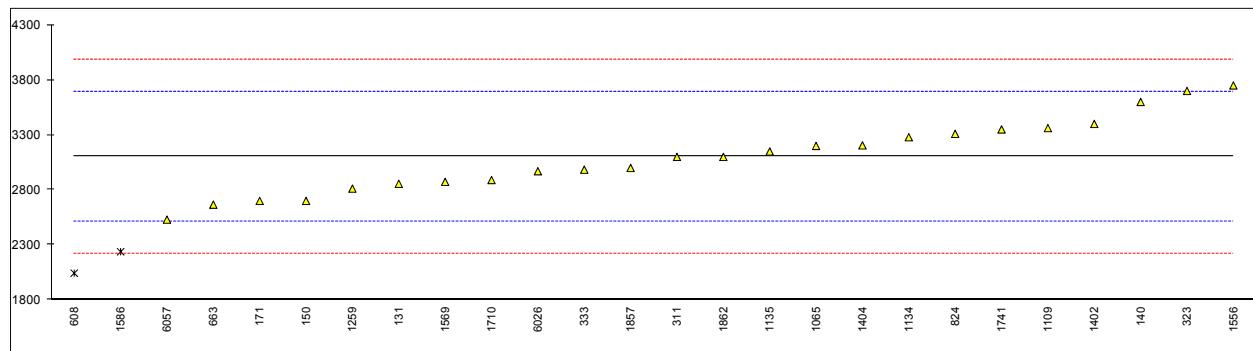
Determination of Nitrogen on sample #17105; results in mg/kg

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|-------------------|---------|-----------|---------|------|-------------------|----------|---------|---------|
| 62 | | ---- | | ---- | 870 | | ---- | | ---- |
| 90 | | ---- | | ---- | 886 | | ---- | | ---- |
| 92 | | ---- | | ---- | 902 | | ---- | | ---- |
| 120 | | ---- | | ---- | 904 | | ---- | | ---- |
| 131 | D5762 Gravimetric | 2855.68 | | -0.84 | 912 | | ---- | | ---- |
| 140 | D5762 Volumetric | 3600 | | 1.68 | 913 | | ---- | | ---- |
| 150 | D5762 Gravimetric | 2700 | | -1.37 | 922 | | ---- | | ---- |
| 158 | | ---- | | ---- | 962 | | ---- | | ---- |
| 159 | | ---- | | ---- | 963 | | ---- | | ---- |
| 168 | | ---- | | ---- | 971 | | ---- | | ---- |
| 169 | | ---- | | ---- | 974 | | ---- | | ---- |
| 171 | D5762 Gravimetric | 2700 | | -1.37 | 982 | | ---- | | ---- |
| 175 | | ---- | | ---- | 997 | | ---- | | ---- |
| 194 | | ---- | | ---- | 1006 | | ---- | | ---- |
| 212 | | ---- | | ---- | 1011 | | ---- | | ---- |
| 221 | | ---- | | ---- | 1059 | | ---- | | ---- |
| 224 | | ---- | | ---- | 1065 | D5762 Gravimetric | 3200 | | 0.33 |
| 225 | | ---- | | ---- | 1082 | | ---- | | ---- |
| 237 | | ---- | | ---- | 1095 | | ---- | | ---- |
| 238 | | ---- | | ---- | 1099 | | ---- | | ---- |
| 252 | | ---- | | ---- | 1109 | D4629 | 3362 | | 0.88 |
| 253 | | ---- | | ---- | 1126 | | ---- | | ---- |
| 254 | | ---- | | ---- | 1134 | D3228 | 3279.356 | | 0.60 |
| 273 | | ---- | | ---- | 1135 | D5762 Volumetric | 3149.8 | | 0.16 |
| 311 | D5762 Volumetric | 3100 | | -0.01 | 1161 | | ---- | | ---- |
| 313 | | ---- | | ---- | 1167 | | ---- | | ---- |
| 323 | D5762 Gravimetric | 3700 | | 2.02 | 1177 | | ---- | | ---- |
| 331 | | ---- | | ---- | 1191 | | ---- | | ---- |
| 333 | D5762 Volumetric | 2984 | | -0.41 | 1213 | | ---- | | ---- |
| 334 | | ---- | | ---- | 1229 | | ---- | | ---- |
| 336 | | ---- | | ---- | 1233 | | ---- | | ---- |
| 337 | | ---- | | ---- | 1254 | | ---- | | ---- |
| 342 | | ---- | | ---- | 1259 | D4629 | 2811.67 | | -0.99 |
| 343 | | ---- | | ---- | 1275 | | ---- | | ---- |
| 349 | | ---- | | ---- | 1299 | | ---- | | ---- |
| 351 | | ---- | | ---- | 1345 | | ---- | | ---- |
| 371 | | ---- | | ---- | 1356 | | ---- | | ---- |
| 391 | | ---- | | ---- | 1367 | | ---- | | ---- |
| 398 | | ---- | | ---- | 1389 | | ---- | | ---- |
| 399 | | ---- | | ---- | 1402 | D5762 Volumetric | 3400 | | 1.01 |
| 440 | | ---- | | ---- | 1404 | D5762 Volumetric | 3205 | | 0.34 |
| 444 | | ---- | | ---- | 1412 | | ---- | | ---- |
| 445 | | ---- | | ---- | 1428 | | ---- | | ---- |
| 447 | | ---- | | ---- | 1431 | | ---- | | ---- |
| 463 | | ---- | | ---- | 1459 | | ---- | | ---- |
| 511 | | ---- | | ---- | 1488 | | ---- | | ---- |
| 541 | | ---- | | ---- | 1510 | | ---- | | ---- |
| 562 | | ---- | | ---- | 1539 | | ---- | | ---- |
| 575 | | ---- | | ---- | 1556 | D5762 Gravimetric | 3750 | | 2.19 |
| 603 | | ---- | | ---- | 1569 | D4629 | 2873 | | -0.78 |
| 604 | | ---- | | ---- | 1584 | | ---- | | ---- |
| 605 | | ---- | | ---- | 1586 | D5762 Gravimetric | 2238 | R(0.05) | -2.94 |
| 608 | D5762 Gravimetric | 2043 | C,R(0.05) | -3.60 | 1613 | | ---- | | ---- |
| 621 | | ---- | | ---- | 1622 | | ---- | | ---- |
| 631 | | ---- | | ---- | 1631 | | ---- | | ---- |
| 663 | D5762 Volumetric | 2666 | | -1.48 | 1643 | | ---- | | ---- |
| 671 | | ---- | | ---- | 1710 | MSZ11794 | 2890 | | -0.72 |
| 750 | | ---- | | ---- | 1720 | | ---- | | ---- |
| 753 | | ---- | | ---- | 1724 | | ---- | | ---- |
| 759 | | ---- | | ---- | 1728 | | ---- | | ---- |
| 824 | D5762 Gravimetric | 3310 | | 0.70 | 1740 | | ---- | | ---- |
| 825 | | ---- | | ---- | 1741 | D5762 Volumetric | 3350.0 | | 0.84 |
| 851 | | ---- | | ---- | 1796 | | ---- | | ---- |
| 855 | | ---- | | ---- | 1807 | | ---- | | ---- |
| 857 | | ---- | | ---- | 1832 | | ---- | | ---- |
| 858 | | ---- | | ---- | 1833 | | ---- | | ---- |
| 859 | | ---- | | ---- | 1849 | | ---- | | ---- |
| 862 | | ---- | | ---- | 1857 | D5762 Volumetric | 3000 | | -0.35 |
| 863 | | ---- | | ---- | 1862 | D5762 Volumetric | 3100 | | -0.01 |
| 864 | | ---- | | ---- | 1881 | | ---- | | ---- |
| 865 | | ---- | | ---- | 1906 | | ---- | | ---- |
| 866 | | ---- | | ---- | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|--------|-------|------|---------|------|-------------------|-------|------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | D5762 Gravimetric | 2970 | | -0.45 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | | ---- | | ---- |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | | ---- | | ---- | 6057 | D5762 Gravimetric | 2530 | | -1.95 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | | ---- | | ---- | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | | ---- | | ---- | 6114 | | ---- | | ---- |
| 6021 | | ---- | | ---- | 6122 | | ---- | | ---- |

| | | <u>Volumetric only</u> | <u>Gravimetric only</u> |
|-------------|---------|------------------------|-------------------------|
| normality | OK | OK | OK |
| n | 24 | 10 | 9 |
| outliers | 2 | 0 | 2 |
| mean (n) | 3103.60 | 3155.48 | 3079.52 |
| st.dev. (n) | 327.386 | 257.560 | 440.783 |
| R(calc.) | 916.68 | 721.17 | 1234.19 |
| R(D5762:12) | 825.56 | 839.36 | 819.15 |

Lab 608 first reported: 1893.03



Determination of Pour Point (Lower) on sample #17105; results in °C

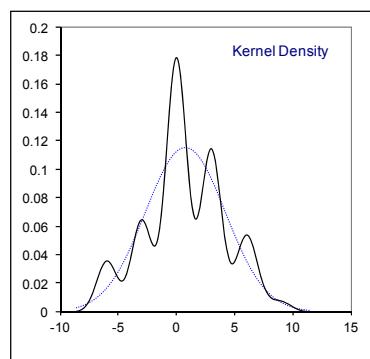
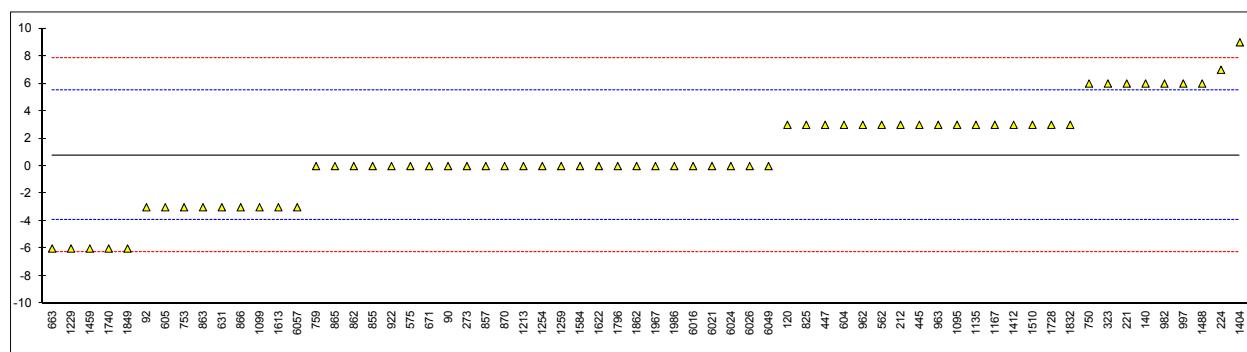
| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|---------|-------|------|---------|------|---------|-------|------|---------|
| 62 | | ---- | | | 870 | ISO3016 | 0 | | -0.33 |
| 90 | D97 | 0 | | -0.33 | 886 | | ---- | | ---- |
| 92 | D97 | -3 | | -1.60 | 902 | | ---- | | ---- |
| 120 | D97 | 3 | | 0.95 | 904 | | ---- | | ---- |
| 131 | | ---- | | | 912 | | ---- | | ---- |
| 140 | ISO3016 | 6 | | 2.22 | 913 | | ---- | | ---- |
| 150 | | ---- | | | 922 | D97 | 0 | | -0.33 |
| 158 | | ---- | | | 962 | ISO3016 | 3 | | 0.95 |
| 159 | | ---- | | | 963 | ISO3016 | 3 | | 0.95 |
| 168 | | ---- | | | 971 | | ---- | | ---- |
| 169 | | ---- | | | 974 | | ---- | | ---- |
| 171 | | ---- | | | 982 | D97 | 6 | | 2.22 |
| 175 | | ---- | | | 997 | D97 | 6 | | 2.22 |
| 194 | | ---- | | | 1006 | | ---- | | ---- |
| 212 | ISO3016 | 3 | | 0.95 | 1011 | | ---- | | ---- |
| 221 | D97 | 6 | | 2.22 | 1059 | | ---- | | ---- |
| 224 | D97 | 7.0 | | 2.65 | 1065 | | ---- | | ---- |
| 225 | | ---- | | | 1082 | | ---- | | ---- |
| 237 | | ---- | | | 1095 | ISO3016 | 3 | | 0.95 |
| 238 | | ---- | | | 1099 | ISO3016 | -3 | | -1.60 |
| 252 | | ---- | | | 1109 | | ---- | | ---- |
| 253 | | ---- | | | 1126 | | ---- | | ---- |
| 254 | | ---- | | | 1134 | | ---- | | ---- |
| 273 | D97 | 0 | | -0.33 | 1135 | ISO3016 | 3 | | 0.95 |
| 311 | | ---- | | | 1161 | | ---- | | ---- |
| 313 | | ---- | | | 1167 | ISO3016 | 3 | | 0.95 |
| 323 | ISO3016 | 6 | | 2.22 | 1177 | | ---- | | ---- |
| 331 | | ---- | | | 1191 | | ---- | | ---- |
| 333 | | ---- | | | 1213 | D97 | 0 | | -0.33 |
| 334 | | ---- | | | 1229 | ISO3016 | -6 | | -2.87 |
| 336 | | ---- | | | 1233 | | ---- | | ---- |
| 337 | | ---- | | | 1254 | D97 | 0 | | -0.33 |
| 342 | | ---- | | | 1259 | ISO3016 | 0 | | -0.33 |
| 343 | | ---- | | | 1275 | | ---- | | ---- |
| 349 | | ---- | | | 1299 | | ---- | | ---- |
| 351 | | ---- | | | 1345 | | ---- | | ---- |
| 371 | | ---- | | | 1356 | | ---- | | ---- |
| 391 | | ---- | | | 1367 | | ---- | | ---- |
| 398 | | ---- | | | 1389 | | ---- | | ---- |
| 399 | | ---- | | | 1402 | | ---- | | ---- |
| 440 | | ---- | | | 1404 | ISO3016 | 9 | | 3.50 |
| 444 | | ---- | | | 1412 | D97 | 3 | | 0.95 |
| 445 | D97 | 3 | | 0.95 | 1428 | | ---- | | ---- |
| 447 | D97 | 3 | | 0.95 | 1431 | | ---- | | ---- |
| 463 | | ---- | | | 1459 | ISO3016 | -6 | C | -2.87 |
| 511 | | ---- | | | 1488 | ISO3016 | 6.0 | | 2.22 |
| 541 | | ---- | | | 1510 | D97 | 3 | | 0.95 |
| 562 | D97 | 3 | | 0.95 | 1539 | | ---- | | ---- |
| 575 | D97 | 0 | | -0.33 | 1556 | | ---- | | ---- |
| 603 | | ---- | | | 1569 | | ---- | | ---- |
| 604 | D97 | 3 | | 0.95 | 1584 | ISO3016 | 0 | | -0.33 |
| 605 | D97 | -3 | | -1.60 | 1586 | | ---- | | ---- |
| 608 | | ---- | | | 1613 | D97 | -3 | | -1.60 |
| 621 | | ---- | | | 1622 | D97 | 0 | | -0.33 |
| 631 | D97 | -3 | | -1.60 | 1631 | | ---- | | ---- |
| 663 | D97 | -6 | | -2.87 | 1643 | | ---- | | ---- |
| 671 | D97 | 0 | | -0.33 | 1710 | | ---- | | ---- |
| 750 | D97 | 6 | | 2.22 | 1720 | | ---- | | ---- |
| 753 | D97 | -3 | | -1.60 | 1724 | | ---- | W | ---- |
| 759 | ISO3016 | 0 | | -0.33 | 1728 | ISO3016 | 3 | | 0.95 |
| 824 | | ---- | | | 1740 | ISO3016 | -6 | | -2.87 |
| 825 | D97 | 3 | | 0.95 | 1741 | | ---- | | ---- |
| 851 | | ---- | | | 1796 | ISO3016 | 0 | | -0.33 |
| 855 | D97 | 0 | | -0.33 | 1807 | | ---- | | ---- |
| 857 | ISO3016 | 0 | | -0.33 | 1832 | ISO3016 | 3 | | 0.95 |
| 858 | | ---- | | | 1833 | | ---- | | ---- |
| 859 | | ---- | | | 1849 | ISO3016 | -6 | | -2.87 |
| 862 | ISO3016 | 0 | | -0.33 | 1857 | | ---- | | ---- |
| 863 | D97 | -3 | | -1.60 | 1862 | ISO3016 | 0 | | -0.33 |
| 864 | | ---- | | | 1881 | | ---- | | ---- |
| 865 | ISO3016 | 0 | | -0.33 | 1906 | | ---- | | ---- |
| 866 | D97 | -3 | | -1.60 | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|---------|-------|------|---------|------|---------|-------|------|---------|
| 1937 | | ---- | | ---- | 6024 | ISO3016 | 0 | | -0.33 |
| 1938 | | ---- | | ---- | 6026 | D97 | 0 | | -0.33 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | D97 | 0 | | -0.33 |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | D97 | 0 | | -0.33 | 6057 | ISO3016 | -3 | | -1.60 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | ISO3016 | 0 | | -0.33 | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | D5853 | 0 | | -0.33 | 6114 | | ---- | | ---- |
| 6021 | ISO3016 | 0 | | -0.33 | 6122 | | ---- | | ---- |

normality OK
n 64
outliers 0
mean (n) 0.77
st.dev. (n) 3.449
R(calc.) 9.66
R(ISO3016:94) 6.59

Lab 1459 first reported: -9

Lab 1724 first reported: -9

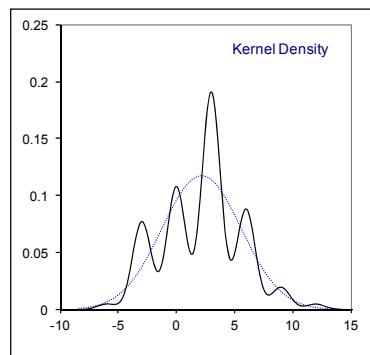
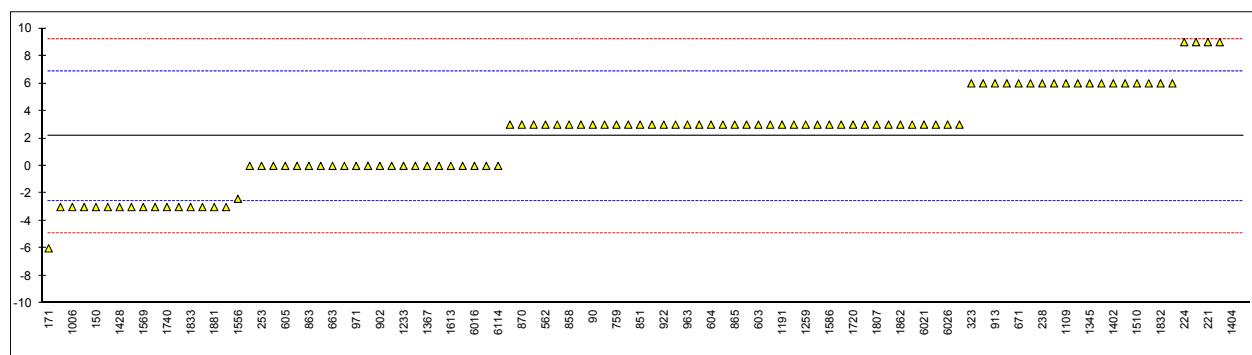


Determination of Pour Point (Upper) on sample #17105; results in °C

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|---------|-------|------|---------|------|---------|-------|------|---------|
| 62 | | ---- | | | 870 | D97 | 3 | | 0.35 |
| 90 | D97 | 3 | | 0.35 | 886 | | ---- | | ---- |
| 92 | D97 | 0 | | -0.92 | 902 | D97 | 0 | | -0.92 |
| 120 | | ---- | | | 904 | D97 | 0 | | -0.92 |
| 131 | | ---- | | | 912 | | ---- | | ---- |
| 140 | | ---- | | | 913 | D97 | 6 | | 1.63 |
| 150 | D97 | -3 | | -2.20 | 922 | D97 | 3 | | 0.35 |
| 158 | | ---- | | | 962 | ISO3016 | 3 | | 0.35 |
| 159 | D97 | 6 | | 1.63 | 963 | ISO3016 | 3 | | 0.35 |
| 168 | | ---- | | | 971 | D97 | 0 | | -0.92 |
| 169 | D97 | 3 | | 0.35 | 974 | D97 | 0 | | -0.92 |
| 171 | D97 | -6 | | -3.47 | 982 | D97 | 9 | | 2.90 |
| 175 | | ---- | | | 997 | D97 | 6 | | 1.63 |
| 194 | D97 | 6 | | 1.63 | 1006 | D97 | -3 | | -2.20 |
| 212 | | ---- | | | 1011 | D97 | -3 | | -2.20 |
| 221 | D97 | 9 | | 2.90 | 1059 | | ---- | | ---- |
| 224 | D97 | 9.0 | | 2.90 | 1065 | | ---- | | ---- |
| 225 | | ---- | | | 1082 | | ---- | | ---- |
| 237 | D97 | -3 | | -2.20 | 1095 | | ---- | | ---- |
| 238 | D97 | 6 | | 1.63 | 1099 | | ---- | | ---- |
| 252 | D97 | 3 | | 0.35 | 1109 | D97 | 6 | | 1.63 |
| 253 | D97 | 0 | | -0.92 | 1126 | | ---- | | ---- |
| 254 | D97 | 3 | | 0.35 | 1134 | | ---- | | ---- |
| 273 | | ---- | | | 1135 | ISO3016 | 3 | | 0.35 |
| 311 | | ---- | | | 1161 | | ---- | | ---- |
| 313 | | ---- | | | 1167 | ISO3016 | 6 | | 1.63 |
| 323 | ISO3016 | 6 | | 1.63 | 1177 | | ---- | | ---- |
| 331 | | ---- | | | 1191 | ISO3016 | 3 | | 0.35 |
| 333 | | ---- | | | 1213 | | ---- | | ---- |
| 334 | | ---- | | | 1229 | | ---- | | ---- |
| 336 | | ---- | | | 1233 | ISO3016 | 0 | | -0.92 |
| 337 | | ---- | | | 1254 | D97 | 3 | | 0.35 |
| 342 | ISO3016 | -3 | | -2.20 | 1259 | ISO3016 | 3 | | 0.35 |
| 343 | | ---- | | | 1275 | | ---- | | ---- |
| 349 | | ---- | | | 1299 | | ---- | | ---- |
| 351 | | ---- | | | 1345 | D97 | 6.0 | | 1.63 |
| 371 | ISO3016 | 3 | | 0.35 | 1356 | ISO3016 | 0 | | -0.92 |
| 391 | ISO3016 | 0 | | -0.92 | 1367 | D97 | 0 | | -0.92 |
| 398 | ISO3016 | 0 | | -0.92 | 1389 | D97 | 6 | | 1.63 |
| 399 | | ---- | | | 1402 | ISO3016 | 6 | | 1.63 |
| 440 | | ---- | | | 1404 | ISO3016 | 12 | | 4.17 |
| 444 | | ---- | | | 1412 | D97 | 6 | | 1.63 |
| 445 | D97 | 6 | | 1.63 | 1428 | ISO3016 | -3 | | -2.20 |
| 447 | | ---- | | | 1431 | D97 | -3 | | -2.20 |
| 463 | | ---- | | | 1459 | | ---- | | ---- |
| 511 | | ---- | | | 1488 | ISO3016 | 9.0 | | 2.90 |
| 541 | | ---- | | | 1510 | D97 | 6 | | 1.63 |
| 562 | D97 | 3 | | 0.35 | 1539 | ISO3016 | 0 | | -0.92 |
| 575 | | ---- | | | 1556 | ISO3016 | -2.4 | | -1.94 |
| 603 | D97 | 3 | | 0.35 | 1569 | D97 | -3 | | -2.20 |
| 604 | D97 | 3 | | 0.35 | 1584 | ISO3016 | 3 | | 0.35 |
| 605 | D97 | 0 | | -0.92 | 1586 | D97 | 3 | | 0.35 |
| 608 | | ---- | | | 1613 | D97 | 0 | | -0.92 |
| 621 | | ---- | | | 1622 | D97 | 0 | | -0.92 |
| 631 | | ---- | | | 1631 | | ---- | | ---- |
| 663 | D97 | 0 | | -0.92 | 1643 | D97 | 3 | | 0.35 |
| 671 | D97 | 6 | | 1.63 | 1710 | | ---- | | ---- |
| 750 | | ---- | | | 1720 | D97 | 3 | | 0.35 |
| 753 | D97 | 3 | | 0.35 | 1724 | D97 | -3 | | -2.20 |
| 759 | ISO3016 | 3 | | 0.35 | 1728 | ISO3016 | 6 | | 1.63 |
| 824 | ISO3016 | 3 | | 0.35 | 1740 | ISO3016 | -3 | | -2.20 |
| 825 | | ---- | | | 1741 | ISO3016 | -3 | | -2.20 |
| 851 | ISO3016 | 3 | | 0.35 | 1796 | ISO3016 | 3 | | 0.35 |
| 855 | ISO3016 | 3 | | 0.35 | 1807 | D97 | 3 | | 0.35 |
| 857 | ISO3016 | 3 | | 0.35 | 1832 | ISO3016 | 6 | | 1.63 |
| 858 | D97 | 3 | | 0.35 | 1833 | | -3 | | -2.20 |
| 859 | D97 | 3 | | 0.35 | 1849 | ISO3016 | -3 | | -2.20 |
| 862 | ISO3016 | 0 | | -0.92 | 1857 | ISO3016 | 3 | | 0.35 |
| 863 | D97 | 0 | | -0.92 | 1862 | ISO3016 | 3 | | 0.35 |
| 864 | D97 | 3 | | 0.35 | 1881 | D97 | -3 | | -2.20 |
| 865 | ISO3016 | 3 | | 0.35 | 1906 | | ---- | | ---- |
| 866 | D97 | 0 | | -0.92 | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|---------|-------|------|---------|------|---------|-------|---------|---------|
| 1937 | | ---- | | ---- | 6024 | ISO3016 | 3 | | 0.35 |
| 1938 | | ---- | | ---- | 6026 | D97 | 3 | | 0.35 |
| 1943 | | ---- | | ---- | 6028 | ISO3016 | 24 | R(0.01) | 9.27 |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | D97 | 3 | | 0.35 |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | D97 | 6 | | 1.63 | 6057 | ISO3016 | 0 | | -0.92 |
| 1971 | ISO3016 | -3.0 | | -2.20 | 6075 | | ---- | | ---- |
| 1986 | ISO3016 | 3 | | 0.35 | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | D5853 | 0 | | -0.92 | 6114 | D97 | 0 | | -0.92 |
| 6021 | ISO3016 | 3 | | 0.35 | 6122 | | ---- | | ---- |

normality OK
n 101
outliers 1
mean (n) 2.17
st.dev. (n) 3.415
R(calc.) 9.56
R(ISO3016:94) 6.59

