# Results of Proficiency Test Base Oil (fresh) May 2015

Organised by: Institute for Interlaboratory Studies

Spijkenisse, the Netherlands

Author: ing. L. Dijkstra

Correctors: dr. R.G. Visser , ing. R.J. Starink & ing. C. Nijssen-Wester

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#### 1 Introduction

Since 2013, the Institute for Interlaboratory Studies organises every year a proficiency test for Base Oil. In the annual proficiency testing program 2014/2015, it was decided to continue the proficiency test for the analyses of Base Oil. In this interlaboratory study 45 laboratories in 32 different countries have participated. See appendix 2 for the number of participants per country. In this report, the results of the 2015 Base Oil proficiency test are presented and discussed. This report is also electronically available through the iis internet site www.iisnl.com.

#### 2 SET UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, the Netherlands, was the organizer of this proficiency test. It was decided to send one bottle of 1L (labelled #15055) of Base Oil that was purchased from a local supplier. The analyses for fit-for-use and homogeneity were subcontracted. Participants were requested to report rounded and unrounded results. The unrounded results were preferably used for statistical evaluation.

## 2.1 ACCREDITATION

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, is accredited in agreement with ISO/IEC 17043:2010 (R007), since January 2000, by the Dutch Accreditation Council (Raad voor Accreditatie). This PT falls under the accredited scope. This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentially of participant's data. Feedback from the participants on the reported data is encouraged and customer's satisfaction is measured on regular basis by sending out questionnaires.

#### 2.2 PROTOCOL

The protocol followed in the organisation was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of April 2014 (iis-protocol, version 3.3). This protocol can be downloaded via the FAQ page of the iis internet site www.iisnl.com.

#### 2.3 CONFIDENTIALITY STATEMENT

All data presented in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

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## 2.4 SAMPLES

The necessary bulk material was obtained from a local supplier. The 200 litre bulk material (a Premium Base 220R) was homogenized and part of this bulk was transferred into 62 brown glass bottles of 1 litre (labelled #15055). The homogeneity of the subsamples #15055 was checked by determination of Density at15°C in accordance with ASTM D4052 and Kinematic Viscosity at 40°C in accordance with ASTM D445 on 8 stratified randomly selected samples.

	Density at 15 °C in kg/L	Kinematic Viscosity at 40°C in mm <sup>2</sup> /s
Sample #15055-1	0.86064	40.25
Sample #15055-2	0.86064	40.23
Sample #15055-3	0.86063	40.22
Sample #15055-4	0.86062	40.22
Sample #15055-5	0.86063	40.24
Sample #15055-6	0.86063	40.19
Sample #15055-7	0.86063	40.19
Sample #15055-8	0.86063	40.25

Table 1: homogeneity test results of subsamples #15055

From the above test results, the repeatabilities were calculated and compared with 0.3 times the corresponding reproducibilities in agreement with the procedure of ISO 13528, Annex B2 in the next table:

	Density at 15 °C in kg/L	Kinematic Viscosity at 40°C in mm <sup>2</sup> /s
r (sample #15055)	0.00001	0.06
reference test	ASTM D4052:11	ASTM D445:15
0.3 x R(reference test)	0.00015	0.16

Table 2: evaluation of the repeatabilities of the subsamples #15055

The calculated repeatabilities were less than 0.3 times the corresponding reproducibilities of the reference test methods. Therefore, homogeneity of the subsample #15055 was assumed.

To each of the participating laboratories, one sample of 1 L in a brown glass bottle (labelled #15055) was sent on May 15, 2015.

#### 2.5 ANALYSES

The participants were requested to determine on sample #15055: Acid Number (Total), Airrelease time at 50°C, Color, Conradson Carbon Residue, Ramsbottom Carbon Residue, Density at 15°C, Evaporation loss by Noack test, Flash Point COC, Kinematic Viscosity at 40°C and at 100°C, Viscosity Index, Viscosity Stabinger at 40°C and at100°C, Pour Point (manual and automated), Rust prevention (proc. B), Sulphur, Water and Water Separability at 54°C.

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To get comparable results a detailed report form, on which the units were prescribed as well as the required standards and a letter of instructions were prepared and made available on the data entry portal www.kpmd.co.uk/sgs-iis/. The detailed report form was also made available for download on the iis website www.iisnl.com. A SDS and a form to confirm receipt of the samples were added to the sample package.

#### 3 RESULTS

During four weeks after sample despatch, the results of the individual laboratories were gathered. The original data are tabulated per determination in the appendix of this report. The laboratories are presented by their code numbers.

Directly after the deadline, a reminder fax was sent to those laboratories that had not reported results at that moment.

Shortly after the deadline, the available results were screened for suspect data. A result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the results. Additional or corrected results are used for data analysis and original results are placed under 'Remarks' in the result tables in appendix 1.

#### 3.1 STATISTICS

Statistical calculations were performed as described in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' (iis-protocol, version 3.3) of April 2014.

For statistical evaluation the *unrounded* (when available) figures were used instead of the rounded results. Results reported as '<...' or '>...' were not used in the statistical evaluation.

First, the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test, a variant of the Kolmogorov-Smirnov test and by the calculation of skewness and kurtosis. Evaluation of the three normality indicators in combination with the visual evaluation of the graphic Kernel density plot, lead to judgement of the normality being either 'unknown', 'OK', 'suspect' or 'not OK'. After removal of outliers, this check was repeated. Not all data sets proved to have a normal distribution, in which cases the statistical evaluation of the results should be used with due care.

According to ISO 5725 the original results per determination were submitted to Dixon's and/or Grubbs' and/or Rosner's outlier tests. Outliers are marked by D(0.01) for the Dixon's test, by G(0.01) or DG(0.01) for the Grubbs' test and by R(0.01) for the Rosner's test (ref. 15). Stragglers are marked by D(0.05) for the Dixon's test, by G(0.05) or DG(0.05) for the Grubbs' test and by R(0.05) for the Rosner's test. Both outliers and stragglers were not included in the calculations of averages and standard deviations.

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For each assigned value the uncertainty was determined in accordance with ISO13528. Subsequently the calculated uncertainty was evaluated against the respective requirement based on the target reproducibility in accordance with ISO13528. When the uncertainty passed the evaluation no remarks are made in the report. However, when the uncertainty failed the evaluation it is mentioned in the report and it will have consequences for the evaluation of the test results.

Finally, the reproducibilities were calculated from the standard deviations by multiplying these with a factor of 2.8.

#### 3.2 GRAPHICS

In order to visualise the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported analysis results are plotted. The corresponding laboratory numbers are under the X-axis.

The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected standard. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle. Furthermore, Kernel Density Graphs were made. The Kernel Density Graph is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. Also a normal Gauss curve was projected over the Kernel Density Graph for reference (see appendix 3; nos.13 and 14).

#### 3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements, e.g. ASTM reproducibilities, the z-scores were calculated using a target standard deviation. This target standard deviation was calculated from the literature reproducibility by division with 2.8.

When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate whether the reported test result is fit-for-use.

The z-scores were calculated according to:

 $z_{\text{(target)}} = \text{(result - average of PT)} / \text{target standard deviation}$ 

Absolute values for z<2 are very common and absolute values for z>3 are very rare.

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Therefore, the usual interpretation of z-scores is as follows:

|z| < 1 good 1 < |z| < 2 satisfactory 2 < |z| < 3 questionable 3 < |z| unsatisfactory

#### 4 **EVALUATION**

In this proficiency test, some problems were encountered during the execution. Six participants reported the test results after the final reporting date and two participants did not report any test results at all. Not all laboratories were able to report all analyses requested. In total 43 participants reported 397 test results. Observed were 11 outlying results, which is 2.8% of the numerical results. In proficiency studies, outlier percentages of 3% - 7.5% are quite normal.