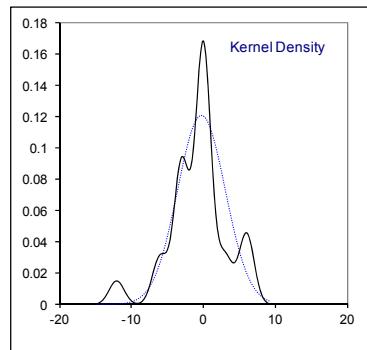
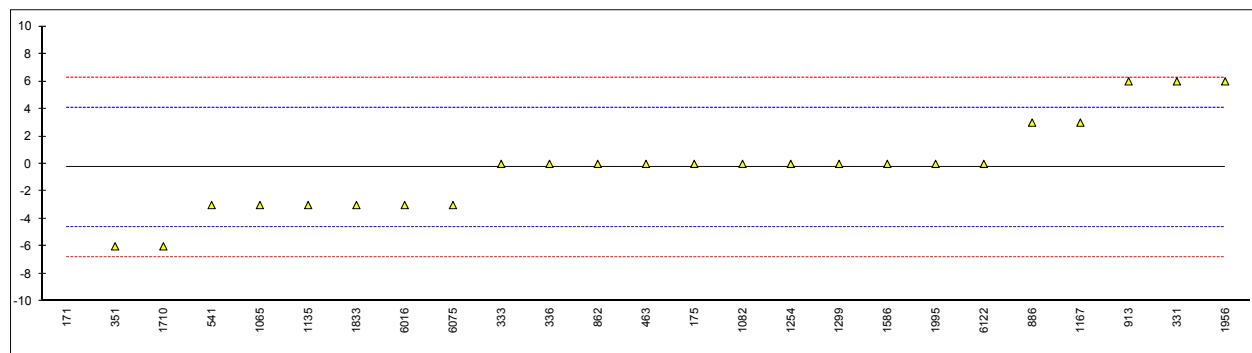


Determination of Pour Point (Automated), 3°C interval on sample #17105; results in °C

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|--------|-------|---------|---------|------|--------|-------|------|---------|
| 62 | | ---- | | | 870 | | ---- | | ---- |
| 90 | | ---- | | | 886 | D5950 | 3 | | 1.49 |
| 92 | | ---- | | | 902 | | ---- | | ---- |
| 120 | | ---- | | | 904 | | ---- | | ---- |
| 131 | | ---- | | | 912 | | ---- | | ---- |
| 140 | | ---- | | | 913 | D6749 | 6 | | 2.87 |
| 150 | | ---- | | | 922 | | ---- | | ---- |
| 158 | | ---- | | | 962 | | ---- | | ---- |
| 159 | | ---- | | | 963 | | ---- | | ---- |
| 168 | | ---- | | | 971 | | ---- | | ---- |
| 169 | | ---- | | | 974 | | ---- | | ---- |
| 171 | D5950 | -12 | R(0.05) | -5.39 | 982 | | ---- | | ---- |
| 175 | D5950 | 0 | | 0.11 | 997 | | ---- | | ---- |
| 194 | | ---- | | | 1006 | | ---- | | ---- |
| 212 | | ---- | | | 1011 | | ---- | | ---- |
| 221 | | ---- | | | 1059 | | ---- | | ---- |
| 224 | | ---- | | | 1065 | D5950 | -3 | | -1.26 |
| 225 | | ---- | | | 1082 | D5950 | 0 | | 0.11 |
| 237 | | ---- | | | 1095 | | ---- | | ---- |
| 238 | | ---- | | | 1099 | | ---- | | ---- |
| 252 | | ---- | | | 1109 | | ---- | | ---- |
| 253 | | ---- | | | 1126 | | ---- | | ---- |
| 254 | | ---- | | | 1134 | | ---- | | ---- |
| 273 | | ---- | | | 1135 | D5950 | -3 | | -1.26 |
| 311 | | ---- | | | 1161 | | ---- | | ---- |
| 313 | | ---- | | | 1167 | D6749 | 3 | | 1.49 |
| 323 | | ---- | | | 1177 | | ---- | | ---- |
| 331 | D5950 | 6.0 | | 2.87 | 1191 | | ---- | | ---- |
| 333 | D5950 | 0 | | 0.11 | 1213 | | ---- | | ---- |
| 334 | | ---- | | | 1229 | | ---- | | ---- |
| 336 | D5950 | 0 | | 0.11 | 1233 | | ---- | | ---- |
| 337 | | ---- | | | 1254 | D5950 | 0 | | 0.11 |
| 342 | | ---- | | | 1259 | | ---- | | ---- |
| 343 | | ---- | | | 1275 | | ---- | | ---- |
| 349 | | ---- | | | 1299 | D97 | 0 | | 0.11 |
| 351 | D6749 | -6 | | -2.64 | 1345 | | ---- | | ---- |
| 371 | | ---- | | | 1356 | | ---- | | ---- |
| 391 | | ---- | | | 1367 | | ---- | | ---- |
| 398 | | ---- | | | 1389 | | ---- | | ---- |
| 399 | | ---- | | | 1402 | | ---- | | ---- |
| 440 | | ---- | | | 1404 | | ---- | | ---- |
| 444 | | ---- | | | 1412 | | ---- | | ---- |
| 445 | | ---- | | | 1428 | | ---- | | ---- |
| 447 | | ---- | | | 1431 | | ---- | | ---- |
| 463 | D6892 | 0.0 | | 0.11 | 1459 | | ---- | | ---- |
| 511 | | ---- | | | 1488 | | ---- | | ---- |
| 541 | D5950 | -3 | | -1.26 | 1510 | | ---- | | ---- |
| 562 | | ---- | | | 1539 | | ---- | | ---- |
| 575 | | ---- | | | 1556 | | ---- | | ---- |
| 603 | | ---- | | | 1569 | | ---- | | ---- |
| 604 | | ---- | | | 1584 | | ---- | | ---- |
| 605 | | ---- | | | 1586 | D5950 | 0 | | 0.11 |
| 608 | | ---- | | | 1613 | | ---- | | ---- |
| 621 | | ---- | | | 1622 | | ---- | | ---- |
| 631 | | ---- | | | 1631 | | ---- | | ---- |
| 663 | | ---- | | | 1643 | | ---- | | ---- |
| 671 | | ---- | | | 1710 | D97 | -6 | | -2.64 |
| 750 | | ---- | | | 1720 | | ---- | | ---- |
| 753 | | ---- | | | 1724 | | ---- | | ---- |
| 759 | | ---- | | | 1728 | | ---- | | ---- |
| 824 | | ---- | | | 1740 | | ---- | | ---- |
| 825 | | ---- | | | 1741 | | ---- | | ---- |
| 851 | | ---- | | | 1796 | | ---- | | ---- |
| 855 | | ---- | | | 1807 | | ---- | | ---- |
| 857 | | ---- | | | 1832 | | ---- | | ---- |
| 858 | | ---- | | | 1833 | D5950 | -3 | | -1.26 |
| 859 | | ---- | | | 1849 | | ---- | | ---- |
| 862 | D5950 | 0 | | 0.11 | 1857 | | ---- | | ---- |
| 863 | | ---- | | | 1862 | | ---- | | ---- |
| 864 | | ---- | | | 1881 | | ---- | | ---- |
| 865 | | ---- | | | 1906 | | ---- | | ---- |
| 866 | | ---- | | | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|--------|-------|------|---------|------|-------------|-------|------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | | ---- | | ---- |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | D5950 | 6 | | 2.87 | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | | ---- | | ---- |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | | ---- | | ---- | 6057 | | ---- | | ---- |
| 1971 | | ---- | | ---- | 6075 | NF T 60-105 | -3 | | -1.26 |
| 1986 | | ---- | | ---- | 6092 | | ---- | | ---- |
| 1995 | | 0 | | 0.11 | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | D5950 | -3 | | -1.26 | 6114 | | ---- | | ---- |
| 6021 | | ---- | | ---- | 6122 | D5950 | 0.0 | | 0.11 |

normality OK
n 24
outliers 1
mean (n) -0.25
st.dev. (n) 3.300
R(calc.) 9.24
R(D5950:14) 6.1



Determination of Sediment by Extraction on sample #17105; results in %M/M

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|--------|--------|---------|---------|------|---------|------------|------|---------|
| 62 | | ---- | | ---- | 870 | D473 | 0.021 | | 0.14 |
| 90 | D473 | 0.028 | | 0.66 | 886 | | ---- | | ---- |
| 92 | D473 | 0.036 | | 1.25 | 902 | D473 | 0.02 | | 0.06 |
| 120 | D473 | 0.01 | | -0.68 | 904 | D473 | 0.018 | | -0.08 |
| 131 | | ---- | | ---- | 912 | | ---- | | ---- |
| 140 | D473 | 0.06 | R(0.01) | 3.02 | 913 | D473 | 0.03 | | 0.80 |
| 150 | D473 | 0.01 | C | -0.68 | 922 | D473 | <0.01 | | ---- |
| 158 | | ---- | | ---- | 962 | D473 | 0.021 | | 0.14 |
| 159 | D473 | 0.012 | | -0.53 | 963 | D473 | 0.015 | | -0.31 |
| 168 | D473 | 0.04 | | 1.54 | 971 | D473 | 0.014 | | -0.38 |
| 169 | | ---- | | ---- | 974 | D473 | 0.014 | | -0.38 |
| 171 | D473 | 0.0029 | | -1.20 | 982 | D473 | 0.0199 | | 0.06 |
| 175 | | ---- | | ---- | 997 | | ---- | | ---- |
| 194 | | ---- | | ---- | 1006 | | ---- | | ---- |
| 212 | D473 | 0.02 | | 0.06 | 1011 | | ---- | | ---- |
| 221 | D473 | 0.0119 | | -0.53 | 1059 | | ---- | | ---- |
| 224 | D473 | 0.0058 | | -0.99 | 1065 | | ---- | | ---- |
| 225 | | ---- | | ---- | 1082 | | ---- | | ---- |
| 237 | | ---- | | ---- | 1095 | | ---- | | ---- |
| 238 | D473 | 0.022 | | 0.21 | 1099 | | ---- | | ---- |
| 252 | D473 | 0.017 | | -0.16 | 1109 | D473 | 0.01 | | -0.68 |
| 253 | | ---- | | ---- | 1126 | | ---- | | ---- |
| 254 | D473 | 0.02 | | 0.06 | 1134 | D473 | 0.00451836 | | -1.08 |
| 273 | D473 | 0.006 | | -0.97 | 1135 | ISO3735 | 0.03 | | 0.80 |
| 311 | D473 | <0.01 | | ---- | 1161 | | ---- | | ---- |
| 313 | | ---- | | ---- | 1167 | | ---- | | ---- |
| 323 | D473 | 0.02 | | 0.06 | 1177 | | ---- | | ---- |
| 331 | | ---- | | ---- | 1191 | | ---- | | ---- |
| 333 | | ---- | | ---- | 1213 | D473 | 0.034 | | 1.10 |
| 334 | | ---- | | ---- | 1229 | | ---- | | ---- |
| 336 | | ---- | | ---- | 1233 | | ---- | | ---- |
| 337 | | ---- | | ---- | 1254 | D473 | 0.016 | | -0.23 |
| 342 | | ---- | | ---- | 1259 | | ---- | | ---- |
| 343 | D473 | 0.00 | | -1.41 | 1275 | | ---- | | ---- |
| 349 | | ---- | | ---- | 1299 | | ---- | | ---- |
| 351 | | ---- | | ---- | 1345 | D473 | 0.012 | | -0.53 |
| 371 | D473 | 0.013 | | -0.45 | 1356 | | ---- | | ---- |
| 391 | | ---- | | ---- | 1367 | | ---- | | ---- |
| 398 | | ---- | | ---- | 1389 | | ---- | | ---- |
| 399 | | ---- | | ---- | 1402 | ISO3735 | 0.03 | | 0.80 |
| 440 | | ---- | | ---- | 1404 | | ---- | | ---- |
| 444 | | ---- | | ---- | 1412 | D473 | 0.013 | | -0.45 |
| 445 | D473 | <0.01 | | ---- | 1428 | D473 | 0.015 | | -0.31 |
| 447 | D473 | 0.02 | | 0.06 | 1431 | | ---- | | ---- |
| 463 | D473 | 0.0167 | | -0.18 | 1459 | | ---- | | ---- |
| 511 | D473 | 0.0229 | | 0.28 | 1488 | | ---- | | ---- |
| 541 | D473 | 0.040 | | 1.54 | 1510 | D473 | 0.02 | | 0.06 |
| 562 | D473 | 0.02 | | 0.06 | 1539 | ISO3735 | 0.0039 | | -1.13 |
| 575 | D473 | 0.024 | | 0.36 | 1556 | ISO3735 | 0.006 | | -0.97 |
| 603 | D473 | 0 | | -1.41 | 1569 | | ---- | | ---- |
| 604 | | ---- | | ---- | 1584 | D473 | 0.018 | | -0.08 |
| 605 | D473 | 0.022 | | 0.21 | 1586 | D473 | 0.02 | | 0.06 |
| 608 | D473 | 0.03 | | 0.80 | 1613 | D473 | 0.029 | | 0.73 |
| 621 | | ---- | | ---- | 1622 | D473 | 0.0292 | | 0.74 |
| 631 | D473 | 0.020 | | 0.06 | 1631 | | ---- | | ---- |
| 663 | D473 | 0.020 | | 0.06 | 1643 | D473 | 0.0288 | | 0.71 |
| 671 | D473 | 0.0241 | C | 0.37 | 1710 | | ---- | | ---- |
| 750 | | ---- | | ---- | 1720 | | ---- | | ---- |
| 753 | D473 | 0.032 | | 0.95 | 1724 | D473 | 0.022 | | 0.21 |
| 759 | D473 | 0.02 | | 0.06 | 1728 | D473 | 0.024 | | 0.36 |
| 824 | D473 | 0.019 | | -0.01 | 1740 | ISO3735 | 0.017 | | -0.16 |
| 825 | | ---- | | ---- | 1741 | | ---- | | ---- |
| 851 | | ---- | | ---- | 1796 | D473 | 0.0186 | | -0.04 |
| 855 | D473 | 0.021 | | 0.14 | 1807 | ISO3735 | 0 | | -1.41 |
| 857 | D473 | 0.023 | | 0.29 | 1832 | ISO3735 | 0.0184 | | -0.05 |
| 858 | D473 | 0.02 | | 0.06 | 1833 | | ---- | | ---- |
| 859 | | ---- | | ---- | 1849 | | ---- | | ---- |
| 862 | D473 | 0.018 | | -0.08 | 1857 | D473 | 0.02 | | 0.06 |
| 863 | D473 | 0.012 | | -0.53 | 1862 | D473 | 0.017 | | -0.16 |
| 864 | D473 | 0.02 | | 0.06 | 1881 | | ---- | | ---- |
| 865 | D473 | 0.015 | | -0.31 | 1906 | | ---- | | ---- |
| 866 | D473 | 0.021 | | 0.14 | 1936 | | ---- | | ---- |

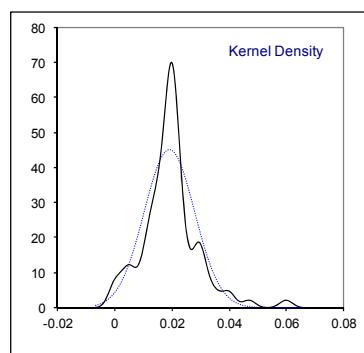
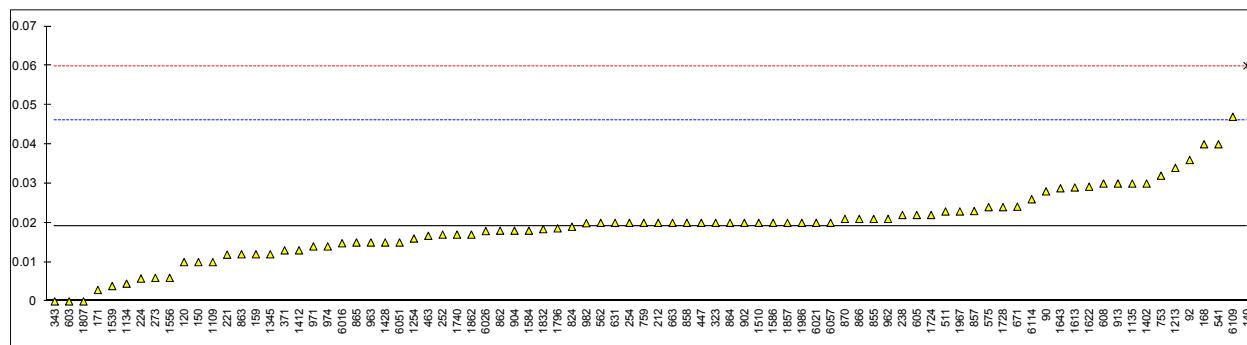
| lab | method | value | mark | z(targ) | Lab | method | value | mark | z(targ) |
|------|--------|--------|------|---------|------|--------|--------|------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | D473 | 0.0179 | | -0.09 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | | ---- | | ---- |
| 1964 | | ---- | | ---- | 6051 | D473 | 0.015 | | -0.31 |
| 1967 | D473 | 0.0229 | | 0.28 | 6057 | D473 | 0.02 | | 0.06 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | D473 | 0.02 | | 0.06 | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | D473 | 0.047 | | 2.06 |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | D473 | 0.0148 | C | -0.32 | 6114 | D473 | 0.026 | | 0.51 |
| 6021 | D473 | 0.020 | | 0.06 | 6122 | | ---- | | ---- |

normality suspect
n 83
outliers 1
mean (n) 0.0191
st.dev. (n) 0.00884
R(calc.) 0.0248
R(D473:07) 0.0379

Lab 150 first reported: 0.06

Lab 671 first reported: 0.0949

Lab 6016 first reported: 0.05

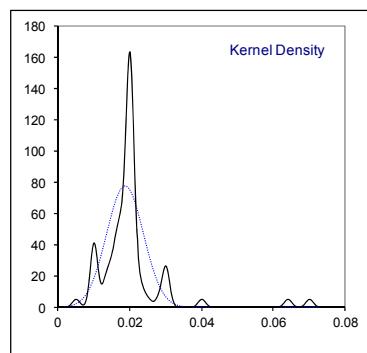
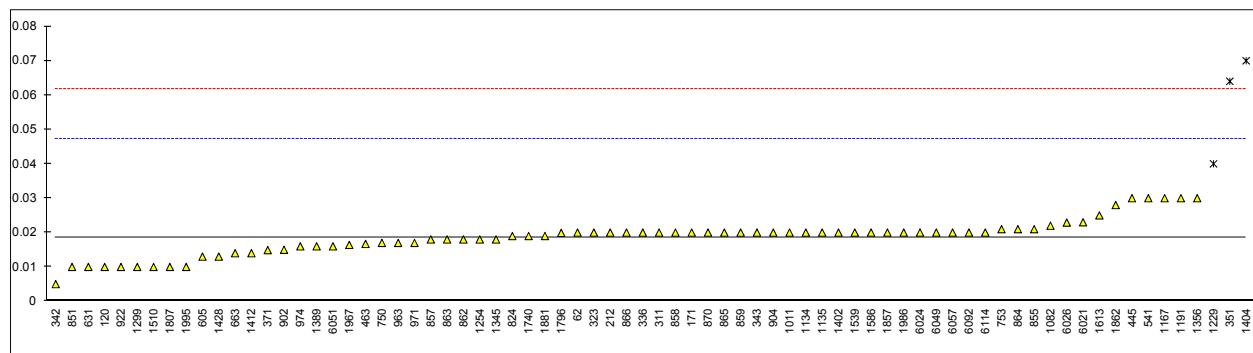


Determination of Total Sediment (Hot filtration) of sample #17105; results in %M/M