#### 4.1 EVALUATION PER TEST

In this section, the results are discussed per sample and test. The methods, which are used by the various laboratories, were taken into account for explaining the observed differences when possible and applicable. These methods are also in the tables together with the original data. The abbreviations, used in these tables, are listed in appendix 3.

In the iis PT reports, ASTM methods are referred to with a number (e.g. D189) and an added designation for the year that the method was adopted or revised (e.g. D189:06). If applicable, a designation in parentheses is added to designate the year of reapproval (e.g. D189:06(2014). In the results tables of Appendix 1 only the method number and year of adoption or revision e.g. D189:06 will be used.

Not all original data sets proved to have a normal Gaussian distribution. These are referred to as "not OK" or "suspect". The statistical evaluation of these data sets should be used with due care, see also paragraph 3.1.

Acid Number (Total): This determination was not problematic. One statistical outlier was observed. However, the calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ASTM D974:14. When the ASTM D974 data were evaluated separately, the calculated reproducibility is somewhat smaller and again in agreement with the requirements of ASTM D974:12.

#### Air-release time:

This determination was not problematic. One statistical outlier was observed. However, the calculated reproducibility after rejection of the statistical outlier is in agreement with the requirements of ASTM D3427:12.

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Color: This determination was not problematic. No statistical outliers were

observed.

Conradson CR: This determination was not problematic. No statistical outliers were

observed. The calculated reproducibility is in agreement with the

requirements of ASTM D189:06(2014).

Ramsbottom CR: Regretfully, only four test results were reported. This determination may

be problematic. The calculated reproducibility is not in agreement with

the requirements of ASTM D524:10.

This determination was problematic. Two statistical outliers were Density at 15°C:

> observed. The calculated reproducibility after rejection of the statistical outliers is not in agreement with the requirements of ASTM D4052:11.

Evaporation loss:

This determination was not problematic. One statistical outlier was by Noack test observed. However, the calculated reproducibility after rejection of the

statistical outlier is in agreement with the requirements of

ASTM D5800:15-proc B.

One participant reported to have used the method CEC L-040-93, which

is equivalent to ASTM D5800, except this method uses a known

correction factor.

Flash Point COC: This determination was not problematic. No statistical outliers were

observed. The calculated reproducibility is in agreement with ASTM

D92:12b.

<u>Kin.Visco.at 40°C:</u> This determination was not problematic. No statistical outliers were

observed. The calculated reproducibility is in agreement with the

requirements of ASTM D445:15.

Kin.Visco.at 100°C: This determination was not problematic. Two statistical outliers were

observed. However, the calculated reproducibility after rejection of the statistical outliers is in good agreement with the requirements of ASTM

D445:15.

Viscosity Index: This determination was problematic. One statistical outlier was

> observed. The calculated reproducibility after rejection of the statistical outlier is in not agreement with ASTM D2270:10e1. Thirty reported test results were rounded to nearest whole number, as is described in the test method. This means that almost all participants submitted rounded results which might explain (part of) the high spread found. This is the reason that participants are advised to report unrounded results during the round robin. One participant used the Stabinger viscosity result to calculate the viscosity index. Although this is allowed by the method (ASTM D2270), the differences reported for this PT sample for both

Base Oil: iis15L02 page 8 of 34 kinematic and Stabinger viscosities by single laboratories are significant and thus will have an impact on the viscosity index result.

Also iis calculated the Viscosity Index from the test results reported for the kinematic viscosities at 40°C and 100°C. These calculated test results were compared to the reported test results and separately statistically evaluated. The calculated reproducibility after rejection of the three statistical outliers is in full agreement with ASTM D2270:10e1. It may be concluded that reporting less rounded results and not making any calculation errors will significantly improve the performance of the group for viscosity index.