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|------------|--------|---------|---------|------|------------|--------|---------|---------|
| 62 | D4870 | 0.02 | | 0.10 | 870 | IP375 | 0.020 | | 0.10 |
| 90 | | ---- | | | 886 | | ---- | | ---- |
| 92 | | ---- | | | 902 | IP375 | 0.015 | | -0.25 |
| 120 | D4870 | 0.01 | | -0.60 | 904 | IP375 | 0.02 | | 0.10 |
| 131 | | ---- | | | 912 | | ---- | | ---- |
| 140 | | ---- | | | 913 | | ---- | | ---- |
| 150 | | ---- | | | 922 | ISO10307-1 | 0.010 | | -0.60 |
| 158 | | ---- | | | 962 | | ---- | | ---- |
| 159 | | ---- | | | 963 | IP375 | 0.017 | | -0.11 |
| 168 | | ---- | | | 971 | IP375 | 0.017 | | -0.11 |
| 169 | | ---- | | | 974 | IP375 | 0.016 | | -0.18 |
| 171 | IP375 | 0.02 | | 0.10 | 982 | | ---- | | ---- |
| 175 | | ---- | | | 997 | | ---- | | ---- |
| 194 | | ---- | | | 1006 | | ---- | | ---- |
| 212 | ISO10307-1 | 0.02 | | 0.10 | 1011 | ISO10307-1 | 0.02 | | 0.10 |
| 221 | | ---- | | | 1059 | | ---- | | ---- |
| 224 | | ---- | | | 1065 | | ---- | | ---- |
| 225 | | ---- | | | 1082 | ISO10307-1 | 0.022 | | 0.24 |
| 237 | | ---- | | | 1095 | | ---- | | ---- |
| 238 | | ---- | | | 1099 | | ---- | | ---- |
| 252 | | ---- | | | 1109 | | ---- | | ---- |
| 253 | | ---- | | | 1126 | | ---- | | ---- |
| 254 | | ---- | | | 1134 | IP375 | 0.020 | | 0.10 |
| 273 | | ---- | | | 1135 | ISO10307-1 | 0.02 | | 0.10 |
| 311 | IP375 | 0.02 | | 0.10 | 1161 | | ---- | | ---- |
| 313 | | ---- | | | 1167 | ISO10307-1 | 0.03 | | 0.79 |
| 323 | IP375 | 0.02 | | 0.10 | 1177 | | ---- | | ---- |
| 331 | | ---- | | | 1191 | ISO10307-1 | 0.030 | | 0.79 |
| 333 | | ---- | | | 1213 | | ---- | | ---- |
| 334 | | ---- | | | 1229 | ISO10307-1 | 0.04 | R(0.01) | 1.49 |
| 336 | IP375 | 0.02 | | 0.10 | 1233 | | ---- | | ---- |
| 337 | | ---- | | | 1254 | IP375 | 0.018 | | -0.04 |
| 342 | ISO10307-1 | 0.005 | | -0.95 | 1259 | | ---- | | ---- |
| 343 | ISO10307-1 | 0.02 | | 0.10 | 1275 | | ---- | | ---- |
| 349 | | ---- | | | 1299 | ISO10307-1 | 0.01 | | -0.60 |
| 351 | ISO10307-1 | 0.064 | R(0.01) | 3.17 | 1345 | ISO10307-1 | 0.018 | | -0.04 |
| 371 | IP375 | 0.0149 | | -0.26 | 1356 | ISO10307-1 | 0.03 | | 0.79 |
| 391 | | ---- | | | 1367 | IP375 | <0.01 | | ---- |
| 398 | | ---- | | | 1389 | ISO10307-1 | 0.016 | | -0.18 |
| 399 | | ---- | | | 1402 | IP375 | 0.02 | | 0.10 |
| 440 | | ---- | | | 1404 | IP375 | 0.07 | R(0.01) | 3.59 |
| 444 | | ---- | | | 1412 | IP375 | 0.014 | | -0.32 |
| 445 | IP375 | 0.03 | | 0.79 | 1428 | ISO10307-1 | 0.013 | | -0.39 |
| 447 | | ---- | | | 1431 | | ---- | | ---- |
| 463 | ISO10307-1 | 0.0167 | | -0.13 | 1459 | | ---- | | ---- |
| 511 | | ---- | | | 1488 | | ---- | | ---- |
| 541 | D4870 | 0.030 | | 0.79 | 1510 | IP375 | 0.01 | | -0.60 |
| 562 | | ---- | | | 1539 | ISO10307-1 | 0.02 | | 0.10 |
| 575 | | ---- | | | 1556 | | ---- | | ---- |
| 603 | | ---- | | | 1569 | | ---- | | ---- |
| 604 | | ---- | | | 1584 | | ---- | | ---- |
| 605 | IP375 | 0.013 | | -0.39 | 1586 | ISO10307-1 | 0.02 | | 0.10 |
| 608 | | ---- | | | 1613 | IP375 | 0.025 | | 0.45 |
| 621 | | ---- | | | 1622 | | ---- | | ---- |
| 631 | D4870 | 0.010 | | -0.60 | 1631 | | ---- | | ---- |
| 663 | IP375 | 0.014 | | -0.32 | 1643 | | ---- | | ---- |
| 671 | | ---- | | | 1710 | | ---- | | ---- |
| 750 | IP375 | 0.017 | | -0.11 | 1720 | | ---- | | ---- |
| 753 | IP375 | 0.021 | | 0.17 | 1724 | | ---- | | ---- |
| 759 | | ---- | | | 1728 | | ---- | | ---- |
| 824 | ISO10307-1 | 0.019 | | 0.03 | 1740 | ISO10307-1 | 0.019 | | 0.03 |
| 825 | | ---- | | | 1741 | | ---- | | ---- |
| 851 | ISO10307-1 | 0.01 | | -0.60 | 1796 | IP375 | 0.0199 | | 0.09 |
| 855 | ISO10307-1 | 0.021 | | 0.17 | 1807 | D4870 | 0.01 | | -0.60 |
| 857 | ISO10307-1 | 0.018 | | -0.04 | 1832 | | ---- | | ---- |
| 858 | D4870 | 0.02 | | 0.10 | 1833 | | ---- | | ---- |
| 859 | ISO10307-1 | 0.02 | | 0.10 | 1849 | | ---- | | ---- |
| 862 | IP375 | 0.018 | | -0.04 | 1857 | IP375 | 0.02 | | 0.10 |
| 863 | D4870 | 0.018 | | -0.04 | 1862 | IP375 | 0.028 | | 0.65 |
| 864 | D4870 | 0.021 | | 0.17 | 1881 | IP375 | 0.019 | | 0.03 |
| 865 | ISO10307-1 | 0.020 | | 0.10 | 1906 | | ---- | | ---- |
| 866 | D4870 | 0.02 | | 0.10 | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | Lab | method | value | mark | z(targ) |
|------|--------|--------|------|---------|------|------------|--------|------|---------|
| 1937 | | ---- | | ---- | 6024 | IP375 | 0.02 | | 0.10 |
| 1938 | | ---- | | ---- | 6026 | IP375 | 0.0229 | | 0.30 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | ISO10307-1 | 0.02 | | 0.10 |
| 1964 | | ---- | | ---- | 6051 | IP375 | 0.016 | | -0.18 |
| 1967 | IP375 | 0.0164 | | -0.15 | 6057 | ISO10307-1 | 0.02 | | 0.10 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | IP375 | 0.02 | | 0.10 | 6092 | IP375 | 0.02 | | 0.10 |
| 1995 | D4870 | 0.01 | | -0.60 | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | | ---- | | ---- | 6114 | ISO10307-1 | 0.020 | | 0.10 |
| 6021 | IP375 | 0.023 | | 0.31 | 6122 | | ---- | | ---- |

normality OK
n 71
outliers 3
mean (n) 0.0186
st.dev. (n) 0.00513
R(calc.) 0.0144
R(IP375:11) 0.0401



Determination of Total Sediment (Accelerated) of sample #17105; results in %M/M

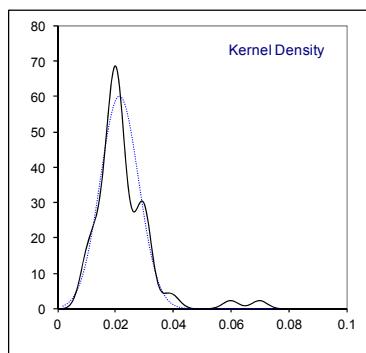
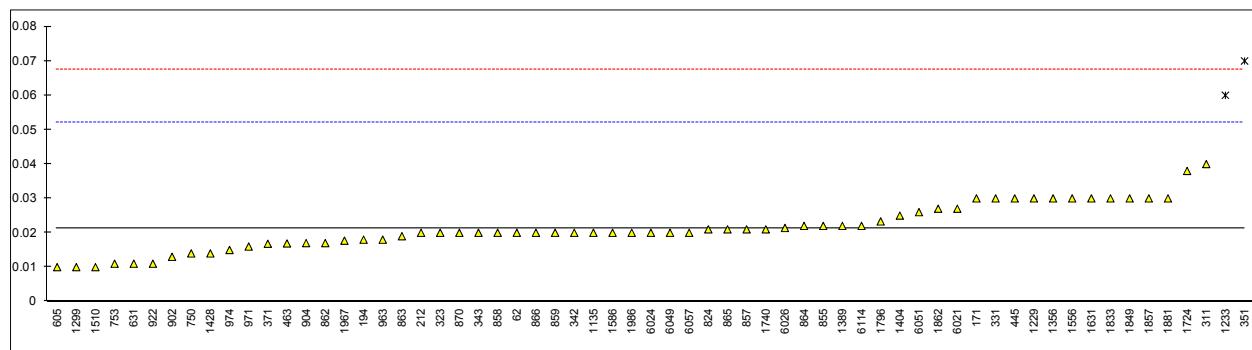
| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|------------|--------|------|---------|------|------------|--------|---------|---------|
| 62 | D4870 | 0.02 | | -0.09 | 870 | IP390 | 0.020 | | -0.09 |
| 90 | | ---- | | ---- | 886 | | ---- | | ---- |
| 92 | | ---- | | ---- | 902 | IP390 | 0.013 | | -0.55 |
| 120 | | ---- | | ---- | 904 | IP390 | 0.017 | | -0.29 |
| 131 | | ---- | | ---- | 912 | | ---- | | ---- |
| 140 | | ---- | | ---- | 913 | | ---- | | ---- |
| 150 | | ---- | | ---- | 922 | ISO10307-2 | 0.011 | | -0.68 |
| 158 | | ---- | | ---- | 962 | | ---- | | ---- |
| 159 | | ---- | | ---- | 963 | IP390 | 0.018 | | -0.22 |
| 168 | | ---- | | ---- | 971 | IP390 | 0.016 | | -0.35 |
| 169 | | ---- | | ---- | 974 | IP390 | 0.015 | | -0.42 |
| 171 | IP390 | 0.03 | | 0.56 | 982 | | ---- | | ---- |
| 175 | | ---- | | ---- | 997 | | ---- | | ---- |
| 194 | ISO10307-2 | 0.018 | | -0.22 | 1006 | | ---- | | ---- |
| 212 | ISO10307-2 | 0.02 | | -0.09 | 1011 | | ---- | | ---- |
| 221 | | ---- | | ---- | 1059 | | ---- | | ---- |
| 224 | | ---- | | ---- | 1065 | | ---- | | ---- |
| 225 | | ---- | | ---- | 1082 | | ---- | | ---- |
| 237 | | ---- | | ---- | 1095 | | ---- | | ---- |
| 238 | | ---- | | ---- | 1099 | | ---- | | ---- |
| 252 | | ---- | | ---- | 1109 | | ---- | | ---- |
| 253 | | ---- | | ---- | 1126 | | ---- | | ---- |
| 254 | | ---- | | ---- | 1134 | | ---- | | ---- |
| 273 | | ---- | | ---- | 1135 | ISO10307-2 | 0.02 | | -0.09 |
| 311 | IP390 | 0.04 | | 1.21 | 1161 | | ---- | | ---- |
| 313 | | ---- | | ---- | 1167 | | ---- | | ---- |
| 323 | IP390 | 0.02 | C | -0.09 | 1177 | | ---- | | ---- |
| 331 | ISO10307-2 | 0.03 | | 0.56 | 1191 | | ---- | | ---- |
| 333 | | ---- | | ---- | 1213 | | ---- | | ---- |
| 334 | | ---- | | ---- | 1229 | ISO10307-2 | 0.03 | | 0.56 |
| 336 | | ---- | | ---- | 1233 | ISO10307-2 | 0.06 | R(0.01) | 2.51 |
| 337 | | ---- | | ---- | 1254 | | ---- | | ---- |
| 342 | ISO10307-2 | 0.02 | C | -0.09 | 1259 | | ---- | | ---- |
| 343 | ISO10307-2 | 0.02 | | -0.09 | 1275 | | ---- | | ---- |
| 349 | | ---- | | ---- | 1299 | ISO10307-2 | 0.01 | | -0.74 |
| 351 | ISO10307-2 | 0.070 | | R(0.01) | 1345 | | ---- | | ---- |
| 371 | IP390 | 0.0168 | | -0.30 | 1356 | ISO10307-2 | 0.03 | | 0.56 |
| 391 | | ---- | | ---- | 1367 | | ---- | | ---- |
| 398 | | ---- | | ---- | 1389 | ISO10307-2 | 0.022 | | 0.04 |
| 399 | | ---- | | ---- | 1402 | | ---- | | ---- |
| 440 | | ---- | | ---- | 1404 | IP390 | 0.025 | | 0.23 |
| 444 | | ---- | | ---- | 1412 | | ---- | | ---- |
| 445 | IP390 | 0.03 | | 0.56 | 1428 | ISO10307-2 | 0.014 | | -0.48 |
| 447 | | ---- | | ---- | 1431 | | ---- | | ---- |
| 463 | ISO10307-2 | 0.0169 | | -0.29 | 1459 | | ---- | | ---- |
| 511 | | ---- | | ---- | 1488 | | ---- | | ---- |
| 541 | | ---- | | ---- | 1510 | IP390 | 0.01 | | -0.74 |
| 562 | | ---- | | ---- | 1539 | | ---- | | ---- |
| 575 | | ---- | | ---- | 1556 | ISO10307-2 | 0.030 | | 0.56 |
| 603 | | ---- | | ---- | 1569 | | ---- | | ---- |
| 604 | | ---- | | ---- | 1584 | | ---- | | ---- |
| 605 | IP390 | 0.010 | | -0.74 | 1586 | ISO10307-2 | 0.02 | | -0.09 |
| 608 | | ---- | | ---- | 1613 | | ---- | | ---- |
| 621 | | ---- | | ---- | 1622 | | ---- | | ---- |
| 631 | D4870 | 0.011 | | -0.68 | 1631 | ISO10307-2 | 0.03 | | 0.56 |
| 663 | | ---- | | ---- | 1643 | | ---- | | ---- |
| 671 | | ---- | | ---- | 1710 | | ---- | | ---- |
| 750 | IP390 | 0.014 | | -0.48 | 1720 | | ---- | | ---- |
| 753 | IP390 | 0.011 | | -0.68 | 1724 | ISO10307-2 | 0.038 | | 1.08 |
| 759 | | ---- | | ---- | 1728 | | ---- | | ---- |
| 824 | ISO10307-2 | 0.021 | | -0.03 | 1740 | ISO10307-2 | 0.021 | | -0.03 |
| 825 | | ---- | | ---- | 1741 | | ---- | | ---- |
| 851 | | ---- | | ---- | 1796 | IP390 | 0.0233 | | 0.12 |
| 855 | ISO10307-2 | 0.022 | | 0.04 | 1807 | | ---- | | ---- |
| 857 | ISO10307-2 | 0.021 | | -0.03 | 1832 | | ---- | | ---- |
| 858 | ISO10307-2 | 0.02 | | -0.09 | 1833 | ISO10307-2 | 0.03 | | 0.56 |
| 859 | ISO10307-2 | 0.02 | | -0.09 | 1849 | ISO10307-2 | 0.03 | | 0.56 |
| 862 | IP390 | 0.017 | | -0.29 | 1857 | IP390 | 0.03 | | 0.56 |
| 863 | D4870 | 0.019 | | -0.16 | 1862 | IP390 | 0.027 | | 0.36 |
| 864 | D4870 | 0.022 | | 0.04 | 1881 | IP390 | 0.030 | | 0.56 |
| 865 | ISO10307-2 | 0.021 | | -0.03 | 1906 | | ---- | | ---- |
| 866 | D4870 | 0.02 | | -0.09 | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|--------|--------|------|---------|------|------------|--------|------|---------|
| 1937 | | ---- | | ---- | 6024 | IP390 | 0.02 | | -0.09 |
| 1938 | | ---- | | ---- | 6026 | IP390 | 0.0214 | | 0.00 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | ISO10307-2 | 0.02 | | -0.09 |
| 1964 | | ---- | | ---- | 6051 | IP390 | 0.026 | | 0.30 |
| 1967 | IP390 | 0.0177 | | -0.24 | 6057 | ISO10307-2 | 0.02 | | -0.09 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | IP390 | 0.02 | | -0.09 | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | | ---- | | ---- | 6114 | ISO10307-2 | 0.022 | | 0.04 |
| 6021 | IP390 | 0.027 | | 0.36 | 6122 | | ---- | | ---- |

normality OK
n 61
outliers 2
mean (n) 0.0214
st.dev. (n) 0.00665
R(calc.) 0.0186
R(IP390:11) 0.0430

Lab 323 first reported: 0.05

Lab 342 first reported: 0

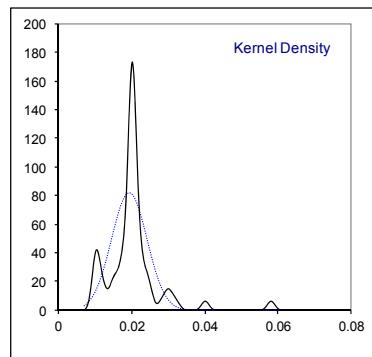
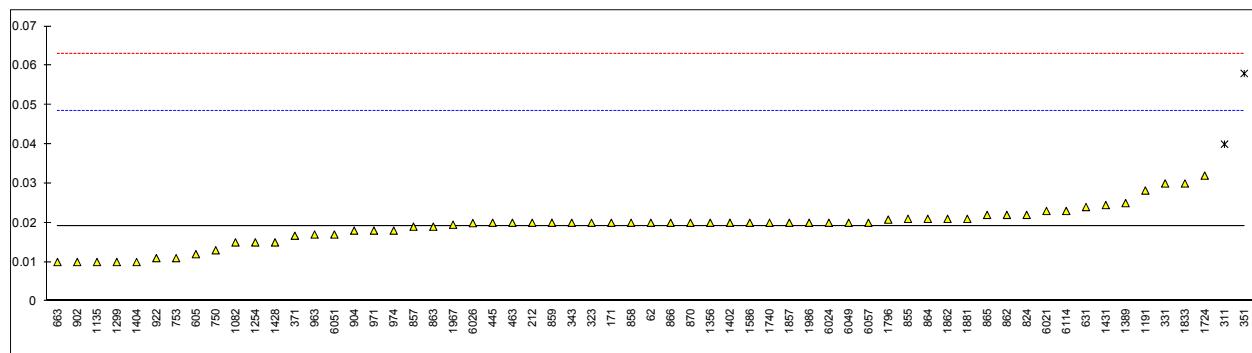


Determination of Total Sediment (Potential) of sample #17105; results in %M/M

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|------------|--------|---------|---------|------|------------|--------|------|---------|
| 62 | D4870 | 0.02 | | 0.05 | 870 | IP390 | 0.020 | | 0.05 |
| 90 | | ---- | | ---- | 886 | | ---- | | ---- |
| 92 | | ---- | | ---- | 902 | IP390 | 0.010 | | -0.63 |
| 120 | | ---- | | ---- | 904 | IP390 | 0.018 | | -0.08 |
| 131 | | ---- | | ---- | 912 | | ---- | | ---- |
| 140 | | ---- | | ---- | 913 | | ---- | | ---- |
| 150 | | ---- | | ---- | 922 | ISO10307-2 | 0.011 | | -0.57 |
| 158 | | ---- | | ---- | 962 | | ---- | | ---- |
| 159 | | ---- | | ---- | 963 | IP390 | 0.017 | | -0.15 |
| 168 | | ---- | | ---- | 971 | IP390 | 0.018 | | -0.08 |
| 169 | | ---- | | ---- | 974 | IP390 | 0.018 | | -0.08 |
| 171 | IP390 | 0.02 | | 0.05 | 982 | | ---- | | ---- |
| 175 | | ---- | | ---- | 997 | | ---- | | ---- |
| 194 | | ---- | | ---- | 1006 | | ---- | | ---- |
| 212 | ISO10307-2 | 0.02 | | 0.05 | 1011 | | ---- | | ---- |
| 221 | | ---- | | ---- | 1059 | | ---- | | ---- |
| 224 | | ---- | | ---- | 1065 | | ---- | | ---- |
| 225 | | ---- | | ---- | 1082 | ISO10307-2 | 0.015 | | -0.29 |
| 237 | | ---- | | ---- | 1095 | | ---- | | ---- |
| 238 | | ---- | | ---- | 1099 | | ---- | | ---- |
| 252 | | ---- | | ---- | 1109 | | ---- | | ---- |
| 253 | | ---- | | ---- | 1126 | | ---- | | ---- |
| 254 | | ---- | | ---- | 1134 | | ---- | | ---- |
| 273 | | ---- | | ---- | 1135 | ISO10307-2 | 0.01 | | -0.63 |
| 311 | IP390 | 0.04 | R(0.01) | 1.43 | 1161 | | ---- | | ---- |
| 313 | | ---- | | ---- | 1167 | | ---- | | ---- |
| 323 | IP390 | 0.02 | | 0.05 | 1177 | | ---- | | ---- |
| 331 | ISO10307-2 | 0.03 | | 0.74 | 1191 | ISO10307-2 | 0.0282 | | 0.62 |
| 333 | | ---- | | ---- | 1213 | | ---- | | ---- |
| 334 | | ---- | | ---- | 1229 | | ---- | | ---- |
| 336 | | ---- | | ---- | 1233 | | ---- | | ---- |
| 337 | | ---- | | ---- | 1254 | IP390 | 0.015 | | -0.29 |
| 342 | ISO10307-2 | <0.01 | | ---- | 1259 | | ---- | | ---- |
| 343 | ISO10307-2 | 0.02 | | 0.05 | 1275 | | ---- | | ---- |
| 349 | | ---- | | ---- | 1299 | ISO10307-2 | 0.01 | | -0.63 |
| 351 | ISO10307-2 | 0.058 | R(0.01) | 2.66 | 1345 | | ---- | | ---- |
| 371 | IP390 | 0.0167 | | -0.17 | 1356 | ISO10307-2 | 0.02 | | 0.05 |
| 391 | | ---- | | ---- | 1367 | IP390 | <0.01 | | ---- |
| 398 | | ---- | | ---- | 1389 | ISO10307-2 | 0.025 | | 0.40 |
| 399 | | ---- | | ---- | 1402 | IP390 | 0.02 | | 0.05 |
| 440 | | ---- | | ---- | 1404 | IP390 | 0.01 | | -0.63 |
| 444 | | ---- | | ---- | 1412 | | ---- | | ---- |
| 445 | IP390 | 0.02 | | 0.05 | 1428 | ISO10307-2 | 0.015 | | -0.29 |
| 447 | | ---- | | ---- | 1431 | D4870 | 0.0245 | | 0.36 |
| 463 | ISO10307-2 | 0.020 | | 0.05 | 1459 | | ---- | | ---- |
| 511 | | ---- | | ---- | 1488 | | ---- | | ---- |
| 541 | | ---- | | ---- | 1510 | | ---- | | ---- |
| 562 | | ---- | | ---- | 1539 | | ---- | | ---- |
| 575 | | ---- | | ---- | 1556 | | ---- | | ---- |
| 603 | | ---- | | ---- | 1569 | | ---- | | ---- |
| 604 | | ---- | | ---- | 1584 | | ---- | | ---- |
| 605 | IP390 | 0.012 | | -0.50 | 1586 | ISO10307-2 | 0.02 | | 0.05 |
| 608 | | ---- | | ---- | 1613 | | ---- | | ---- |
| 621 | | ---- | | ---- | 1622 | | ---- | | ---- |
| 631 | D4870 | 0.024 | | 0.33 | 1631 | | ---- | | ---- |
| 663 | IP390 | 0.010 | | -0.63 | 1643 | | ---- | | ---- |
| 671 | | ---- | | ---- | 1710 | | ---- | | ---- |
| 750 | IP390 | 0.013 | | -0.43 | 1720 | | ---- | | ---- |
| 753 | IP390 | 0.011 | | -0.57 | 1724 | ISO10307-2 | 0.032 | | 0.88 |
| 759 | | ---- | | ---- | 1728 | | ---- | | ---- |
| 824 | ISO10307-2 | 0.022 | | 0.19 | 1740 | ISO10307-2 | 0.020 | | 0.05 |
| 825 | | ---- | | ---- | 1741 | | ---- | | ---- |
| 851 | | ---- | | ---- | 1796 | IP390 | 0.0208 | | 0.11 |
| 855 | ISO10307-2 | 0.021 | | 0.12 | 1807 | | ---- | | ---- |
| 857 | ISO10307-2 | 0.019 | | -0.02 | 1832 | | ---- | | ---- |
| 858 | ISO10307-2 | 0.02 | | 0.05 | 1833 | ISO10307-2 | 0.03 | | 0.74 |
| 859 | ISO10307-2 | 0.02 | | 0.05 | 1849 | | ---- | | ---- |
| 862 | IP390 | 0.022 | | 0.19 | 1857 | IP390 | 0.02 | | 0.05 |
| 863 | D4870 | 0.019 | | -0.02 | 1862 | IP390 | 0.021 | | 0.12 |
| 864 | D4870 | 0.021 | | 0.12 | 1881 | IP390 | 0.021 | | 0.12 |
| 865 | ISO10307-2 | 0.022 | | 0.19 | 1906 | | ---- | | ---- |
| 866 | D4870 | 0.02 | | 0.05 | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|--------|--------|------|---------|------|------------|--------|------|---------|
| 1937 | | ---- | | ---- | 6024 | IP390 | 0.02 | | 0.05 |
| 1938 | | ---- | | ---- | 6026 | IP390 | 0.0199 | | 0.05 |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | | ---- | | ---- | 6049 | ISO10307-2 | 0.02 | | 0.05 |
| 1964 | | ---- | | ---- | 6051 | IP390 | 0.017 | | -0.15 |
| 1967 | IP390 | 0.0195 | | 0.02 | 6057 | ISO10307-2 | 0.02 | | 0.05 |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | IP390 | 0.02 | | 0.05 | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | | ---- | | ---- | 6114 | ISO10307-2 | 0.023 | | 0.26 |
| 6021 | IP390 | 0.023 | | 0.26 | 6122 | | ---- | | ---- |

normality OK
n 59
outliers 2
mean (n) 0.0192
st.dev. (n) 0.00485
R(calc.) 0.0136
R(IP390:11) 0.0408



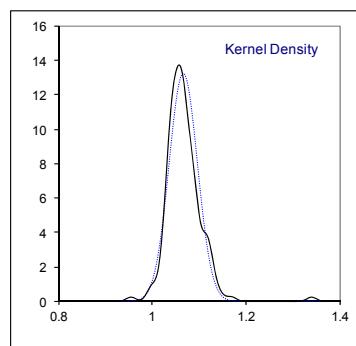
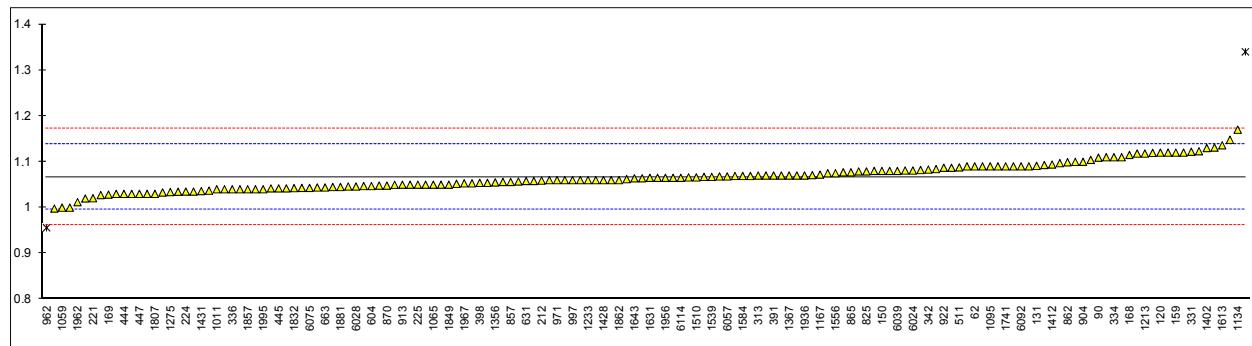
Determination of Total Sulphur on sample #17105; results in %M/M

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|---------|---------|------|---------|------|--------------|--------|---------|---------|
| 62 | D4294 | 1.09 | | 0.65 | 870 | ISO8754 | 1.048 | | -0.54 |
| 90 | D4294 | 1.109 | | 1.19 | 886 | | ----- | | ----- |
| 92 | D4294 | 1.12 | | 1.50 | 902 | ISO8754 | 1.08 | | 0.36 |
| 120 | D4294 | 1.12 | | 1.50 | 904 | D4294 | 1.1 | | 0.93 |
| 131 | D4294 | 1.09110 | | 0.68 | 912 | D4294 | 1.033 | | -0.97 |
| 140 | D4294 | 1.12 | | 1.50 | 913 | D4294 | 1.05 | | -0.49 |
| 150 | D4294 | 1.08 | | 0.36 | 922 | D4294 | 1.087 | | 0.56 |
| 158 | ----- | ----- | | ----- | 962 | ISO8754 | 0.956 | R(0.05) | -3.15 |
| 159 | D4294 | 1.12 | | 1.50 | 963 | ISO8754 | 1.03 | | -1.05 |
| 168 | D4294 | 1.11493 | | 1.35 | 971 | D4294 | 1.06 | | -0.20 |
| 169 | D4294 | 1.0284 | | -1.10 | 974 | D4294 | 1.06 | | -0.20 |
| 171 | D4294 | 1.11 | | 1.21 | 982 | | ----- | | ----- |
| 175 | D4294 | 1.11 | | 1.21 | 997 | D4294 | 1.06 | | -0.20 |
| 194 | ----- | ----- | | ----- | 1006 | D2622 | 1.062 | | -0.15 |
| 212 | ISO8754 | 1.059 | | -0.23 | 1011 | ISO8754 | 1.04 | | -0.77 |
| 221 | D4294 | 1.0206 | | -1.32 | 1059 | ISO14596mod. | 1.00 | | -1.90 |
| 224 | D4294 | 1.035 | | -0.91 | 1065 | D4294 | 1.05 | | -0.49 |
| 225 | D4294 | 1.050 | | -0.49 | 1082 | ISO8754 | 1.058 | | -0.26 |
| 237 | D4294 | 1.057 | | -0.29 | 1095 | ISO8754 | 1.09 | | 0.65 |
| 238 | D4294 | 1.075 | | 0.22 | 1099 | ISO8754 | 1.0274 | | -1.13 |
| 252 | ----- | ----- | | ----- | 1109 | D4294 | 1.05 | | -0.49 |
| 253 | D4294 | 1.09 | | 0.65 | 1126 | ISO20846mod. | 1.04 | | -0.77 |
| 254 | ----- | ----- | | ----- | 1134 | IP336 | 1.17 | | 2.91 |
| 273 | D4294 | 1.02 | | -1.34 | 1135 | ISO8754 | 1.0346 | | -0.92 |
| 311 | D4294 | 1.09 | | 0.65 | 1161 | | ----- | | ----- |
| 313 | D4294 | 1.07 | | 0.08 | 1167 | ISO8754 | 1.072 | | 0.14 |
| 323 | ISO8754 | 1.05 | | -0.49 | 1177 | DIN10304-1 | 1.045 | | -0.63 |
| 331 | ISO8754 | 1.122 | | 1.55 | 1191 | ISO8754 | 1.037 | | -0.85 |
| 333 | ISO8754 | 1.05 | | -0.49 | 1213 | D4294 | 1.118 | | 1.44 |
| 334 | D4294 | 1.11 | | 1.21 | 1229 | ISO8754 | 1.06 | | -0.20 |
| 336 | D4294 | 1.040 | | -0.77 | 1233 | ISO8754 | 1.06 | | -0.20 |
| 337 | D2622 | 1.08 | | 0.36 | 1254 | D4294 | 1.0498 | | -0.49 |
| 342 | ISO8754 | 1.083 | | 0.45 | 1259 | ISO8754 | 1.148 | | 2.29 |
| 343 | IP336 | 1.123 | | 1.58 | 1275 | IP336 | 1.034 | | -0.94 |
| 349 | ----- | ----- | | ----- | 1299 | D2622 | 1.07 | | 0.08 |
| 351 | ISO8754 | 1.118 | | 1.44 | 1345 | D4294 | 1.0691 | | 0.06 |
| 371 | D4294 | 1.048 | | -0.54 | 1356 | ISO8754 | 1.055 | | -0.34 |
| 391 | ISO8754 | 1.07 | | 0.08 | 1367 | D4294 | 1.07 | | 0.08 |
| 398 | ISO8754 | 1.054 | | -0.37 | 1389 | D4294 | 1.00 | | -1.90 |
| 399 | ISO8754 | 1.03 | | -1.05 | 1402 | IP336 | 1.13 | | 1.78 |
| 440 | ----- | ----- | | ----- | 1404 | ISO8754 | 1.06 | | -0.20 |
| 444 | D2622 | 1.03 | | -1.05 | 1412 | D4294 | 1.094 | | 0.76 |
| 445 | IP336 | 1.042 | | -0.71 | 1428 | ISO8754 | 1.06 | | -0.20 |
| 447 | IP336 | 1.03 | | -1.05 | 1431 | D4294 | 1.036 | | -0.88 |
| 463 | ISO8754 | 1.04 | | -0.77 | 1459 | ISO8754 | 1.03 | | -1.05 |
| 511 | D4294 | 1.08771 | | 0.58 | 1488 | ISO8754 | 0.998 | | -1.96 |
| 541 | ----- | ----- | | ----- | 1510 | IP336 | 1.066 | | -0.03 |
| 562 | ----- | ----- | | ----- | 1539 | ISO8754 | 1.067 | | 0.00 |
| 575 | D4294 | 1.09982 | | 0.93 | 1556 | ISO8754 | 1.075 | | 0.22 |
| 603 | D4294 | 1.077 | | 0.28 | 1569 | ISO8754 | 1.097 | | 0.85 |
| 604 | D4294 | 1.047 | | -0.57 | 1584 | ISO8754 | 1.069 | | 0.05 |
| 605 | D4294 | 1.081 | | 0.39 | 1586 | ISO8754 | 1.06 | | -0.20 |
| 608 | D4294 | 1.07 | | 0.08 | 1613 | D4294 | 1.136 | | 1.95 |
| 621 | ----- | ----- | | ----- | 1622 | D4294 | 1.34 | R(0.01) | 7.73 |
| 631 | D4294 | 1.058 | | -0.26 | 1631 | ISO8754 | 1.065 | | -0.06 |
| 663 | D4294 | 1.044 | | -0.66 | 1643 | D1552 | 1.064 | | -0.09 |
| 671 | D4294 | 1.1041 | | 1.05 | 1710 | ISO14596 | 1.046 | | -0.60 |
| 750 | D4294 | 1.06 | | -0.20 | 1720 | D4294 | 1.084 | | 0.48 |
| 753 | D4294 | 1.056 | | -0.32 | 1724 | IP336 | 1.082 | | 0.42 |
| 759 | D4294 | 1.069 | | 0.05 | 1728 | D4294 | 1.065 | | -0.06 |
| 824 | ISO8754 | 1.079 | | 0.34 | 1740 | ISO8754 | 1.09 | | 0.65 |
| 825 | D4294 | 1.079 | | 0.34 | 1741 | ISO8754 | 1.090 | | 0.65 |
| 851 | ISO8754 | 1.093 | | 0.73 | 1796 | ISO8754 | 1.054 | | -0.37 |
| 855 | ISO8754 | 1.044 | | -0.66 | 1807 | ISO8754 | 1.03 | | -1.05 |
| 857 | D4294 | 1.056 | | -0.32 | 1832 | ISO8754 | 1.0425 | | -0.70 |
| 858 | D4294 | 1.066 | | -0.03 | 1833 | ISO8754 | 1.07 | | 0.08 |
| 859 | D4294 | 1.067 | | 0.00 | 1849 | ISO8754 | 1.05 | | -0.49 |
| 862 | D2622 | 1.099 | | 0.90 | 1857 | ISO8754 | 1.04 | | -0.77 |
| 863 | D4294 | 1.042 | | -0.71 | 1862 | D4294 | 1.06 | | -0.20 |
| 864 | D4294 | 1.052 | | -0.43 | 1881 | D4294 | 1.045 | | -0.63 |
| 865 | ISO8754 | 1.077 | | 0.28 | 1906 | D5623 | 1.042 | | -0.71 |
| 866 | D4294 | 1.047 | | -0.57 | 1936 | ISO8754 | 1.07 | | 0.08 |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|---------|-------|------|---------|------|---------|--------|------|---------|
| 1937 | ISO8754 | 1.035 | | -0.91 | 6024 | ISO8754 | 1.081 | | 0.39 |
| 1938 | ISO8754 | 1.087 | | 0.56 | 6026 | D4294 | 1.064 | | -0.09 |
| 1943 | | 1.071 | | 0.11 | 6028 | ISO8754 | 1.046 | | -0.60 |
| 1956 | ISO8754 | 1.065 | | -0.06 | 6039 | ISO8754 | 1.08 | | 0.36 |
| 1962 | ISO8754 | 1.012 | | -1.56 | 6049 | D4294 | 1.053 | | -0.40 |
| 1964 | | ---- | | ---- | 6051 | D4294 | 1.043 | | -0.68 |
| 1967 | D4294 | 1.053 | | -0.40 | 6057 | ISO8754 | 1.068 | | 0.02 |
| 1971 | ISO8754 | 1.068 | | 0.02 | 6075 | ISO8754 | 1.043 | | -0.68 |
| 1986 | D4294 | 1.04 | | -0.77 | 6092 | D4294 | 1.09 | | 0.65 |
| 1995 | D4294 | 1.04 | | -0.77 | 6109 | D1552 | 1.1194 | | 1.48 |
| 6004 | D4294 | 1.09 | | 0.65 | 6112 | | ---- | | ---- |
| 6016 | D4294 | 1.131 | C | 1.81 | 6114 | D4294 | 1.065 | | -0.06 |
| 6021 | ISO8754 | 1.065 | | -0.06 | 6122 | ISO8754 | 1.09 | | 0.65 |

normality OK
n 154
outliers 2
mean (n) 1.0671
st.dev. (n) 0.03006
R(calc.) 0.0842
R(ISO8754:03) 0.0988
Compare R(D4294:16e1) 0.0758

Lab 6016 first reported: 0.11215



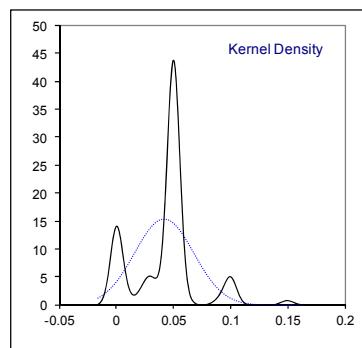
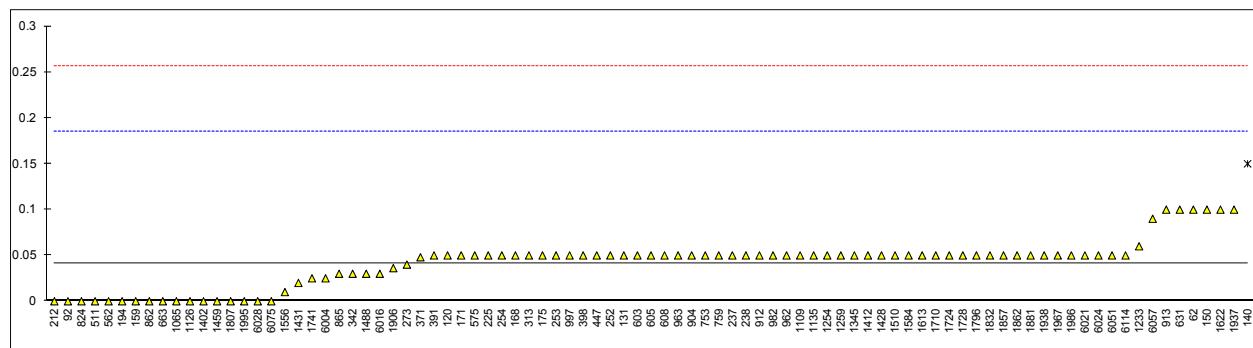
Determination of Water by distillation on sample #17105; results in %V/V

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|---------|-------|---------|---------|------|----------|----------|------|---------|
| 62 | D95 | 0.1 | | 0.82 | 870 | ISO3733 | <0.05 | | ---- |
| 90 | D95 | < 0.1 | | ---- | 886 | | ---- | | ---- |
| 92 | D95 | 0 | | -0.58 | 902 | ISO3733 | <0,1 | | ---- |
| 120 | D95 | 0.05 | | 0.12 | 904 | D95 | 0.05 | | 0.12 |
| 131 | D95 | 0.05 | | 0.12 | 912 | D95 | 0.05 | | 0.12 |
| 140 | D95 | 0.15 | R(0.01) | 1.52 | 913 | D95 | 0.1 | | 0.82 |
| 150 | D95 | 0.10 | | 0.82 | 922 | D95 | <0.05 | | ---- |
| 158 | | ---- | | ---- | 962 | ISO3733 | 0.05 | | 0.12 |
| 159 | D95 | 0.0 | | -0.58 | 963 | ISO3733 | 0.05 | | 0.12 |
| 168 | D95 | 0.05 | | 0.12 | 971 | D95 | <0.05 | | ---- |
| 169 | | ---- | | ---- | 974 | D95 | <0.05 | | ---- |
| 171 | D95 | 0.05 | | 0.12 | 982 | D95 | 0.05 | | 0.12 |
| 175 | D95 | 0.05 | | 0.12 | 997 | D95 | 0.05 | | 0.12 |
| 194 | D95 | 0 | | -0.58 | 1006 | D95 | <0.05 | | ---- |
| 212 | ISO3733 | 0.0 | | -0.58 | 1011 | ISO3733 | < 0.10 | | ---- |
| 221 | | ---- | | ---- | 1059 | ISO3733 | <0,05 | | ---- |
| 224 | | ---- | | ---- | 1065 | D95 | 0.00 | | -0.58 |
| 225 | D95 | 0.05 | | 0.12 | 1082 | | ---- | | ---- |
| 237 | D95 | 0.05 | | 0.12 | 1095 | D95 | <0.1 | | ---- |
| 238 | D95 | 0.05 | | 0.12 | 1099 | ISO9029 | <0.05 | | ---- |
| 252 | D95 | 0.05 | | 0.12 | 1109 | D95 | 0.05 | | 0.12 |
| 253 | D95 | 0.05 | | 0.12 | 1126 | D95 | 0.00 | | -0.58 |
| 254 | D95 | 0.05 | | 0.12 | 1134 | D95 | <0.05 | | ---- |
| 273 | D95 | 0.04 | C | -0.02 | 1135 | ISO3733 | 0.05 | | 0.12 |
| 311 | | ---- | | ---- | 1161 | | ---- | | ---- |
| 313 | D95 | 0.05 | | 0.12 | 1167 | EN1428 | <0.1 | | ---- |
| 323 | ISO3733 | <0.05 | | ---- | 1177 | | ---- | | ---- |
| 331 | D95 | <0.05 | | ---- | 1191 | | ---- | | ---- |
| 333 | | ---- | | ---- | 1213 | D95 | <0.1 | | ---- |
| 334 | | ---- | | ---- | 1229 | | ---- | | ---- |
| 336 | | ---- | | ---- | 1233 | ISO3733 | 0.06 | | 0.26 |
| 337 | | ---- | | ---- | 1254 | D95 | 0.05 | | 0.12 |
| 342 | ISO3733 | 0.03 | | -0.16 | 1259 | ISO3733 | 0.05 | | 0.12 |
| 343 | D95 | <0,1 | | ---- | 1275 | IP74 | <0.10 | | ---- |
| 349 | D95 | <0,1 | | ---- | 1299 | D95 | <0.1 | | ---- |
| 351 | ISO3733 | <0,05 | | ---- | 1345 | D95 | 0.05 | | 0.12 |
| 371 | D95 | 0.048 | | 0.09 | 1356 | D6304-A | <0.05 | | ---- |
| 391 | ISO3733 | 0.05 | | 0.12 | 1367 | D95 | <0.05 | | ---- |
| 398 | ISO3733 | 0.05 | | 0.12 | 1389 | D95 | <0.1 | | ---- |
| 399 | | ---- | | ---- | 1402 | D95 | 0.00 | | -0.58 |
| 440 | | ---- | | ---- | 1404 | | ---- | | ---- |
| 444 | | ---- | | ---- | 1412 | D95 | 0.050 | | 0.12 |
| 445 | D95 | <0.05 | | ---- | 1428 | ISO3733 | 0.05 | | 0.12 |
| 447 | D95 | 0.05 | | 0.12 | 1431 | D95 | 0.02 | | -0.30 |
| 463 | ISO3733 | <0,1 | | ---- | 1459 | In house | 0 | | -0.58 |
| 511 | D95 | 0.0 | | -0.58 | 1488 | ISO3733 | 0.030 | | -0.16 |
| 541 | D95 | <0.05 | | ---- | 1510 | D95 | 0.05 | | 0.12 |
| 562 | D95 | 0.00 | | -0.58 | 1539 | D95 | <0,05 | | ---- |
| 575 | D95 | 0.05 | | 0.12 | 1556 | D6304-C | 0.01 | | -0.44 |
| 603 | D95 | 0.05 | | 0.12 | 1569 | D95 | <0.10 | | ---- |
| 604 | | ---- | | ---- | 1584 | ISO3733 | 0.05 | | 0.12 |
| 605 | D95 | 0.05 | | 0.12 | 1586 | D95 | < 0.05 | | ---- |
| 608 | D95 | 0.05 | | 0.12 | 1613 | D95 | 0.05 | | 0.12 |
| 621 | | ---- | | ---- | 1622 | D95 | 0.10 | | 0.82 |
| 631 | D95 | 0.10 | | 0.82 | 1631 | D95 | <0.1 | | ---- |
| 663 | D95 | 0.00 | | -0.58 | 1643 | D95 | <0.1 | | ---- |
| 671 | D95 | <0.1 | | ---- | 1710 | ISO9029 | 0.05 | | 0.12 |
| 750 | | ---- | | ---- | 1720 | | ---- | | ---- |
| 753 | D95 | 0.05 | | 0.12 | 1724 | D95 | 0.05 | | 0.12 |
| 759 | D95 | 0.05 | | 0.12 | 1728 | D95 | 0.05 | | 0.12 |
| 824 | ISO3733 | 0 | | -0.58 | 1740 | ISO3733 | <0.05 | | ---- |
| 825 | D95 | <0.05 | | ---- | 1741 | ISO3733 | 0.025 | | -0.23 |
| 851 | ISO3733 | <0.05 | | ---- | 1796 | ISO3733 | 0.05 | | 0.12 |
| 855 | ISO3733 | <0.05 | | ---- | 1807 | ISO3733 | 0 | | -0.58 |
| 857 | ISO3733 | <0.05 | | ---- | 1832 | ISO3733 | 0.05 | | 0.12 |
| 858 | D95 | <0.05 | | ---- | 1833 | ISO3733 | <0.1 | | ---- |
| 859 | D95 | <0.05 | | ---- | 1849 | EN1428 | < 0,1 | | ---- |
| 862 | D95 | 0 | | -0.58 | 1857 | ISO3733 | 0.05 | | 0.12 |
| 863 | D95 | <0.05 | | ---- | 1862 | D95 | 0.05 | | 0.12 |
| 864 | D95 | <0.05 | | ---- | 1881 | D95 | 0.05 | | 0.12 |
| 865 | ISO3733 | 0.03 | | -0.16 | 1906 | D6304-C | 0.036143 | | -0.08 |
| 866 | D95 | <0.05 | | ---- | 1936 | EN1428 | <0.1 | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|---------|-------|------|---------|------|---------|--------|------|---------|
| 1937 | EN1428 | 0.1 | | 0.82 | 6024 | ISO3733 | 0.05 | | 0.12 |
| 1938 | | 0.05 | | 0.12 | 6026 | | ----- | | ----- |
| 1943 | ISO3733 | <0.05 | | ----- | 6028 | D95 | 0 | | -0.58 |
| 1956 | | ----- | | ----- | 6039 | | ----- | | ----- |
| 1962 | D95 | <0.1 | | ----- | 6049 | ISO3733 | < 0.05 | | ----- |
| 1964 | | ----- | | ----- | 6051 | D95 | 0.05 | | 0.12 |
| 1967 | D95 | 0.05 | | 0.12 | 6057 | ISO3733 | 0.09 | | 0.68 |
| 1971 | | ----- | | ----- | 6075 | ISO3733 | 0.00 | | -0.58 |
| 1986 | D95 | 0.05 | | 0.12 | 6092 | D95 | <0.05 | | ----- |
| 1995 | D95 | 0 | | -0.58 | 6109 | | ----- | | ----- |
| 6004 | D95 | 0.025 | | -0.23 | 6112 | | ----- | | ----- |
| 6016 | D95 | 0.03 | | -0.16 | 6114 | D95 | 0.05 | | 0.12 |
| 6021 | ISO3733 | 0.05 | | 0.12 | 6122 | | ----- | | ----- |

normality OK
n 88
outliers 1
mean (n) 0.0418
st.dev. (n) 0.02601
R(calc.) 0.0728
R(ISO3733:99) 0.2
Compare R(D95:13e1) 0.2

Lab 273 first reported: 0.4



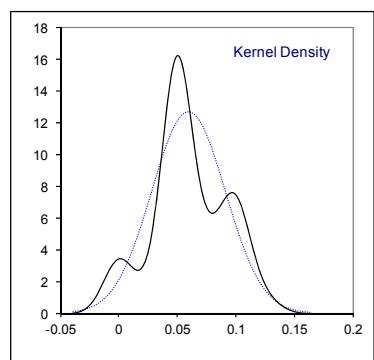
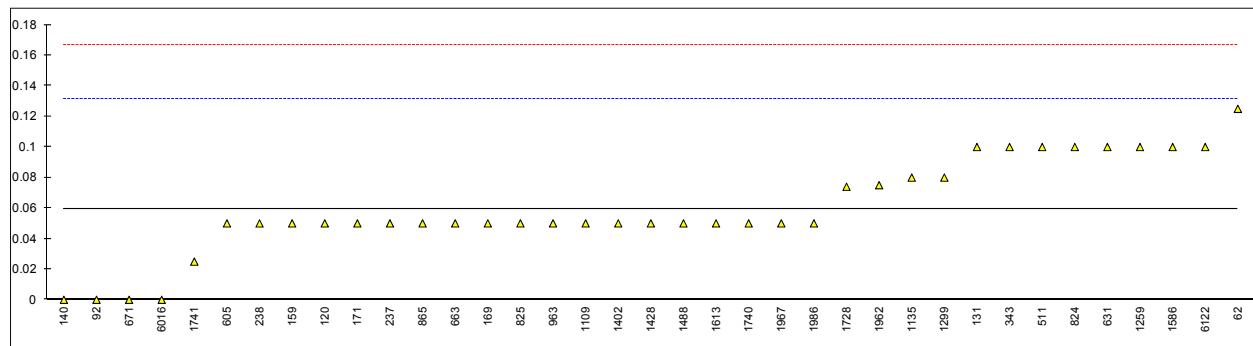
Determination of Water and Sediment on sample #17105; results in %V/V

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|-----|---------|-------|------|---------|------|---------|--------|------|---------|
| 62 | D1796 | 0.125 | | 1.83 | 870 | | ---- | | ---- |
| 90 | | ---- | | ---- | 886 | | ---- | | ---- |
| 92 | D1796 | 0 | | -1.67 | 902 | | ---- | | ---- |
| 120 | D1796 | 0.05 | | -0.27 | 904 | | ---- | | ---- |
| 131 | D1796 | 0.10 | | 1.13 | 912 | | ---- | | ---- |
| 140 | D1796 | 0.00 | | -1.67 | 913 | | ---- | | ---- |
| 150 | | ---- | | ---- | 922 | D1796 | <0.05 | | ---- |
| 158 | | ---- | | ---- | 962 | | ---- | | ---- |
| 159 | D1796 | 0.05 | | -0.27 | 963 | D1796 | 0.05 | | -0.27 |
| 168 | | ---- | | ---- | 971 | | ---- | | ---- |
| 169 | D1796 | 0.050 | | -0.27 | 974 | | ---- | | ---- |
| 171 | D1796 | 0.05 | | -0.27 | 982 | | ---- | | ---- |
| 175 | | ---- | | ---- | 997 | | ---- | | ---- |
| 194 | | ---- | | ---- | 1006 | | ---- | | ---- |
| 212 | | ---- | | ---- | 1011 | | ---- | | ---- |
| 221 | | ---- | | ---- | 1059 | D1796 | <0,05 | | ---- |
| 224 | | ---- | | ---- | 1065 | | ---- | | ---- |
| 225 | | ---- | | ---- | 1082 | | ---- | | ---- |
| 237 | D1796 | 0.05 | | -0.27 | 1095 | | ---- | | ---- |
| 238 | D1796 | 0.05 | | -0.27 | 1099 | | ---- | | ---- |
| 252 | | ---- | | ---- | 1109 | D1796 | 0.05 | | -0.27 |
| 253 | | ---- | | ---- | 1126 | | ---- | | ---- |
| 254 | | ---- | | ---- | 1134 | D1796 | <0.01 | | ---- |
| 273 | | ---- | | ---- | 1135 | D1796 | 0.08 | | 0.57 |
| 311 | | ---- | | ---- | 1161 | | ---- | | ---- |
| 313 | | ---- | | ---- | 1167 | | ---- | | ---- |
| 323 | D1796 | <0.05 | | ---- | 1177 | | ---- | | ---- |
| 331 | | ---- | | ---- | 1191 | | ---- | | ---- |
| 333 | | ---- | | ---- | 1213 | | ---- | | ---- |
| 334 | | ---- | | ---- | 1229 | | ---- | | ---- |
| 336 | | ---- | | ---- | 1233 | | ---- | | ---- |
| 337 | | ---- | | ---- | 1254 | | ---- | | ---- |
| 342 | | ---- | | ---- | 1259 | ISO3734 | 0.1 | C | 1.13 |
| 343 | D2068-C | 0.1 | 1.13 | | 1275 | | ---- | | ---- |
| 349 | | ---- | | ---- | 1299 | D1796 | 0.08 | | 0.57 |
| 351 | | ---- | | ---- | 1345 | | ---- | | ---- |
| 371 | | ---- | | ---- | 1356 | | ---- | | ---- |
| 391 | | ---- | | ---- | 1367 | | ---- | | ---- |
| 398 | | ---- | | ---- | 1389 | D1796 | <0.025 | | ---- |
| 399 | | ---- | | ---- | 1402 | D1796 | 0.05 | | -0.27 |
| 440 | | ---- | | ---- | 1404 | | ---- | | ---- |
| 444 | | ---- | | ---- | 1412 | | ---- | | ---- |
| 445 | | ---- | | ---- | 1428 | ISO3734 | 0.05 | | -0.27 |
| 447 | | ---- | | ---- | 1431 | | ---- | | ---- |
| 463 | | ---- | | ---- | 1459 | | ---- | | ---- |
| 511 | D1796 | 0.10 | 1.13 | | 1488 | D1796 | 0.050 | | -0.27 |
| 541 | | ---- | | ---- | 1510 | | ---- | | ---- |
| 562 | | ---- | | ---- | 1539 | | ---- | | ---- |
| 575 | | ---- | | ---- | 1556 | | ---- | | ---- |
| 603 | | ---- | | ---- | 1569 | | ---- | | ---- |
| 604 | | ---- | | ---- | 1584 | | ---- | | ---- |
| 605 | D1796 | 0.05 | | -0.27 | 1586 | ISO3734 | 0.1 | | 1.13 |
| 608 | | ---- | | ---- | 1613 | D1796 | 0.05 | | -0.27 |
| 621 | | ---- | | ---- | 1622 | | ---- | | ---- |
| 631 | D1796 | 0.10 | 1.13 | | 1631 | | ---- | | ---- |
| 663 | D1796 | 0.05 | | -0.27 | 1643 | | ---- | | ---- |
| 671 | D1796 | 0 | | -1.67 | 1710 | | ---- | | ---- |
| 750 | | ---- | | ---- | 1720 | | ---- | | ---- |
| 753 | | ---- | | ---- | 1724 | | ---- | | ---- |
| 759 | | ---- | | ---- | 1728 | D1796 | 0.074 | | 0.40 |
| 824 | D1796 | 0.10 | 1.13 | | 1740 | D1796 | 0.05 | | -0.27 |
| 825 | D1796 | 0.05 | | -0.27 | 1741 | ISO3734 | 0.025 | | -0.97 |
| 851 | | ---- | | ---- | 1796 | | ---- | | ---- |
| 855 | | ---- | | ---- | 1807 | | ---- | | ---- |
| 857 | | ---- | | ---- | 1832 | | ---- | | ---- |
| 858 | | ---- | | ---- | 1833 | | ---- | | ---- |
| 859 | | ---- | | ---- | 1849 | | ---- | | ---- |
| 862 | | ---- | | ---- | 1857 | | ---- | | ---- |
| 863 | | ---- | | ---- | 1862 | | ---- | | ---- |
| 864 | | ---- | | ---- | 1881 | | ---- | | ---- |
| 865 | D1796 | 0.05 | | -0.27 | 1906 | | ---- | | ---- |
| 866 | | ---- | | ---- | 1936 | | ---- | | ---- |

| lab | method | value | mark | z(targ) | lab | method | value | mark | z(targ) |
|------|--------|-------|------|---------|------|---------|-------|------|---------|
| 1937 | | ---- | | ---- | 6024 | | ---- | | ---- |
| 1938 | | ---- | | ---- | 6026 | | ---- | | ---- |
| 1943 | | ---- | | ---- | 6028 | | ---- | | ---- |
| 1956 | | ---- | | ---- | 6039 | | ---- | | ---- |
| 1962 | D1796 | 0.075 | | 0.43 | 6049 | | ---- | | ---- |
| 1964 | | ---- | | ---- | 6051 | | ---- | | ---- |
| 1967 | D1796 | 0.05 | | -0.27 | 6057 | | ---- | | ---- |
| 1971 | | ---- | | ---- | 6075 | | ---- | | ---- |
| 1986 | D1796 | 0.05 | | -0.27 | 6092 | | ---- | | ---- |
| 1995 | | ---- | | ---- | 6109 | | ---- | | ---- |
| 6004 | | ---- | | ---- | 6112 | | ---- | | ---- |
| 6016 | D4007 | 0 | | -1.67 | 6114 | | ---- | | ---- |
| 6021 | | ---- | | ---- | 6122 | ISO3734 | 0.10 | | 1.13 |

normality OK
n 37
outliers 0
mean (n) 0.0597
st.dev. (n) 0.03152
R(calc.) 0.0883
R(D1796:11) 0.1

Lab 1259 first reported: 0.2



Vacuum Distillation at 10mmHg acc. ASTM D1160 (reported as AET) on sample #17105, results in °C

| lab | method | IBP | 5% rec | 10% rec | 20% rec | 30% rec | 40% rec | 50% rec | FBP |
|-----|--------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|
| 62 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 90 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 92 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 120 | D1160 | 219.0 | 260.2 | 271.1 | 348.3 | 411.4 | 477.5 | 530.8 | 560.2 |
| 131 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 140 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 150 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 158 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 159 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 168 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 169 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 171 | D1160 | 252 | 274 | 312 | 379 | 439 | 501 | 551 | 571 |
| 175 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 194 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 212 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 221 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 224 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 225 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 237 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 238 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 252 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 253 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 254 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 273 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 311 | D1160 | 217 | 270 | 308 | 375 | 434 | 491 | ---- | 521 |
| 313 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 323 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 331 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 333 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 334 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 336 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 337 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 342 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 343 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 349 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 351 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 371 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 391 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 398 | D1160 | 170.6 | 251.7 | 281.8 | 352.4 | 406.7 | 452.9 | 494.9 | 495.0 |
| 399 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 440 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 444 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 445 | D1160 | 211.9 | 255.1 | 303.1 | 370.1 | 430.6 | 478.3 | ---- | 498.0 |
| 447 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 463 | D1160 | 207 | 254 | 287 | 362 | 423 | 481 | 537 | 543 |
| 511 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 541 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 562 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 575 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 603 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 604 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 605 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 608 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 621 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 631 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 663 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 671 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 750 | D1160 | 226 | 267 | 305 | 375 | 435 | ---- | ---- | ---- |
| 753 | D1160 | 191 | 259 | 298 | 366 | 428 | 482 | ---- | 505 |
| 759 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 824 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 825 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 851 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 855 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 857 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 858 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 859 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 862 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 863 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 864 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 865 | | 227.5 | 271.2 | 305.9 | 373.5 | 433.5 | 490.6 | 539.3 | ---- |
| 866 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 870 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 886 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 902 | D1160 | 213.1 | 264.7 | 303.0 | 372.5 | 432.9 | 486.6 | ---- | 519.8 |

| lab | method | IBP | 5% rec | 10% rec | 20% rec | 30% rec | 40% rec | 50% rec | FBP |
|------|--------|-------|------------|------------|---------|---------|---------|---------|------------|
| 904 | D1160 | 199.5 | 252.0 | 293.0 | 363.0 | 425.0 | 480.0 | --- | 522 |
| 912 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 913 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 922 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 962 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 963 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 971 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 974 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 982 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 997 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1006 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1011 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1059 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1065 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1082 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1095 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1099 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1109 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1126 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1134 | D1160 | 217 | 267 | 304 | 379 | 436 | 489 | 540 | 552 |
| 1135 | D1160 | 220 | 238 | 272 | 354 | 417 | 475 | 537 | 565 |
| 1161 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1167 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1177 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1191 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1213 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1229 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1233 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1254 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1259 | D1160 | 229.0 | 267.8 | 305.1 | 368.5 | 430.7 | 485.0 | 539.7 | ---- |
| 1275 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1299 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1345 | D1160 | 197.0 | 249.0 | 287.0 | 360.0 | 419.0 | 477.0 | 526.0 | ---- |
| 1356 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1367 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1389 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1402 | D1160 | 219.1 | 269.5 | 305.3 | 369.5 | 426.8 | 485.2 | ---- | 533.5 |
| 1404 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1412 | D1160 | 220.5 | 268.0 | 297.0 | 365.0 | 424.0 | 477.0 | 525.5 | ---- |
| 1428 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1431 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1459 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1488 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1510 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1539 | D1160 | 229 | 266 C | 304 C | 377 C | 430 C | 491 C | ---- | 513 |
| 1556 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1569 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1584 | D1160 | 216 | 257 | 295 | 368 | 428 | 480 | ---- | 521 |
| 1586 | | 223.8 | 265.9 | 303.0 | 371.5 | 429.0 | 486.7 | ---- | 510.9 |
| 1613 | | 236.7 | 264.5 | 303.1 | 373.8 | 434.6 | 487.0 | ---- | 509.0 |
| 1622 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1631 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1643 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1710 | D1160 | 217.4 | 269.4 | 303.3 | 372.0 | 432.8 | 484.4 | ---- | 517.9 |
| 1720 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1724 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1728 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1740 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1741 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1796 | D1160 | 214 | 261 | 300 | 368 | 429 | 481 | ---- | 522 |
| 1807 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1832 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1833 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1849 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1857 | D1160 | 214.8 | 257.3 | 295.1 | 366.4 | 426.2 | 473.6 | ---- | 509.7 |
| 1862 | | 219 | 254 | 283 | 364 | 426 | 478 | ---- | 525 |
| 1881 | | 213.9 | 261.2 | 297.9 | 369.4 | 429.9 | 482.8 | 531.5 | 535.9 |
| 1906 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1936 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1937 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1938 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1943 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1956 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1962 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1964 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1967 | D1160 | 218 | 265 | 289 | 363 | 425 | 476 | W | 515 |
| 1971 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 1986 | D1160 | 218 | 260 | 295 | 368 | 426 | 481 | ---- | ---- |

| lab | method | IBP | 5% rec | 10% rec | 20% rec | 30% rec | 40% rec | 50% rec | FBP |
|-------------|---------|--------|--------|---------|---------|---------|---------|---------|--------|
| 1995 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6004 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6016 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6021 | D1160 | 214 | 257 | 295 | 366 | 427 | 477 | --- | 514 |
| 6024 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6026 | D1160 | 205 | 257 | 291 | 360 | 420 | 476 | W | 512 |
| 6028 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6039 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6049 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6051 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6057 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6075 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6092 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6109 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 6112 | D1160 | 219.3 | 265.9 | 304.2 | 373.4 | 433.5 | 484.4 | --- | 517.7 |
| 6114 | D1160 | 212.0 | 267.8 | 309.2 | 382.7 | 441.7 | 494.9 | 538.6 | 543.2 |
| 6122 | | --- | --- | --- | --- | --- | --- | --- | --- |
| normality | suspect | OK | OK | OK | OK | OK | OK | OK | OK |
| n | | 30 | 30 | 29 | 31 | 31 | 30 | 11 | 23 |
| outliers | | 2 | 1+1ex | 2+1ex | 0+1ex | 1 | 1 | 1 | 2+1ex |
| mean (n) | | 216.18 | 262.58 | 299.35 | 368.50 | 428.54 | 483.00 | 536.04 | 522.64 |
| st.dev. (n) | | 9.578 | 6.366 | 7.286 | 7.333 | 6.423 | 6.458 | 7.293 | 15.403 |
| R(calc.) | | 26.82 | 17.82 | 20.40 | 20.53 | 17.99 | 18.08 | 20.42 | 43.13 |
| R(D1160:15) | | 49 | 22.13 | 20.70 | 19.96 | 19.00 | 18.52 | 18.41 | 27 |

The reported results underlined and bold are statistical outliers.

The reported results inderlined and italic are excluded (see §4.1)

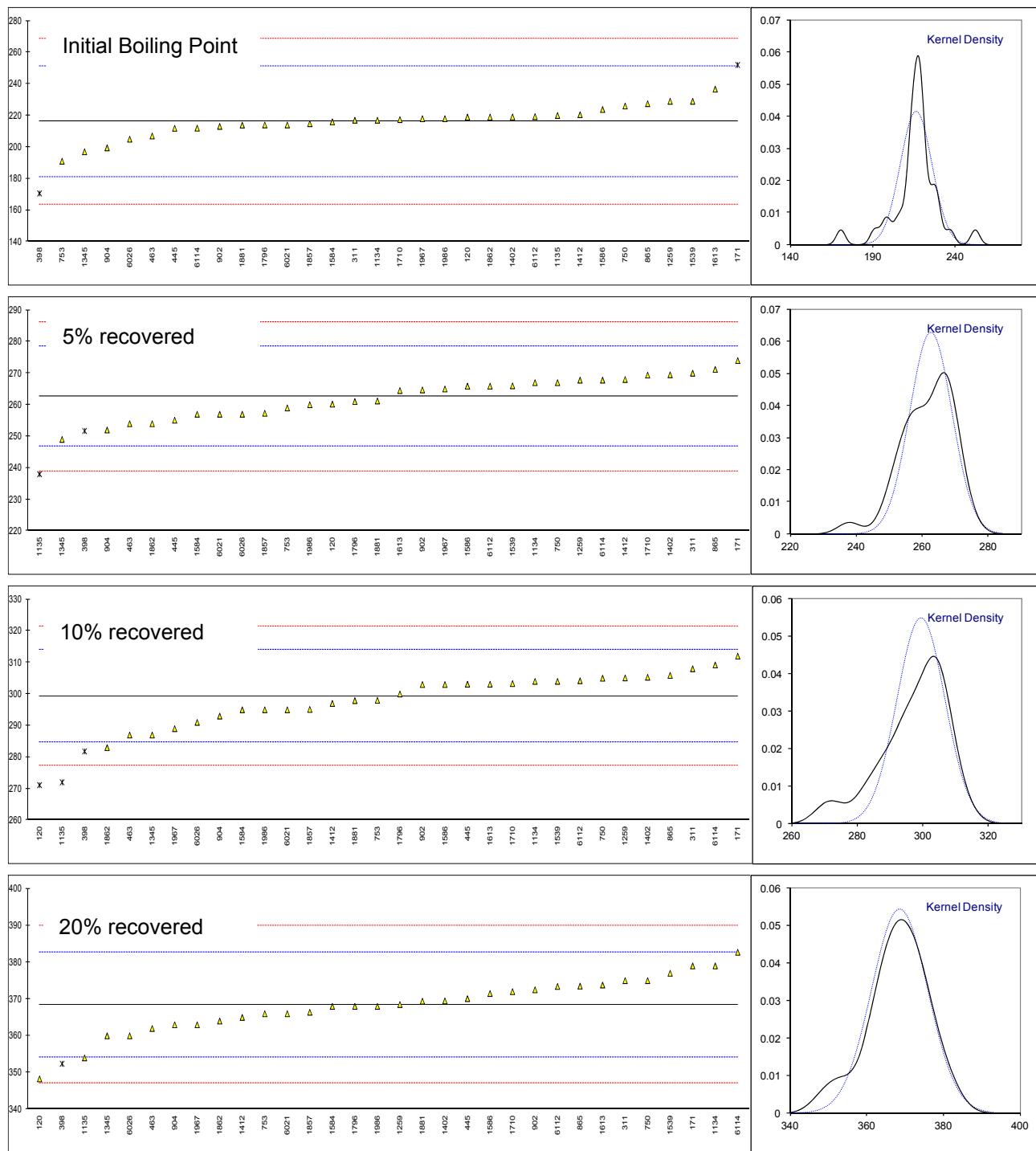
Lab 1539 first reported respectively; 292; 325; 390; 449; 508 for 5%; 10%; 20%; 30% and 40% recovered

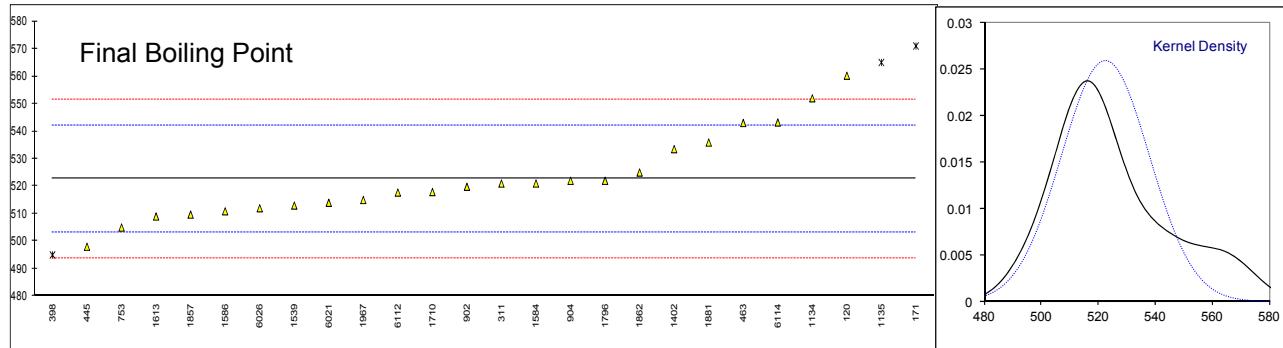
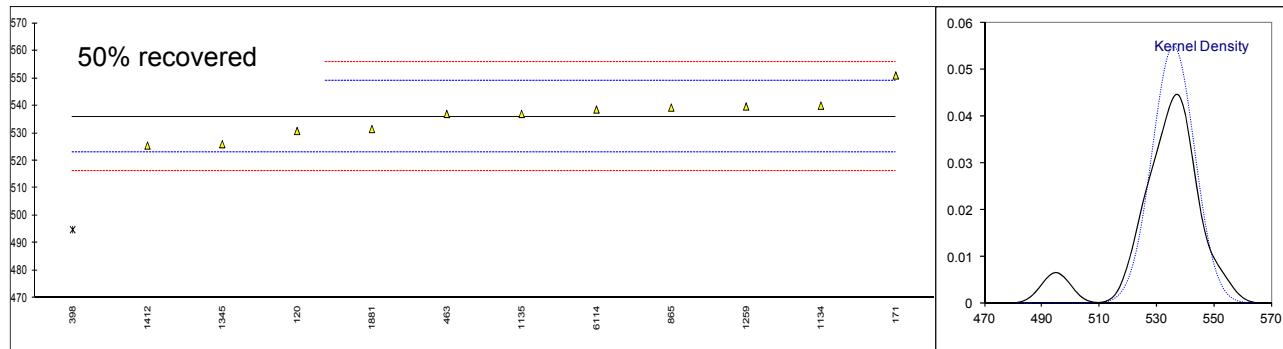
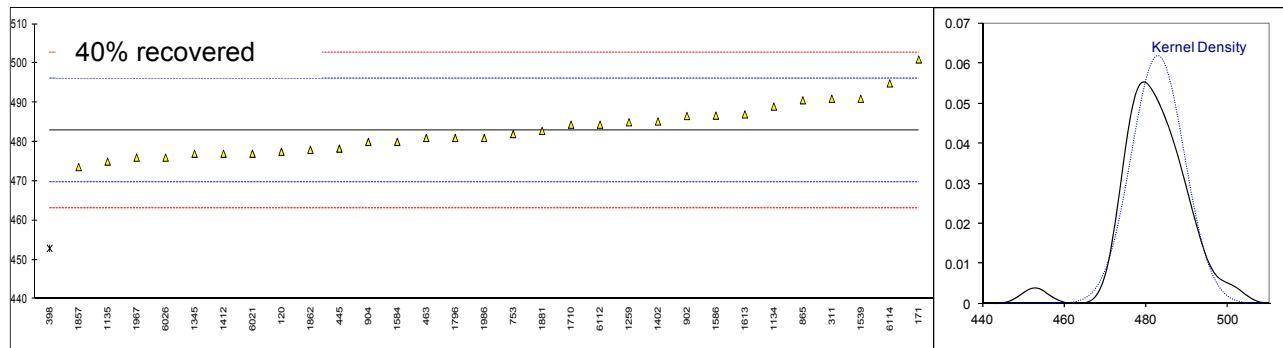
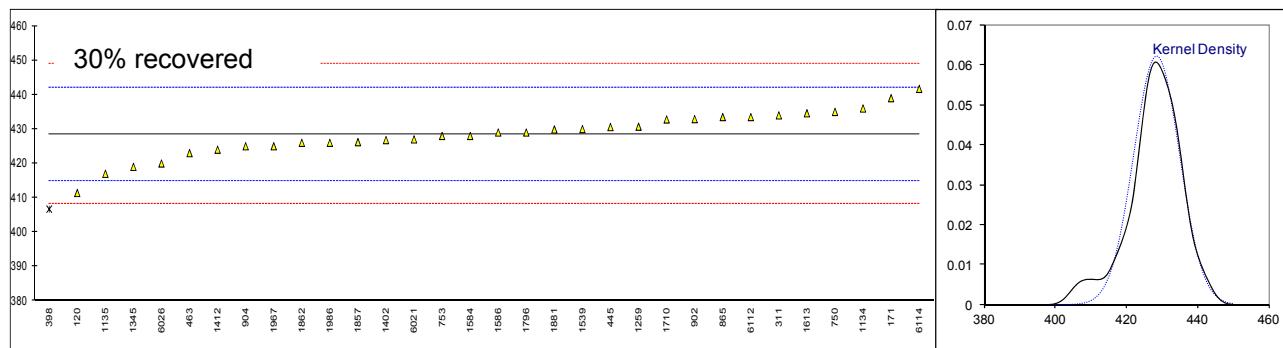
Lab 1796 reported: Final Boiling Point of Vacuum Distillation is 522 °C at 49 vol %.

Lab 1967 first reported: 508 at 50% recovered

Lab 6026 first reported: 512; distillation yield: 48%

Lab 6112 reported: recovery 46.7%





z-scores of Vacuum Distillation according to ASTM D1160 on sample #17105, results in °C

| lab | method | IBP | 5% rec | 10% rec | 20% rec | 30% rec | 40% rec | 50% rec | FBP |
|-----|--------|-------|--------|---------|---------|---------|---------|---------|-------|
| 62 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 90 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 92 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 120 | D1160 | 0.16 | -0.30 | -3.82 | -2.83 | -2.53 | -0.83 | -0.80 | 3.89 |
| 131 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 140 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 150 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 158 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 159 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 168 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 169 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 171 | D1160 | 2.05 | 1.44 | 1.71 | 1.47 | 1.54 | 2.72 | 2.28 | 5.01 |
| 175 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 194 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 212 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 221 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 224 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 225 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 237 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 238 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 252 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 253 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 254 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 273 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 311 | D1160 | 0.05 | 0.94 | 1.17 | 0.91 | 0.81 | 1.21 | ----- | -0.17 |
| 313 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 323 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 331 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 333 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 334 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 336 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 337 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 342 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 343 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 349 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 351 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 371 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 391 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 398 | D1160 | -2.60 | -1.38 | -2.37 | -2.26 | -3.22 | -4.55 | -6.25 | -2.87 |
| 399 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 440 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 444 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 445 | D1160 | -0.24 | -0.95 | 0.51 | 0.22 | 0.30 | -0.71 | ----- | -2.56 |
| 447 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 463 | D1160 | -0.52 | -1.09 | -1.67 | -0.91 | -0.82 | -0.30 | 0.15 | 2.11 |
| 511 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 541 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 562 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 575 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 603 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 604 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 605 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 608 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 621 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 631 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 663 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 671 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 750 | D1160 | 0.56 | 0.56 | 0.76 | 0.91 | 0.95 | ----- | ----- | ----- |
| 753 | D1160 | -1.44 | -0.45 | -0.18 | -0.35 | -0.08 | -0.15 | ----- | -1.83 |
| 759 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 824 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 825 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 851 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 855 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 857 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 858 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 859 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 862 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 863 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 864 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 865 | | 0.65 | 1.09 | 0.89 | 0.70 | 0.73 | 1.15 | 0.50 | ----- |
| 866 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 870 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 886 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 902 | D1160 | -0.18 | 0.27 | 0.49 | 0.56 | 0.64 | 0.54 | ----- | -0.29 |

| lab | method | IBP | 5% rec | 10% rec | 20% rec | 30% rec | 40% rec | 50% rec | FBP |
|------|--------|-------|--------|---------|---------|---------|---------|---------|-------|
| 904 | D1160 | -0.95 | -1.34 | -0.86 | -0.77 | -0.52 | -0.45 | --- | -0.07 |
| 912 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 913 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 922 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 962 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 963 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 971 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 974 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 982 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 997 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1006 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1011 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1059 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1065 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1082 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1095 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1099 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1109 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1126 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1134 | D1160 | 0.05 | 0.56 | 0.63 | 1.47 | 1.10 | 0.91 | 0.60 | 3.04 |
| 1135 | D1160 | 0.22 | -3.11 | -3.70 | -2.03 | -1.70 | -1.21 | 0.15 | 4.39 |
| 1161 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1167 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1177 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1191 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1213 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1229 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1233 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1254 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1259 | D1160 | 0.73 | 0.66 | 0.78 | 0.00 | 0.32 | 0.30 | 0.56 | --- |
| 1275 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1299 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1345 | D1160 | -1.10 | -1.72 | -1.67 | -1.19 | -1.41 | -0.91 | -1.53 | --- |
| 1356 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1367 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1389 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1402 | D1160 | 0.17 | 0.87 | 0.80 | 0.14 | -0.26 | 0.33 | --- | 1.13 |
| 1404 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1412 | D1160 | 0.25 | 0.69 | -0.32 | -0.49 | -0.67 | -0.91 | -1.60 | --- |
| 1428 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1431 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1459 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1488 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1510 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1539 | D1160 | 0.73 | 0.43 | 0.63 | 1.19 | 0.22 | 1.21 | --- | -1.00 |
| 1556 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1569 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1584 | D1160 | -0.01 | -0.71 | -0.59 | -0.07 | -0.08 | -0.45 | --- | -0.17 |
| 1586 | | 0.44 | 0.42 | 0.49 | 0.42 | 0.07 | 0.56 | --- | -1.22 |
| 1613 | | 1.17 | 0.24 | 0.51 | 0.74 | 0.89 | 0.60 | --- | -1.41 |
| 1622 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1631 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1643 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1710 | D1160 | 0.07 | 0.86 | 0.53 | 0.49 | 0.63 | 0.21 | --- | -0.49 |
| 1720 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1724 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1728 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1740 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1741 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1796 | D1160 | -0.12 | -0.20 | 0.09 | -0.07 | 0.07 | -0.30 | --- | -0.07 |
| 1807 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1832 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1833 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1849 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1857 | D1160 | -0.08 | -0.67 | -0.58 | -0.30 | -0.34 | -1.42 | --- | -1.34 |
| 1862 | | 0.16 | -1.09 | -2.21 | -0.63 | -0.37 | -0.76 | --- | 0.24 |
| 1881 | | -0.13 | -0.17 | -0.20 | 0.13 | 0.20 | -0.03 | -0.69 | 1.37 |
| 1906 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1936 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1937 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1938 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1943 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1956 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1962 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1964 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1967 | D1160 | 0.10 | 0.31 | -1.40 | -0.77 | -0.52 | -1.06 | --- | -0.79 |
| 1971 | | --- | --- | --- | --- | --- | --- | --- | --- |
| 1986 | D1160 | 0.10 | -0.33 | -0.59 | -0.07 | -0.37 | -0.30 | --- | --- |

| lab | method | IBP | 5% rec | 10% rec | 20% rec | 30% rec | 40% rec | 50% rec | FBP |
|------|--------|-------|--------|---------|---------|---------|---------|---------|-------|
| 1995 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6004 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6016 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6021 | D1160 | -0.12 | -0.71 | -0.59 | -0.35 | -0.23 | -0.91 | ---- | -0.90 |
| 6024 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6026 | D1160 | -0.64 | -0.71 | -1.13 | -1.19 | -1.26 | -1.06 | ---- | -1.10 |
| 6028 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6039 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6049 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6051 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6057 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6075 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6092 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6109 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6112 | D1160 | 0.18 | 0.42 | 0.66 | 0.69 | 0.73 | 0.21 | ---- | -0.51 |
| 6114 | D1160 | -0.24 | 0.66 | 1.33 | 1.99 | 1.94 | 1.80 | 0.39 | 2.13 |
| 6122 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |

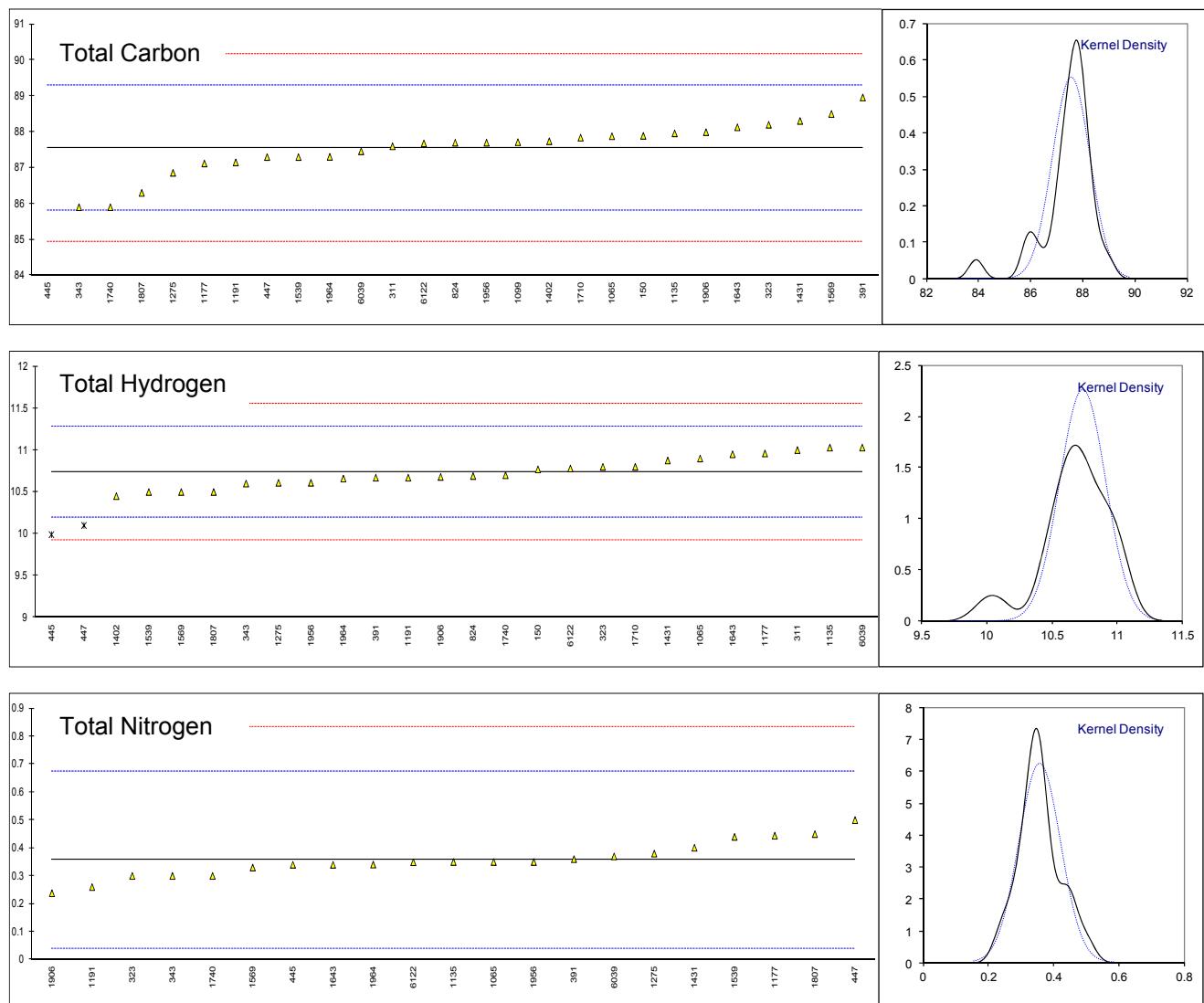
Determination of Total Carbon, Hydrogen and Nitrogen on sample #17105; results in %M/M

| Lab | method | Total C | mark | z(targ) | Total H | mark | z(targ) | Total N | mark | z(targ) |
|-----|-----------|---------|---------|---------|---------|---------|---------|---------|------|---------|
| 62 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 90 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 92 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 120 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 131 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 140 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 150 | D5291 - C | 87.89 | | 0.38 | 10.77 | | 0.11 | ---- | | ---- |
| 158 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 159 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 168 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 169 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 171 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 175 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 194 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 212 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 221 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 224 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 225 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 237 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 238 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 252 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 253 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 254 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 273 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 311 | | 87.6 | | 0.05 | 11.0 | | 0.96 | <0.75 | | ---- |
| 313 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 323 | D5291 - A | 88.2 | | 0.74 | 10.8 | | 0.23 | 0.3 | | -0.36 |
| 331 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 333 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 334 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 336 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 337 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 342 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 343 | D5291 - A | 85.9 | | -1.89 | 10.6 | | -0.51 | 0.3 | C | -0.36 |
| 349 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 351 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 371 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 391 | D5291 - A | 88.96 | | 1.61 | 10.67 | | -0.25 | 0.36 | | 0.02 |
| 398 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 399 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 440 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 444 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 445 | D5291 - C | 83.90 | R(0.01) | -4.18 | 9.99 | R(0.05) | -2.77 | 0.34 | | -0.11 |
| 447 | D5291 - B | 87.3 | | -0.29 | 10.1 | R(0.05) | -2.36 | 0.5 | | 0.90 |
| 463 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 511 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 541 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 562 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 575 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 603 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 604 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 605 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 608 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 621 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 631 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 663 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 671 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 750 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 753 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 759 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 824 | D5291 - D | 87.7 | | 0.17 | 10.69 | | -0.18 | ---- | | ---- |
| 825 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 851 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 855 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 857 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 858 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 859 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 862 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 863 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 864 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 865 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 866 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 870 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 886 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 902 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |

| Lab | method | Total C | mark | z(targ) | Total H | mark | z(targ) | Total N | mark | z(targ) |
|------|-----------|----------|------|---------|---------|------|---------|---------|--------|---------|
| 904 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 912 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 913 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 922 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 962 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 963 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 971 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 974 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 982 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 997 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1006 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1011 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1059 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1065 | D5291 - D | 87.88 | | 0.37 | 10.9 | | | 0.59 | 0.35 | -0.04 |
| 1082 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1095 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1099 | INH-77 | 87.71377 | | 0.18 | ---- | | ---- | ---- | | ---- |
| 1109 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1126 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1134 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1135 | D5291 - A | 87.96 | | 0.47 | 11.03 | | | 1.07 | 0.350 | -0.04 |
| 1161 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1167 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1177 | D5291 - D | 87.12 | | -0.50 | 10.96 | | | 0.82 | 0.444 | 0.55 |
| 1191 | | 87.15 | | -0.46 | 10.67 | | | -0.25 | 0.26 | -0.61 |
| 1213 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1229 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1233 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1254 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1259 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1275 | D5291 - D | 86.86 | | -0.79 | 10.61 | | | -0.48 | 0.38 | 0.15 |
| 1299 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1345 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1356 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1367 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1389 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1402 | D5291 - C | 87.74 | | 0.21 | 10.45 | | | -1.07 | ---- | ---- |
| 1404 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1412 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1428 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1431 | D5291 - C | 88.306 | | 0.86 | 10.876 | | | 0.51 | 0.401 | 0.28 |
| 1459 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1488 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1510 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1539 | D5291 - D | 87.30 | | -0.29 | 10.50 | | | -0.88 | 0.44 | 0.52 |
| 1556 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1569 | D5291 - A | 88.50 | | 1.08 | 10.50 | | | -0.88 | 0.33 | -0.17 |
| 1584 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1586 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1613 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1622 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1631 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1643 | D5291 - A | 88.13 | | 0.66 | 10.95 | | | 0.78 | 0.34 | -0.11 |
| 1710 | D5291 - B | 87.84 | | 0.33 | 10.80 | | | 0.23 | ---- | ---- |
| 1720 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1724 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1728 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1740 | D5291 - A | 85.9 | | -1.89 | 10.7 | | | -0.14 | 0.30 | -0.36 |
| 1741 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1796 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1807 | | 86.3 | | -1.43 | 10.5 | | | -0.88 | 0.45 | 0.59 |
| 1832 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1833 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1849 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1857 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1862 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1881 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1906 | | 87.992 | | 0.50 | 10.68 | | | -0.22 | 0.238 | -0.75 |
| 1936 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1937 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1938 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1943 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1956 | D5291 - C | 87.7 | | 0.17 | 10.61 | | | -0.48 | 0.35 | -0.04 |
| 1962 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1964 | | 87.305 | | -0.28 | 10.66 | | | -0.29 | 0.3407 | -0.10 |
| 1967 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1971 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1986 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |

| Lab | method | Total C | mark | z(targ) | Total H | mark | z(targ) | Total N | mark | z(targ) |
|-----------------|-----------|---------|------|---------|---------|------|---------|---------|-------|---------|
| 1995 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6004 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6016 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6021 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6024 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6026 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6028 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6039 | D5291 - C | 87.46 | | -0.11 | 11.03 | | | 1.07 | 0.37 | 0.08 |
| 6049 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6051 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6057 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6075 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6092 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6109 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6112 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6114 | | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6122 | D5291 - A | 87.68 | | 0.14 | 10.78 | | | 0.15 | 0.349 | -0.05 |
| normality | | OK | | | OK | | | OK | | |
| n | | 26 | | | 24 | | | 21 | | |
| outliers | | 1 | | | 2 | | | 0 | | |
| mean (n) | | 87.5533 | | | 10.7390 | | | 0.3568 | | |
| st.dev. (n) | | 0.72227 | | | 0.17647 | | | 0.06376 | | |
| R(calc.) | | 2.0223 | | | 0.4941 | | | 0.1785 | | |
| R(D5291-ABC:16) | | 2.4486 | | | 0.7583 | | | 0.4456 | | |

Lab 343 first reported: 0.2



Determination of Aluminium as Al, Silicon as Si and total Al+Si on sample #17106; results in mg/kg

| Lab | method | Al | mark | z(targ) | Si | mark | z(targ) | Sum Al+Si | mark | z(targ) |
|------|-----------|-------|---------|---------|--------|-----------|---------|-----------|-----------|---------|
| 62 | IP470 | 10 | | -0.49 | 12 | | 0.10 | 22 | | -0.16 |
| 90 | D5184 | 9.2 | | -1.07 | 7.3 | | -1.72 | 16.5 | | -2.04 |
| 92 | D5184 | 9.8 | | -0.64 | 6.4 | | -2.07 | 16.2 | | -2.14 |
| 120 | IP501 | 8.9 | | -1.29 | 13.6 | | 0.72 | 22.5 | | 0.01 |
| 131 | IP501 | 11.01 | C | 0.24 | 12.02 | | 0.11 | 23.03 | C | 0.19 |
| 140 | IP501 | 10.75 | | 0.05 | 12.39 | | 0.25 | 23.14 | | 0.23 |
| 150 | IP501 | 10.63 | | -0.03 | 10.86 | | -0.34 | 21.49 | | -0.33 |
| 158 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 159 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 168 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 171 | IP501 | 11 | | 0.23 | 12 | | 0.10 | 23 | | 0.18 |
| 175 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 194 | IP470 | 9.1 | | -1.14 | 16.8 | | 1.96 | 25.9 | | 1.17 |
| 212 | IP470 | 9 | C | -1.22 | 11 | | -0.28 | 20 | C | -0.84 |
| 221 | IP470 | 11.45 | | 0.56 | 13.74 | | 0.78 | 25.19 | | 0.93 |
| 237 | IP501 | 11.0 | C | 0.23 | 8.755 | | -1.15 | 19.755 | C | -0.93 |
| 254 | IP501 | 8.272 | | -1.75 | 6.947 | | -1.85 | 15.219 | | -2.48 |
| 273 | IP470 | 21 | R(0.01) | 7.50 | 26 | R(0.01) | 5.53 | ---- | | ---- |
| 311 | IP501 | 11 | | 0.23 | 12 | | 0.10 | 23 | | 0.18 |
| 323 | IP501 | 10 | | -0.49 | 10 | | -0.67 | 20 | | -0.84 |
| 331 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 333 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 334 | IP501 | 10 | | -0.49 | 13 | | 0.49 | 23 | | 0.18 |
| 336 | IP470 | 10 | | -0.49 | 12 | | 0.10 | 22 | | -0.16 |
| 342 | IP501 | 10.8 | | 0.09 | 12.1 | | 0.14 | 22.9 | | 0.15 |
| 343 | IP501 | 9 | | -1.22 | 11 | | -0.28 | 20 | | -0.84 |
| 351 | IP501 | 9.68 | | -0.72 | 10.41 | | -0.51 | 20.09 | | -0.81 |
| 357 | IP501 | 9.6 | | -0.78 | 5.0 | | -2.61 | 14.6 | | -2.69 |
| 371 | IP470 | 9.2 | | -1.07 | 9.8 | | -0.75 | 19 | | -1.18 |
| 391 | IP501 | 11 | | 0.23 | 12 | | 0.10 | 23 | | 0.18 |
| 398 | IP501 | 10 | | -0.49 | 11 | | -0.28 | 21 | | -0.50 |
| 399 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 444 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 445 | IP501 | 11.9 | | 0.89 | 13.8 | | 0.80 | 25.7 | | 1.11 |
| 447 | IP470 | 11.7 | | 0.74 | ---- | | ---- | ---- | | ---- |
| 463 | IP470 | 31.6 | R(0.01) | 15.19 | 37.1 | C,R(0.01) | 9.83 | 68.7 | C,R(0.01) | 15.80 |
| 511 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 541 | IP470 | 10 | | -0.49 | 12 | | 0.10 | 22 | | -0.16 |
| 605 | IP501 | 10 | | -0.49 | 9 | | -1.06 | 19 | | -1.18 |
| 608 | IP501 | 13.5 | | 2.05 | ---- | | ---- | ---- | | ---- |
| 621 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 631 | IP470 | 10.6 | | -0.06 | 11.4 | | -0.13 | 22.0 | | -0.16 |
| 663 | IP501 | 9.5 | | -0.85 | 10.3 | | -0.56 | 19.8 | | -0.91 |
| 750 | IP501 | 11 | | 0.23 | 11 | | -0.28 | 22 | | -0.16 |
| 824 | IP501 | 11 | | 0.23 | 13 | | 0.49 | 24 | | 0.52 |
| 851 | IP501 | 12.58 | | 1.38 | 13.13 | | 0.54 | 25.71 | | 1.11 |
| 855 | IP501 | 11.9 | | 0.89 | 13.1 | | 0.53 | 25.0 | | 0.87 |
| 862 | IP501 | 12.5 | | 1.32 | 13.8 | | 0.80 | 26.3 | | 1.31 |
| 863 | IP501 | 10.9 | | 0.16 | 12.4 | | 0.26 | 23.3 | | 0.29 |
| 864 | IP501 | 11.2 | | 0.38 | 12.8 | | 0.41 | 24.0 | | 0.52 |
| 865 | IP501 | 11.9 | | 0.89 | 13.5 | | 0.68 | 25.4 | | 1.00 |
| 902 | IP470 | <5 | f-? | <-4.12 | <10 | | ---- | <15 | | ---- |
| 904 | IP470 | <5 | f-? | <-4.12 | <10 | | ---- | <15 | | ---- |
| 912 | IP501 | 8.597 | | -1.51 | 9.595 | | -0.83 | 18.192 | | -1.46 |
| 913 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 922 | IP470 | 11.0 | | 0.23 | 10.9 | | -0.32 | 21.9 | | -0.19 |
| 963 | IP501 | 9.8 | | -0.64 | 11.8 | | 0.03 | 21.6 | | -0.30 |
| 971 | IP501 | 11 | | 0.23 | 12 | | 0.10 | 23 | | 0.18 |
| 1011 | ISO10478 | 11 | | 0.23 | 10 | | -0.67 | 21 | | -0.50 |
| 1059 | In house | 12 | | 0.96 | 13 | | 0.49 | ---- | | ---- |
| 1080 | D5185mod. | 3.7 | R(0.01) | -5.07 | 9.5 | | -0.87 | 13.2 | ex | -3.17 |
| 1082 | ISO10478 | 13.9 | | 2.34 | 8.54 | | -1.24 | 22.4 | | -0.02 |
| 1109 | IP470 | 15.0 | | 3.14 | 16.6 | | 1.89 | 31.6 | | 3.12 |
| 1126 | IP501 | 10.2 | | -0.35 | 11.8 | | 0.03 | ---- | | ---- |
| 1134 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1135 | IP501 | 9.658 | | -0.74 | 12.059 | | 0.13 | 21.717 | | -0.26 |
| 1191 | ISO10478 | 10.2 | | -0.35 | 14.8 | | 1.19 | 24.9 | | 0.83 |
| 1229 | ISO10478 | 10.56 | | -0.08 | 11.14 | | -0.23 | 21.7 | | -0.26 |
| 1233 | IP501 | 10 | | -0.49 | 12 | | 0.10 | 22 | | -0.16 |
| 1259 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1299 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1356 | IP501 | 10 | | -0.49 | 17 | | 2.04 | 27 | | 1.55 |
| 1367 | IP501 | 9 | | -1.22 | 13 | | 0.49 | 22 | | -0.16 |
| 1372 | IP470 | 12.89 | | 1.61 | 11.848 | | 0.04 | 24.738 | | 0.78 |
| 1389 | IP470 | 11 | | 0.23 | 11 | | -0.28 | 22 | | -0.16 |

| Lab | method | Al | mark | z(targ) | Si | mark | z(targ) | Sum Al+Si | mark | z(targ) |
|------|-----------|-------|---------|---------|--------|------|---------|-----------|---------|---------|
| 1402 | IP501 | 18 | R(0.01) | 5.32 | 17 | ex | 2.04 | 35 | R(0.01) | 4.28 |
| 1404 | IP470 | 8 | | -1.94 | 15 | | 1.27 | 23 | | 0.18 |
| 1412 | | ----- | | ----- | | | ----- | ----- | | ----- |
| 1431 | IP501mod. | 10.3 | | -0.27 | 13.3 | | 0.61 | 23.6 | | 0.39 |
| 1510 | IP501 | 13 | | 1.69 | 17 | | 2.04 | 30 | | 2.58 |
| 1556 | IP470 | 17.3 | R(0.01) | 4.81 | 14.7 | | 1.15 | 32.0 | ex | 3.26 |
| 1586 | IP470 | 12 | | 0.96 | 11 | | -0.28 | 23 | | 0.18 |
| 1613 | IP470 | 11.5 | | 0.60 | 12.0 | | 0.10 | 23.5 | | 0.35 |
| 1643 | | ----- | | ----- | | | ----- | ----- | | ----- |
| 1720 | D5708 | 9.24 | | -1.04 | ----- | | ----- | ----- | | ----- |
| 1724 | IP501 | 11.8 | | 0.82 | 13.7 | | 0.76 | 25.5 | | 1.04 |
| 1740 | IP501 | 12 | | 0.96 | 14 | | 0.88 | 26 | | 1.21 |
| 1741 | IP501 | 12.6 | | 1.40 | 12.4 | | 0.26 | 25.0 | | 0.87 |
| 1833 | IP501 | 11.67 | | 0.72 | 12.77 | | 0.40 | 24.44 | | 0.67 |
| 1857 | IP501 | 10.4 | | -0.20 | 11.05 | | -0.27 | 21.45 | | -0.35 |
| 1862 | IP501 | 10.8 | | 0.09 | 11.8 | | 0.03 | 22.6 | | 0.05 |
| 1881 | IP470 | 11.4 | | 0.53 | 12.6 | | 0.34 | 24.0 | | 0.52 |
| 1967 | IP470 | 9.695 | | -0.71 | 10.155 | | -0.61 | 19.850 | | -0.89 |
| 1995 | IP501 | 4.3 | R(0.01) | -4.63 | 5.00 | | -2.61 | 9.3 | R(0.01) | -4.50 |
| 6016 | | ----- | | ----- | | | ----- | ----- | | ----- |
| 6021 | IP501 | 9.6 | | -0.78 | 10.2 | | -0.59 | 19.8 | | -0.91 |
| 6028 | D5184 | 10.46 | ex | -0.16 | 10.06 | ex | -0.65 | 20.52 | ex | -0.67 |
| 6057 | IP501 | 10 | | -0.49 | 11 | | -0.28 | 21 | | -0.50 |
| 6075 | | ----- | | ----- | | | ----- | ----- | | ----- |
| 6092 | IP501 | 9 | | -1.22 | 11 | | -0.28 | ----- | | ----- |

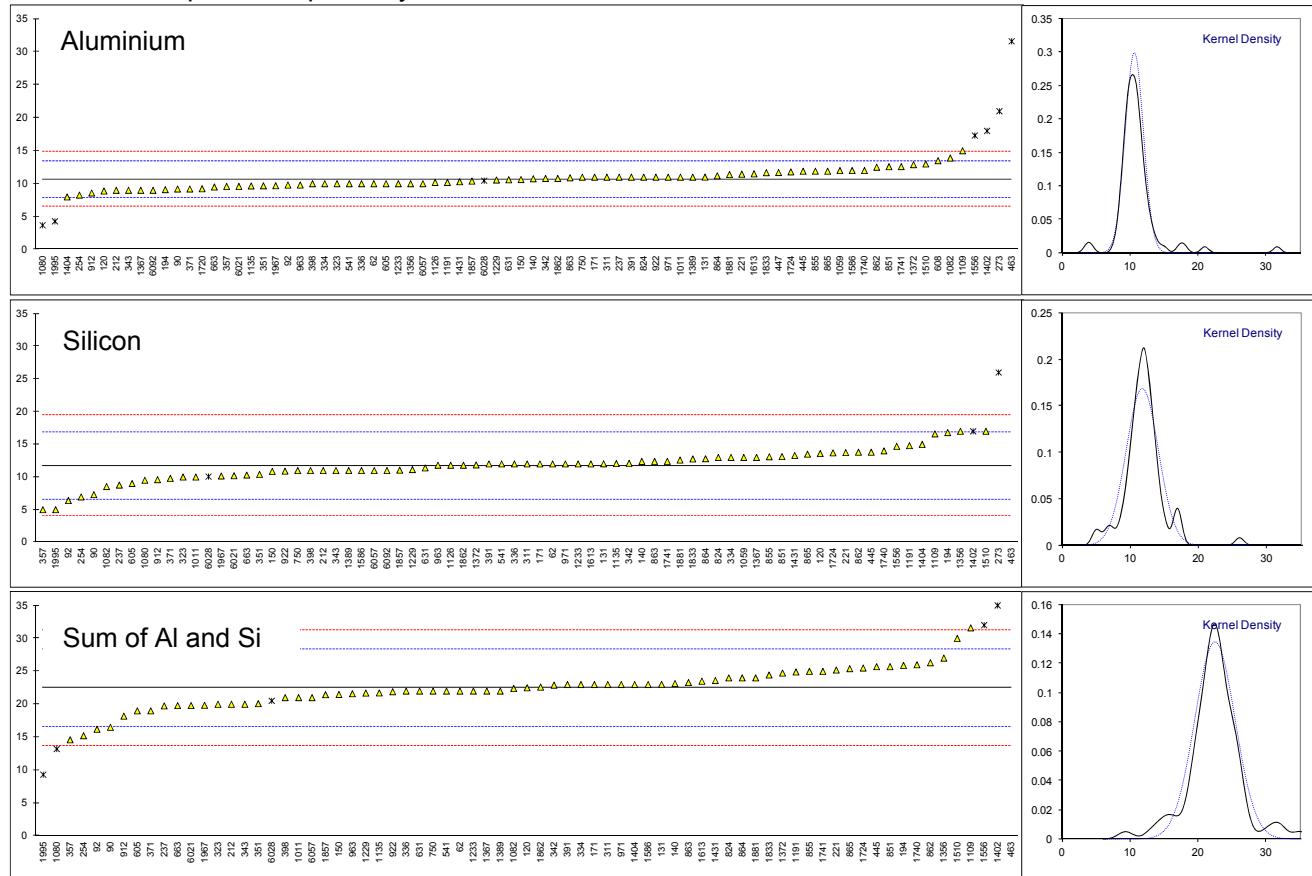
| | | | |
|---------------------|-------|---------|---------|
| normality | OK | suspect | suspect |
| n | 73 | 73 | 67 |
| outliers | 6+1ex | 2+2ex | 3+3ex |
| mean (n) | 10.68 | 11.73 | 22.47 |
| st.dev. (n) | 1.336 | 2.365 | 2.972 |
| R(calc.) | 3.74 | 6.62 | 8.32 |
| R(IP470:05) | 3.86 | 7.23 | 8.19 |
| Compare R(IP501:05) | 3.60 | 3.90 | 5.30 |

Lab 131 first reported respectively for Al and for Al+Si: 24.04; 36.06

Lab 212 first reported: 19 for Al and reported for Al+Si 30

Lab 237 first reported respectively for Al and for Al+Si: 24.2; 32.955

Lab 463 first reported respectively for Si and Al+Si: 42.9; 74.5



Determination of Iron as Fe, Nickel as Ni and Sodium as Na on sample #17106; results in mg/kg

| Lab | method | Fe | mark | z(targ) | Ni | mark | z(targ) | Na | mark | z(targ) |
|------|-----------|--------|---------|---------|--------|---------|---------|--------|---------|---------|
| 62 | IP470 | 25 | | 1.27 | 21 | | 0.66 | 10 | | -0.14 |
| 90 | D5863-B | ---- | | ---- | 26.4 | R(0.05) | 1.97 | 16 | R(0.05) | 3.04 |
| 92 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 120 | IP501 | 15.0 | | -1.20 | 13.2 | | -1.24 | 10.7 | | 0.23 |
| 131 | IP501 | 20.18 | | 0.08 | 18.64 | | 0.08 | 10.74 | | 0.25 |
| 140 | IP501 | 22.03 | | 0.53 | 20.05 | | 0.43 | 10.77 | | 0.26 |
| 150 | IP501 | 18.72 | | -0.28 | 16.78 | | -0.37 | 9.767 | | -0.27 |
| 158 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 159 | IP501 | 23 | | 0.77 | ---- | | ---- | 10 | | -0.14 |
| 168 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 171 | IP501 | 21 | | 0.28 | 19 | | 0.17 | 10 | | -0.14 |
| 175 | D5863-B | ---- | | ---- | 16 | | -0.56 | ---- | | ---- |
| 194 | IP470 | ---- | | ---- | ---- | | 8.7 | | | -0.83 |
| 212 | IP470 | 17 | | -0.71 | 18 | | -0.07 | 10 | | -0.14 |
| 221 | IP470 | ---- | | ---- | ---- | | ---- | 10.58 | | 0.16 |
| 237 | IP501 | 19.55 | | -0.08 | 17.6 | | -0.17 | 11.81 | | 0.82 |
| 254 | IP501 | 16.985 | | -0.71 | 15.672 | C | -0.64 | ---- | | ---- |
| 273 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 311 | IP501 | 22 | | 0.52 | 21 | | 0.66 | 11 | | 0.39 |
| 323 | IP501 | 20 | | 0.03 | 19 | | 0.17 | 10 | | -0.14 |
| 331 | IP501 | 17.0 | | -0.71 | 19.0 | | 0.17 | 10.5 | | 0.12 |
| 333 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 334 | IP501 | 19 | | -0.22 | 17 | | -0.31 | 12 | | 0.92 |
| 336 | IP470 | ---- | | ---- | 18 | | -0.07 | 10 | | -0.14 |
| 342 | IP501 | 21.3 | | 0.35 | 17.6 | | -0.17 | 9.3 | | -0.52 |
| 343 | D5708 | 18 | | -0.46 | 23 | | 1.14 | 13 | | 1.45 |
| 351 | IP501 | 17.13 | | -0.68 | 15.66 | | -0.64 | 10.21 | | -0.03 |
| 357 | IP501 | 22.6 | | 0.67 | 25.4 | R(0.05) | 1.72 | 9.9 | | -0.20 |
| 371 | IP470 | 17.3 | | -0.64 | 20.1 | | 0.44 | 9.8 | | -0.25 |
| 391 | IP501 | 21 | | 0.28 | 19 | | 0.17 | 10 | | -0.14 |
| 398 | IP501 | ---- | | ---- | 18 | | -0.07 | 11 | | 0.39 |
| 399 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 444 | IP501 | ---- | | ---- | ---- | | ---- | 13.2 | | 1.56 |
| 445 | IP501 | 19.5 | | -0.09 | 16.3 | | -0.48 | 11.8 | | 0.81 |
| 447 | IP470 | 49.1 | R(0.01) | 7.21 | 22.1 | | 0.92 | 17.6 | R(0.01) | 3.89 |
| 463 | IP470 | 19.4 | | -0.12 | 19.0 | | 0.17 | 10.9 | | 0.33 |
| 511 | D5863-A | 21.107 | | 0.30 | 34.853 | R(0.01) | 4.02 | ---- | | ---- |
| 541 | IP470 | 21 | | 0.28 | 18 | | -0.07 | 10 | | -0.14 |
| 605 | IP501 | 17 | | -0.71 | 17 | | -0.31 | 9 | | -0.68 |
| 608 | IP501 | 18.6 | | -0.31 | 16.9 | | -0.34 | ---- | | ---- |
| 621 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 631 | IP470 | 20.0 | | 0.03 | 17.9 | | -0.10 | 8.9 | | -0.73 |
| 663 | IP501 | 18.3 | | -0.39 | 16.1 | | -0.53 | 9.3 | | -0.52 |
| 750 | IP501 | 20 | | 0.03 | 17 | | -0.31 | 9 | | -0.68 |
| 824 | IP501 | 21 | | 0.28 | 21 | | 0.66 | 10 | | -0.14 |
| 851 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 855 | IP501 | 20.4 | | 0.13 | 17.4 | | -0.22 | 12.8 | | 1.34 |
| 862 | IP501 | 21.8 | | 0.48 | 16.7 | | -0.39 | 10.9 | | 0.33 |
| 863 | IP501 | 19.2 | | -0.17 | 16.8 | | -0.36 | 10.9 | | 0.33 |
| 864 | IP501 | 20.9 | | 0.25 | 18.1 | | -0.05 | 14.3 | | 2.14 |
| 865 | IP501 | 20.3 | | 0.11 | 18.5 | | 0.05 | 12.1 | | 0.97 |
| 902 | IP470 | 20 | | 0.03 | 18 | | -0.07 | 10 | | -0.14 |
| 904 | IP470 | 18 | | -0.46 | 18 | | -0.07 | 10 | | -0.14 |
| 912 | IP501 | 17.40 | | -0.61 | 14.805 | | -0.85 | 6.8995 | | -1.79 |
| 913 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 922 | IP470 | 29.4 | | 2.35 | 18.1 | | -0.05 | 8.9 | | -0.73 |
| 963 | IP501 | 19.7 | | -0.04 | 21.6 | | 0.80 | 9.9 | | -0.20 |
| 971 | IP501 | 21 | | 0.28 | 19 | | 0.17 | 9 | C | -0.68 |
| 1011 | D5863-B | ---- | | ---- | 16 | | -0.56 | 7.3 | | -1.58 |
| 1059 | In house | 17 | | -0.71 | 20 | | 0.41 | ---- | | ---- |
| 1080 | D5185mod. | 11 | | -2.19 | 25 | R(0.05) | 1.63 | 8.1 | | -1.15 |
| 1082 | INH-561B | 21.7 | | 0.45 | 18.9 | | 0.15 | 10.4 | | 0.07 |
| 1109 | IP470 | 21.2 | | 0.33 | 16.4 | | -0.46 | 10.8 | | 0.28 |
| 1126 | IP501 | 21.2 | | 0.33 | 18.2 | | -0.02 | 9.8 | | -0.25 |
| 1134 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1135 | IP501 | 19.838 | | -0.01 | 17.548 | | -0.18 | 7.859 | | -1.28 |
| 1191 | INH-22 | 18.5 | | -0.34 | 19.6 | | 0.32 | ---- | | ---- |
| 1229 | In house | 21.04 | | 0.29 | 19.15 | | 0.21 | 7.23 | | -1.62 |
| 1233 | IP501 | 19 | | -0.22 | 19 | | 0.17 | 10 | | -0.14 |
| 1259 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1299 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1356 | IP501 | 20 | | 0.03 | 30 | R(0.01) | 2.84 | 8 | | -1.21 |
| 1367 | IP501 | 19 | | -0.22 | 17 | | -0.31 | 12 | | 0.92 |
| 1372 | D5708 | 16.66 | | -0.79 | 18.11 | | -0.04 | 7.77 | | -1.33 |

| Lab | method | Fe | mark | z(targ) | Ni | mark | z(targ) | Na | mark | z(targ) |
|------|-------------|--------|---------|---------|--------|-----------|---------|-------|-----------|---------|
| 1389 | IP470 | 18 | | -0.46 | 18 | | -0.07 | 10 | | -0.14 |
| 1402 | IP501 | 23 | ex | 0.77 | 18 | ex | -0.07 | 11 | ex | 0.39 |
| 1404 | IP470 | 23 | | 0.77 | 22 | | 0.90 | 11 | | 0.39 |
| 1412 | IP501 | 21 | | 0.28 | 17 | | -0.31 | 11 | | 0.39 |
| 1431 | IP501mod. | 19.5 | | -0.09 | 16.7 | | -0.39 | 11.5 | | 0.65 |
| 1510 | IP501 | 19 | | -0.22 | 21 | | 0.66 | 11 | | 0.39 |
| 1556 | IP470 | ---- | | ---- | ---- | | ---- | 11.5 | | 0.65 |
| 1586 | IP470 | 21 | | 0.28 | 19 | | 0.17 | 10 | | -0.14 |
| 1613 | IP470 | 18.2 | | -0.41 | 20.8 | | 0.61 | 10.5 | | 0.12 |
| 1643 | D5185 | 5.18 | R(0.01) | -3.63 | 6.09 | R(0.01) | -2.96 | 3.28 | R(0.01) | -3.71 |
| 1720 | D5708 | 20.52 | | 0.16 | 20.32 | | 0.49 | 13.66 | | 1.80 |
| 1724 | IP501 | 21.2 | | 0.33 | 17.8 | | -0.12 | 9.47 | | -0.43 |
| 1740 | IP501 | 20 | | 0.03 | 18 | | -0.07 | 11 | | 0.39 |
| 1741 | IP501/IP470 | 20.2 | | 0.08 | 18.2 | | -0.02 | 9.6 | | -0.36 |
| 1833 | IP501 | 20.43 | | 0.14 | 18.49 | | 0.05 | 9.65 | | -0.33 |
| 1857 | IP501 | 20.7 | | 0.20 | 19.0 | | 0.17 | 10.2 | | -0.04 |
| 1862 | IP501 | 20.0 | | 0.03 | 18.3 | | 0.00 | 10.7 | | 0.23 |
| 1881 | IP470 | 27.0 | | 1.76 | 17.3 | | -0.24 | 10.3 | | 0.01 |
| 1967 | IP470 | 19.560 | | -0.08 | 19.700 | | 0.34 | 9.368 | | -0.48 |
| 1995 | IP501 | 15 | | -1.20 | 26.04 | R(0.05) | 1.88 | 13 | | 1.45 |
| 6016 | D5708 | 27.9 | | 1.98 | 19.0 | | 0.17 | 22.2 | C,R(0.01) | 6.34 |
| 6021 | IP501 | 19.5 | | -0.09 | 19.9 | | 0.39 | 9.1 | | -0.62 |
| 6028 | D5185 | 25.30 | ex | 1.34 | 33.82 | C,R(0.01) | 3.77 | 11.70 | ex | 0.76 |
| 6057 | IP501 | 20 | | 0.03 | 15 | | -0.80 | 11 | | 0.39 |
| 6075 | ---- | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 6092 | IP501 | 15 | | -1.20 | 8 | R(0.01) | -2.50 | 10 | | -0.14 |

normality

n

outliers

mean (n)

st.dev. (n)

R(calc.)

R(IP470:05)

Compare R(IP501:05)

OK

OK

72

75

9+1ex

4+2ex

18.29

10.27

1.811

1.428

5.07

4.00

11.54

5.27

8.32

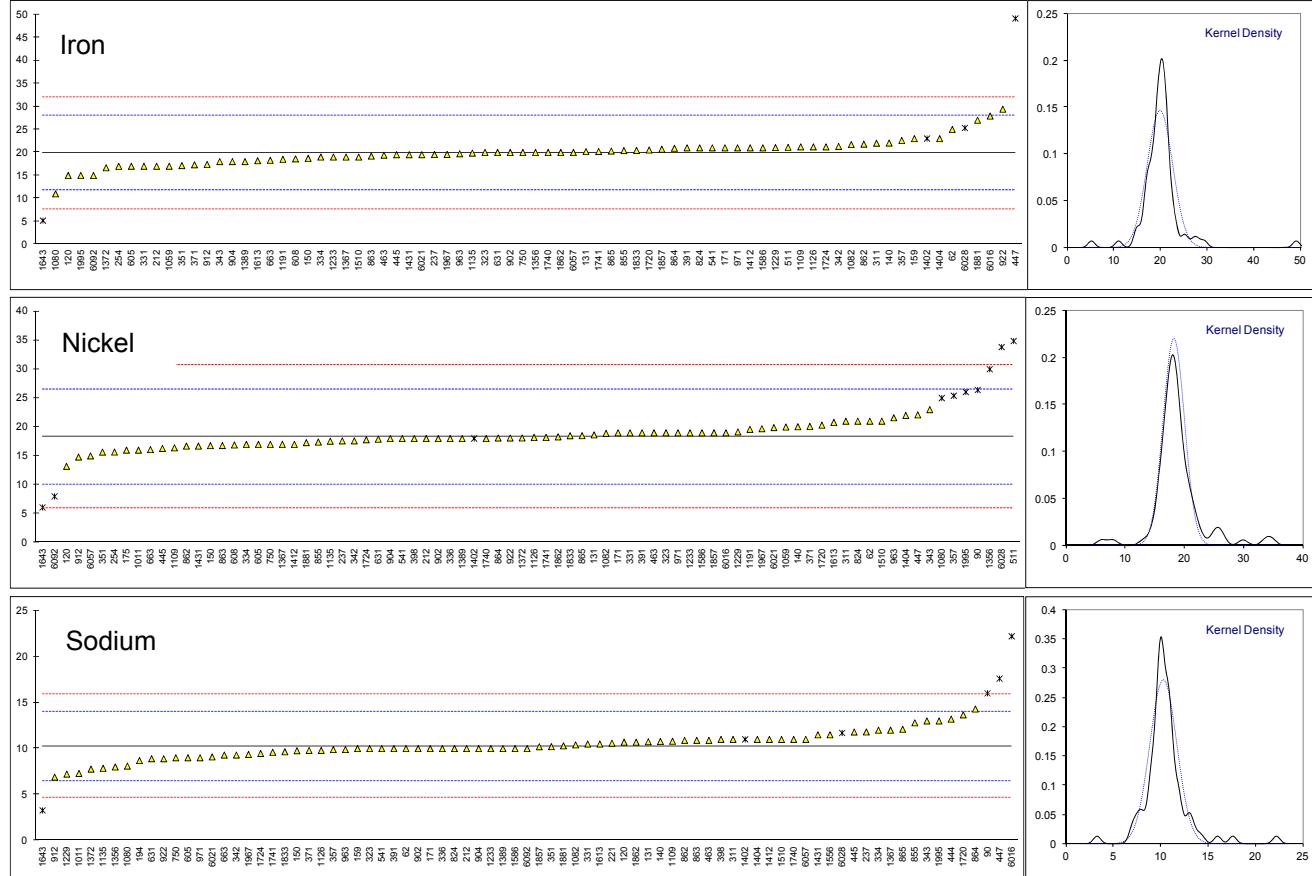
3.84

Lab 254 first reported: 7.972 for Ni

Lab 6016 first reported: 22.7 for Na

Lab 971 first reported: 19 for Na

Lab 6028 first reported: 36.6 for Ni



Determination of Vanadium as V, Calcium as Ca and Zinc as Zn on sample #17106; results in mg/kg

| Lab | method | V | mark | z(targ) | Ca | mark | z(targ) | Zn | mark | z(targ) |
|------|-----------|--------|-----------|---------|--------|---------|---------|--------|---------|---------|
| 62 | IP470 | 38 | | -0.21 | 28 | | 0.77 | 19 | C | 0.41 |
| 90 | D5863-B | 56 | R(0.05) | 2.25 | ---- | | ---- | ---- | | ---- |
| 92 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 120 | IP501 | 29.7 | | -1.34 | 20.8 | | -2.21 | 13.8 | | -2.43 |
| 131 | IP501 | 41.85 | | 0.32 | 24.04 | | -0.87 | ---- | | ---- |
| 140 | IP501 | 43.84 | | 0.59 | 28.19 | | 0.85 | 38.91 | R(0.01) | 11.30 |
| 150 | IP501 | 36.84 | | -0.36 | 23.04 | | -1.28 | 17.33 | | -0.50 |
| 158 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 159 | IP501 | 40 | | 0.07 | 27 | | 0.36 | 21 | | 1.50 |
| 168 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 171 | IP501 | 43 | | 0.48 | 24 | | -0.89 | 19 | | 0.41 |
| 175 | D5863-B | 44 | | 0.61 | ---- | | ---- | ---- | | ---- |
| 194 | IP470 | 40 | | 0.07 | 26.6 | | 0.19 | 17.7 | | -0.30 |
| 212 | IP470 | 59 | C,R(0.05) | 2.66 | 24 | | -0.89 | 18 | | -0.14 |
| 221 | IP470 | ---- | | ---- | ---- | | ---- | 10.74 | R(0.01) | -4.11 |
| 237 | IP501 | 41.68 | | 0.30 | 25.52 | | -0.26 | 19.7 | | 0.79 |
| 254 | IP501 | 36.692 | | -0.38 | ---- | | ---- | 16.030 | | -1.21 |
| 273 | IP470 | 33 | | -0.89 | ---- | | ---- | ---- | | ---- |
| 311 | IP501 | 43 | | 0.48 | 28 | | 0.77 | 20 | | 0.96 |
| 323 | IP501 | 41 | | 0.20 | 27 | | 0.36 | 19 | | 0.41 |
| 331 | IP501 | 39.0 | | -0.07 | 27.5 | | 0.56 | 20.0 | | 0.96 |
| 333 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 334 | IP501 | 38 | | -0.21 | 24 | | -0.89 | 18 | | -0.14 |
| 336 | IP470 | 36 | | -0.48 | 27 | | 0.36 | 22 | | 2.05 |
| 342 | IP501 | 37.7 | | -0.25 | 28.1 | | 0.81 | 18.2 | | -0.03 |
| 343 | D5708 | 51 | | 1.57 | 25 | | -0.47 | 17 | | -0.68 |
| 351 | IP501 | 35.80 | | -0.51 | 23.65 | | -1.03 | 16.75 | | -0.82 |
| 357 | IP501 | 40.6 | | 0.15 | 26.7 | | 0.23 | 21.7 | | 1.89 |
| 371 | IP470 | 34.6 | | -0.67 | 25.5 | C | -0.27 | 16.6 | | -0.90 |
| 391 | IP501 | 41 | | 0.20 | 30 | | 1.60 | 20 | | 0.96 |
| 398 | IP501 | ---- | | ---- | 28 | | 0.77 | 18 | | -0.14 |
| 399 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 444 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 445 | IP501 | 37.7 | | -0.25 | 26.1 | | -0.02 | 17.8 | | -0.25 |
| 447 | IP470 | 46.8 | | 1.00 | 25.7 | | -0.18 | 19.6 | | 0.74 |
| 463 | IP470 | 39.6 | | 0.01 | 26.4 | | 0.11 | 19.6 | | 0.74 |
| 511 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 541 | IP470 | 38 | | -0.21 | 26 | | -0.06 | 18 | | -0.14 |
| 605 | IP501 | 38 | | -0.21 | 23 | | -1.30 | 14 | | -2.32 |
| 608 | IP501 | 33.1 | | -0.88 | 27.3 | | 0.48 | ---- | | ---- |
| 621 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 631 | D5863-A | 31.6 | | -1.08 | ---- | | ---- | 24.9 | R(0.05) | 3.64 |
| 663 | IP501 | 37.5 | | -0.27 | 25.8 | | -0.14 | 18.3 | | 0.03 |
| 750 | IP501 | 40 | | 0.07 | 28 | | 0.77 | 18 | | -0.14 |
| 824 | IP501 | 44 | | 0.61 | 27 | | 0.36 | 20 | | 0.96 |
| 851 | IP501 | 36.37 | | -0.43 | 27.82 | | 0.69 | 17.49 | | -0.42 |
| 855 | IP501 | 35.7 | | -0.52 | 26.4 | | 0.11 | 16.4 | | -1.01 |
| 862 | IP501 | 37.5 | | -0.27 | 28.2 | | 0.85 | 19.2 | | 0.52 |
| 863 | IP501 | 35.0 | | -0.62 | 24.3 | | -0.76 | 17.2 | | -0.57 |
| 864 | IP501 | 36.6 | | -0.40 | 26.7 | | 0.23 | 16.3 | | -1.07 |
| 865 | IP501 | 37.2 | | -0.31 | 27.8 | | 0.69 | 18.8 | | 0.30 |
| 902 | IP470 | 36 | | -0.48 | 22 | | -1.71 | 18 | | -0.14 |
| 904 | IP470 | 38 | | -0.21 | 23 | | -1.30 | 18 | | -0.14 |
| 912 | IP501 | 29.48 | | -1.37 | 22.72 | | -1.42 | 15.04 | | -1.76 |
| 913 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 922 | IP470 | 41.2 | | 0.23 | 37.5 | R(0.01) | 4.70 | 19.5 | | 0.68 |
| 963 | IP501 | 36.6 | | -0.40 | 25.8 | | -0.14 | 15.5 | | -1.50 |
| 971 | IP501 | 39 | | -0.07 | 27 | | 0.36 | 19 | | 0.41 |
| 1011 | D5863-B | 45 | | 0.75 | ---- | | ---- | ---- | | ---- |
| 1059 | In house | 40 | | 0.07 | 31 | | 2.01 | 20 | | 0.96 |
| 1080 | D5185mod. | 55 | R(0.05) | 2.12 | 22 | | -1.71 | 18 | | -0.14 |
| 1082 | INH-561B | 39.2 | | -0.04 | 28.1 | | 0.81 | 20.0 | | 0.96 |
| 1109 | IP470 | 39.0 | | -0.07 | ---- | | ---- | ---- | | ---- |
| 1126 | IP501 | 41.6 | | 0.29 | 27.2 | | 0.44 | 20.9 | | 1.45 |
| 1134 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1135 | IP501 | 39.648 | | 0.02 | 28.132 | | 0.82 | 18.102 | | -0.08 |
| 1191 | INH-22 | 41.1 | | 0.22 | 29.2 | | 1.27 | ---- | | ---- |
| 1229 | In house | 47.24 | | 1.06 | 27.44 | | 0.54 | 20.61 | | 1.29 |
| 1233 | IP501 | 41 | | 0.20 | 26 | | -0.06 | 18 | | -0.14 |
| 1259 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1299 | | ---- | | ---- | ---- | | ---- | ---- | | ---- |
| 1356 | IP501 | 50 | | 1.43 | 23 | | -1.30 | 14 | | -2.32 |
| 1367 | IP501 | 38 | | -0.21 | 23 | | -1.30 | 17 | | -0.68 |
| 1372 | D5708 | 35.44 | | -0.56 | 23.2 | | -1.22 | 17.78 | | -0.26 |
| 1389 | IP470 | 34 | | -0.75 | ---- | W | ---- | ---- | W | ---- |

| Lab | method | V | mark | z(targ) | Ca | mark | z(targ) | Zn | mark | z(targ) |
|---------------------|-------------|--------|-----------|---------|-------------------------|-----------|-------------------------|--------|-----------|---------|
| 1402 | IP501 | 38 | ex | -0.21 | 10 | R(0.01) | -6.68 | 2 | R(0.01) | -8.88 |
| 1404 | IP470 | 35 | | -0.62 | 17 | R(0.01) | -3.78 | 19 | | 0.41 |
| 1412 | IP501 | 40 | | 0.07 | ---- | | ---- | 19 | | 0.41 |
| 1431 | IP501mod. | 39.5 | | 0.00 | 25.8 | | -0.14 | 16.8 | | -0.79 |
| 1510 | IP501 | 39 | | -0.07 | 27 | | 0.36 | 19 | | 0.41 |
| 1556 | IP470 | 47 | | 1.02 | 6.0 | R(0.01) | -8.33 | 1.9 | R(0.01) | -8.94 |
| 1586 | IP470 | 43 | | 0.48 | 28 | | 0.77 | 20 | | 0.96 |
| 1613 | D5863-A | 50 | | 1.43 | ---- | W | ---- | 17.0 | | -0.68 |
| 1643 | D5185 | 42.5 | | 0.41 | 10.0 | R(0.01) | -6.68 | ---- | ---- | ---- |
| 1720 | D5708 | 41.50 | | 0.27 | 28.92 | | 1.15 | ---- | ---- | ---- |
| 1724 | IP501 | 40.7 | | 0.16 | 28.2 | | 0.85 | 17.8 | | -0.25 |
| 1740 | IP501 | 39 | | -0.07 | 26 | | -0.06 | 18 | | -0.14 |
| 1741 | IP501/IP470 | 39.3 | | -0.03 | 26.7 | | 0.23 | 18.6 | | 0.19 |
| 1833 | IP501 | 39.57 | | 0.01 | 27.49 | | 0.56 | 18.71 | | 0.25 |
| 1857 | IP501 | 39.7 | | 0.03 | 27.7 | | 0.64 | 19.2 | | 0.52 |
| 1862 | IP501 | 39.4 | | -0.01 | 26.4 | | 0.11 | 18.2 | | -0.03 |
| 1881 | IP470 | 48.4 | | 1.22 | 27.0 | | 0.36 | 19.0 | | 0.41 |
| 1967 | IP470 | 41.410 | | 0.26 | 25.830 | | -0.13 | 18.465 | | 0.12 |
| 1995 | IP501 | 89.46 | R(0.01) | 6.83 | 24.96 | | -0.49 | 17.96 | | -0.16 |
| 6016 | D5708 | 41.2 | | 0.23 | ---- | | ---- | ---- | | ---- |
| 6021 | IP501 | 40.1 | | 0.08 | 25.8 | | -0.14 | 18.6 | | 0.19 |
| 6028 | D5185 | 64.39 | C,R(0.01) | 3.40 | 14.99 | C,R(0.01) | -4.61 | 41.91 | C,R(0.01) | 12.94 |
| 6057 | IP501 | 35 | | -0.62 | 25 | | -0.47 | 18 | | -0.14 |
| 6075 | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- | ---- |
| 6092 | IP501 | 37 | | -0.34 | 26 | | -0.06 | 17 | | -0.68 |
| normality | | OK | | OK | | OK | | OK | | OK |
| n | | 79 | | 69 | | 69 | | 69 | | 69 |
| outliers | | 5+1ex | | 6 | | 6 | | 6 | | 6 |
| mean (n) | | 39.50 | | 26.14 | Spike 19.4 (Rec < 135%) | 18.25 | Spike 16.9 (Rec < 108%) | | | |
| st.dev. (n) | | 4.217 | | 2.048 | | 1.652 | | | | |
| R(calc.) | | 11.81 | | 5.73 | | 4.62 | | | | |
| R(IP470:05) | | 20.49 | | 6.77 | | 5.12 | | | | |
| Compare R(IP501:05) | | 15.25 | | 5.37 | | 3.88 | | | | |

Lab 62 first reported: 10 for Zn

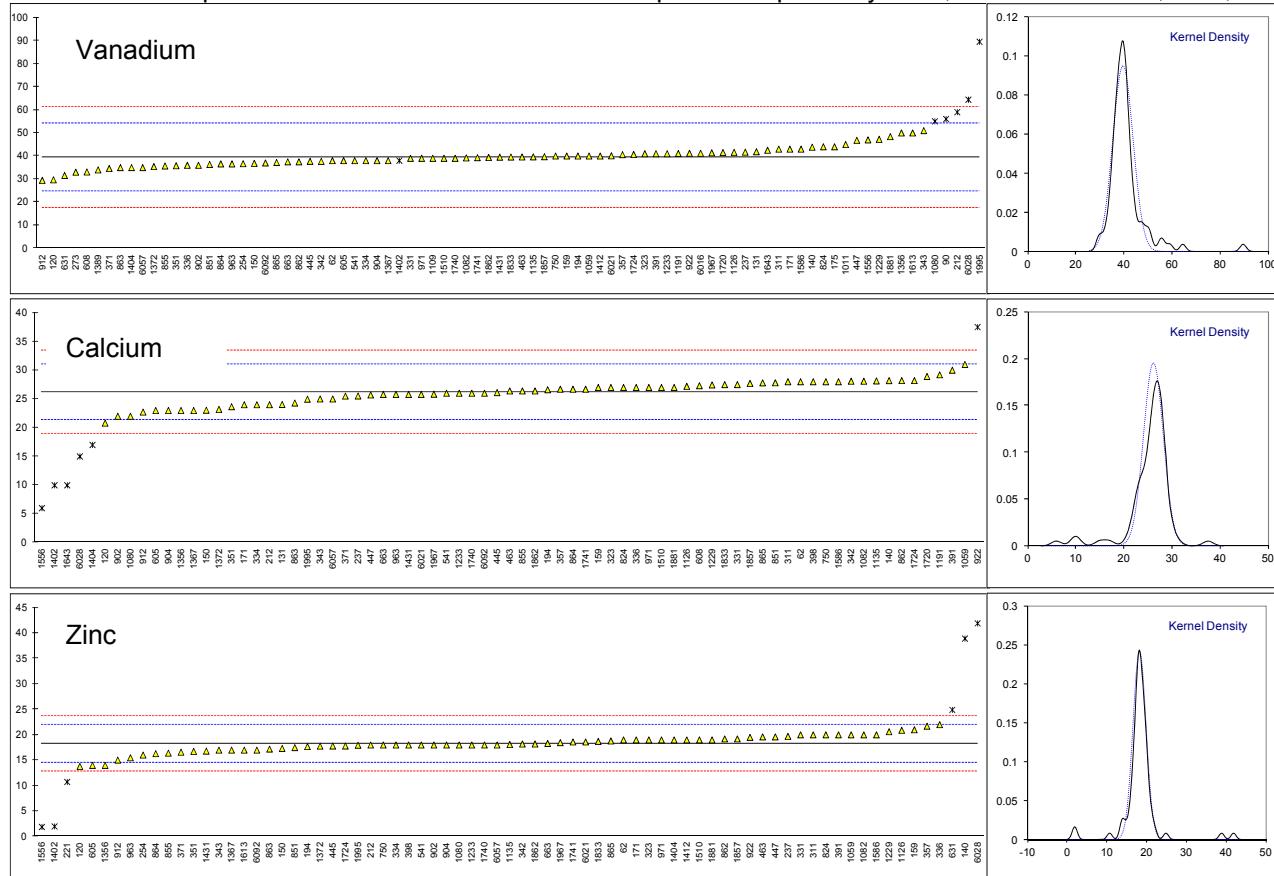
Lab 212 first reported: 24 for V

Lab 371 first reported: 14.5 for Ca

Lab 1389 first reported respectively for Ca and Zn: 10; 11

Lab 1613 first reported: 34.0 for Ca

Lab 6028 first reported respectively for V, Ca and Zn: :71.7; 3.88; 3.7



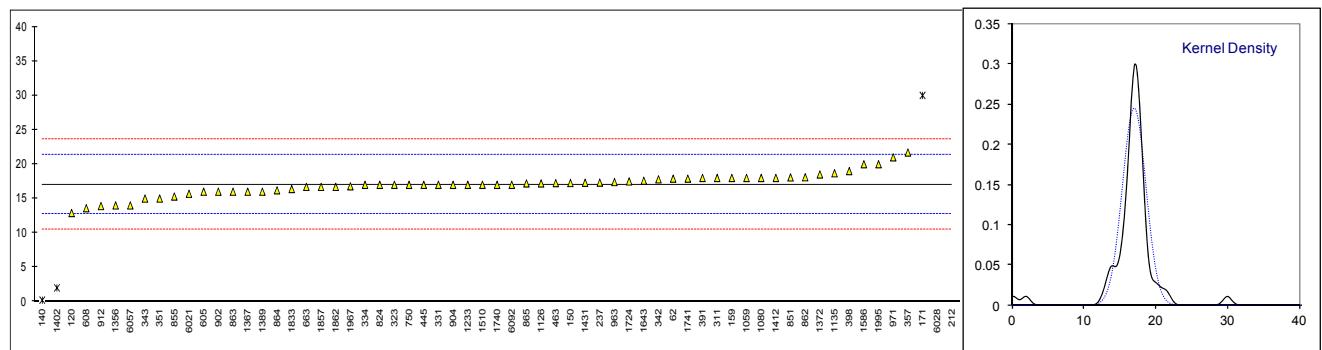
Determination of Phosphorus as P on sample #17106; results in mg/kg

| lab | method | value | mark | z(targ) | remarks |
|------|-----------|--------|-----------|---------|---------|
| 62 | IP500 | 17.9 | | 0.39 | |
| 90 | | ---- | | ---- | |
| 92 | | ---- | | ---- | |
| 120 | IP501 | 12.9 | | -1.91 | |
| 131 | | ---- | | ---- | |
| 140 | IP501 | 0.217 | R(0.01) | -7.76 | |
| 150 | IP501 | 17.26 | | 0.10 | |
| 158 | | ---- | | ---- | |
| 159 | IP501 | 18 | | 0.44 | |
| 168 | | ---- | | ---- | |
| 171 | IP501 | 30 | R(0.01) | 5.97 | |
| 175 | | ---- | | ---- | |
| 194 | | ---- | | ---- | |
| 212 | IP500 | 49 | C,R(0.01) | 14.73 | |
| 221 | | ---- | | ---- | |
| 237 | IP501 | 17.32 | | 0.13 | |
| 254 | | ---- | | ---- | |
| 273 | | ---- | | ---- | |
| 311 | IP501 | 18 | | 0.44 | |
| 323 | IP501 | 17 | | -0.02 | |
| 331 | IP501 | 17.0 | | -0.02 | |
| 333 | | ---- | | ---- | |
| 334 | IP501 | 17 | | -0.02 | |
| 336 | | ---- | | ---- | |
| 342 | IP501 | 17.8 | | 0.35 | |
| 343 | IP501 | 15 | | -0.94 | |
| 351 | IP501 | 15.01 | | -0.94 | |
| 357 | IP501 | 21.7 | | 2.15 | |
| 371 | | ---- | | ---- | |
| 391 | IP501 | 18 | | 0.44 | |
| 398 | IP501 | 19 | | 0.90 | |
| 399 | | ---- | | ---- | |
| 444 | | ---- | | ---- | |
| 445 | IP501 | 17.0 | | -0.02 | |
| 447 | | ---- | | ---- | |
| 463 | IP500 | 17.25 | | 0.09 | |
| 511 | | ---- | | ---- | |
| 541 | | ---- | | ---- | |
| 605 | IP501 | 16 | | -0.48 | |
| 608 | IP501 | 13.6 | | -1.59 | |
| 621 | | ---- | | ---- | |
| 631 | | ---- | | ---- | |
| 663 | IP501 | 16.7 | | -0.16 | |
| 750 | IP501 | 17 | | -0.02 | |
| 824 | IP501 | 17 | | -0.02 | |
| 851 | IP501 | 18.08 | | 0.48 | |
| 855 | IP501 | 15.3 | | -0.80 | |
| 862 | IP501 | 18.1 | | 0.49 | |
| 863 | IP501 | 16.0 | | -0.48 | |
| 864 | IP501 | 16.2 | | -0.39 | |
| 865 | IP501 | 17.2 | | 0.07 | |
| 902 | IP501 | 16 | | -0.48 | |
| 904 | IP500 | 17 | | -0.02 | |
| 912 | IP501 | 13.91 | | -1.45 | |
| 913 | | ---- | | ---- | |
| 922 | | ---- | | ---- | |
| 963 | IP501 | 17.4 | | 0.16 | |
| 971 | IP501 | 21 | | 1.82 | |
| 1011 | | ---- | | ---- | |
| 1059 | In house | 18 | | 0.44 | |
| 1080 | D5185mod. | 18 | | 0.44 | |
| 1082 | | ---- | | ---- | |
| 1109 | | ---- | | ---- | |
| 1126 | IP501 | 17.2 | | 0.07 | |
| 1134 | | ---- | | ---- | |
| 1135 | IP501 | 18.684 | | 0.76 | |
| 1191 | | ---- | | ---- | |
| 1229 | | ---- | | ---- | |
| 1233 | IP501 | 17 | | -0.02 | |
| 1259 | | ---- | | ---- | |
| 1299 | | ---- | | ---- | |
| 1356 | IP501 | 14 | | -1.40 | |
| 1367 | IP501 | 16 | | -0.48 | |
| 1372 | IP500 | 18.51 | | 0.68 | |
| 1389 | IP500 | 16 | | -0.48 | |

| lab | method | value | mark | z(targ) | remarks |
|---------------------|-----------|---------|-----------|---------|------------------------|
| 1402 | IP501 | 2 | R(0.01) | -6.94 | |
| 1404 | | ---- | | ---- | |
| 1412 | IP501 | 18 | | 0.44 | |
| 1431 | IP501mod. | 17.3 | | 0.12 | |
| 1510 | IP501 | 17 | | -0.02 | |
| 1556 | | ---- | | ---- | |
| 1586 | IP501 | 20 | | 1.36 | |
| 1613 | | ---- | | ---- | |
| 1643 | D5185 | 17.6 | | 0.26 | |
| 1720 | | ---- | | ---- | |
| 1724 | IP501 | 17.5 | | 0.21 | |
| 1740 | IP501 | 17 | | -0.02 | |
| 1741 | IP501 | 17.9 | | 0.39 | |
| 1833 | IP501 | 16.39 | | -0.30 | |
| 1857 | IP501 | 16.7 | | -0.16 | |
| 1862 | IP501 | 16.7 | | -0.16 | |
| 1881 | | ---- | | ---- | |
| 1967 | IP501 | 16.780 | | -0.12 | |
| 1995 | IP501 | 20 | | 1.36 | |
| 6016 | | ---- | | ---- | |
| 6021 | IP501 | 15.7 | | -0.62 | |
| 6028 | D5185 | 46.76 | C,R(0.01) | 13.70 | |
| 6057 | IP501 | 14 | | -1.40 | |
| 6075 | | ---- | | ---- | |
| 6092 | IP501 | 17 | | -0.02 | |
| | | | | | |
| normality | | | | | |
| n | | suspect | | | |
| outliers | | 5 | | | |
| mean (n) | | 17.04 | | | <u>Spike</u> |
| st.dev. (n) | | 1.631 | | | 14.6 (Recovery < 117%) |
| R(calc.) | | 4.57 | | | |
| R(IP501:05) | | 6.07 | | | |
| Compare R(IP500:03) | | 3.76 | | | |

Lab 212 first reported: 50

Lab 6028 first reported: 0.001



APPENDIX 2**Number of participants per country**

| Main round | Metals in Fuel Oil |
|-------------------------------------|-------------------------------------|
| 1 lab in ARGENTINA | 1 lab in ARGENTINA |
| 1 lab in AUSTRALIA | 1 lab in AUSTRALIA |
| 1 lab in AZERBAIJAN | 1 lab in AZERBAIJAN |
| 4 labs in BELGIUM | 2 labs in BELGIUM |
| 1 lab in BULGARIA | 3 labs in CANADA |
| 3 labs in CANADA | 5 labs in CHINA, People's Republic |
| 1 lab in CHILE | 1 lab in CROATIA |
| 10 labs in CHINA, People's Republic | 2 labs in EGYPT |
| 1 lab in COLOMBIA | 4 labs in FINLAND |
| 1 lab in COTE D'IVOIRE | 5 labs in FRANCE |
| 2 labs in CROATIA | 1 lab in GERMANY |
| 1 lab in CYPRUS | 2 labs in GREECE |
| 1 lab in DENMARK | 1 lab in HONG KONG |
| 1 lab in DJIBOUTI | 1 lab in HUNGARY |
| 1 lab in EGYPT | 2 labs in INDIA |
| 3 labs in FINLAND | 1 lab in INDONESIA |
| 8 labs in FRANCE | 3 labs in ITALY |
| 2 labs in GEORGIA | 1 lab in JORDAN |
| 2 labs in GERMANY | 1 lab in KAZAKHSTAN |
| 4 labs in GREECE | 1 lab in KENYA |
| 1 lab in GUAM | 1 lab in LATVIA |
| 1 lab in GUINEA REPUBLIC | 1 lab in LITHUANIA |
| 1 lab in HONG KONG | 2 labs in MALAYSIA |
| 1 lab in HUNGARY | 1 lab in MALTA |
| 2 labs in INDIA | 1 lab in MARTINIQUE |
| 2 labs in INDONESIA | 1 lab in MOROCCO |
| 1 lab in IRAN, Islamic Republic of | 2 labs in NETHERLANDS |
| 1 lab in ISRAEL | 1 lab in NIGERIA |
| 3 labs in ITALY | 1 lab in PAKISTAN |
| 1 lab in JORDAN | 1 lab in PERU |
| 1 lab in KAZAKHSTAN | 1 lab in PHILIPPINES |
| 2 labs in KENYA | 2 labs in PORTUGAL |
| 4 labs in LATVIA | 5 labs in RUSSIAN FEDERATION |
| 1 lab in LITHUANIA | 1 lab in SAUDI ARABIA |
| 4 labs in MALAYSIA | 1 lab in SENEGAL |
| 1 lab in MALTA | 1 lab in SERBIA |
| 1 lab in MARTINIQUE | 1 lab in SLOVENIA |
| 1 lab in MOROCCO | 1 lab in SOUTH AFRICA |
| 3 labs in NETHERLANDS | 1 lab in SOUTH KOREA |
| 2 labs in NIGERIA | 5 labs in SPAIN |
| 1 lab in PAKISTAN | 1 lab in SUDAN |
| 1 lab in PERU | 3 labs in SWEDEN |
| 1 lab in PHILIPPINES | 1 lab in THAILAND |
| 3 labs in POLAND | 1 lab in TUNISIA |
| 3 labs in PORTUGAL | 4 labs in TURKEY |
| 1 lab in ROMANIA | 1 lab in UNITED ARAB EMIRATES |
| 13 labs in RUSSIAN FEDERATION | 9 labs in UNITED KINGDOM |
| 2 labs in SAUDI ARABIA | 10 labs in UNITED STATES OF AMERICA |
| 1 lab in SENEGAL | |
| 1 lab in SERBIA | |
| 1 lab in SLOVENIA | |
| 1 lab in SOUTH AFRICA | |
| 2 labs in SOUTH KOREA | |
| 10 labs in SPAIN | |
| 1 lab in SUDAN | |
| 3 labs in SWEDEN | |
| 2 labs in TAIWAN | |
| 1 lab in THAILAND | |
| 1 lab in TUNISIA | |
| 12 labs in TURKEY | |
| 1 lab in UKRAINE | |
| 2 labs in UNITED ARAB EMIRATES | |
| 11 labs in UNITED KINGDOM | |
| 11 labs in UNITED STATES OF AMERICA | |
| 1 lab in VIETNAM | |

APPENDIX 3**Abbreviations:**

| | |
|----------|--|
| C | = final test result after checking of first reported suspect test result |
| D(0.01) | = outlier in Dixon's outlier test |
| D(0.05) | = straggler in Dixon's outlier test |
| G(0.01) | = outlier in Grubbs' outlier test |
| G(0.05) | = straggler in Grubbs' outlier test |
| DG(0.01) | = outlier in Double Grubbs' outlier test |
| DG(0.05) | = straggler in Double Grubbs' outlier test |
| R(0.01) | = outlier in Rosner's outlier test |
| R(0.05) | = straggler in Rosner's outlier test |
| E | = probably an error in calculations |
| U | = test result probably reported in a different unit |
| W | = test result withdrawn on request of participant |
| ex | = test result excluded from statistical evaluation |
| n.a. | = not applicable |
| n.e. | = not evaluated |
| n.d. | = not detected |
| fr. | = first reported |
| SDS | = Safety Data Sheet |

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