<u>Visco. Stabinger at 40°C:</u> This determination was very problematic. No statistical outliers were observed. However, the calculated reproducibility is not at all in agreement with ASTM D7042:14. The small number of reported results may explain (partly) the spread.

<u>Visco. Stabinger at 100°C:</u> This determination was very problematic. No statistical outliers were observed. However, the calculated reproducibility is not at all in agreement with ASTM D7042:14. The small number of reported results may explain (partly) the spread.

Pour Point: manual

This determination was not problematic. One statistical outlier was observed. However, the calculated reproducibility after rejection of the statistical outlier is in good agreement with the requirements of ASTM D97:12.

Pour Point: automated

This determination was not problematic. No statistical outliers were observed. The calculated reproducibility is in agreement with the requirements of ASTM D5950:14.

Rust prevention:

Regretfully, only six participants reported a test result. Five reported the presence of rust (Fail), while one participant reported the test as "Pass".

Sulphur:

The consensus value of the group was below the application range (3 mg/kg - 4.6 %M/M) of ASTM D2622:10. Therefore, no significant conclusions were drawn. One false positive test result was observed, possibly due to a unit error.

Water:

This determination was not problematic. Two statistical outliers were observed. However, the calculated reproducibility after rejection of the statistical outliers is in good agreement with the requirements of ASTM D6304:07.

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Water separability: This determination was not problematic. No statistical outliers were observed. The calculated reproducibilities are in good agreement with the requirements of ASTM D1401:12.

> ASTM D1401 describes complete break only as '40-40-0', whereas a complete break also was interpreted as 'no emulsion layer present'. All participants, except one, reported the complete break as 40-40-0. One participant reported the complete break as 40-39-1.

#### PERFORMANCE EVALUATION FOR THE GROUP OF LABORATORIES

A comparison has been made between the reproducibility as declared by the relevant standard and the reproducibility as found for the group of participating laboratories that participated. The average results, calculated reproducibilities and reproducibilities derived from literature standards (in casu ASTM standards), are compared in the next table.

Parameter	Unit	n	Average	2.8 * sd	R(lit)
Acid Number, Total	mg KOH/g	21	0.013	0.027	0.040
Air-release time at 50°C	Min	6	1.8	1.4	1.7
Color		40	L0.5	n.a.	n.a.
Conradson Carbon Residue	%M/M	12	0.008	0.017	0.021
Ramsbottom Carbon Residue	%M/M	4	0.047	0.035	0.027
Density at 15 °C	kg/L	39	0.8607	0.0006	0.0005
Evaporation loss by Noack	%M/M	10	9.11	0.78	1.25
Flash Point COC	°C	34	234	15	18
Kinematic Viscosity at 40 °C	mm²/s	36	40.48	0.40	0.55
Kinematic Viscosity at 100 °C	mm²/s	33	6.432	0.048	0.122
Viscosity Index		35	108.5	2.8	2.0
Stabinger Viscosity at 40 °C	mm²/s	9	40.58	0.71	0.24
Stabinger Viscosity at 100 °C	mm²/s	9	6.446	0.100	0.033
Pour Point manual	°C	25	-12.2	4.1	9.0
Pour Point automated	°C	15	-13.4	4.9	4.5
Rust Prevention (proc. B)		6	fail	n.a.	n.a.
Sulphur	mg/kg	14	<3	n.a.	n.a.
Water	mg/kg	27	21.2	17.9	105.6
Water Separability at 54°C					
- Time to reach 3 ml or less emulsion	min	8	3.6	6.5	20.0
- Time to reach 37 of water	min	8	3.3	6.5	20.0

Table 3: reproducibilities of results of sample #15055

Without further statistical calculations it can be concluded that for a number of tests there is a good compliance of the group of participants with the relevant standards. The tests that are problematic have been discussed in paragraph 4.1.

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#### 4.3 COMPARISON OF THE PROFICIENCY TEST OF MAY 2015 WITH PREVIOUS PTS

	May 2015	May 2014	May 2013
Number of reporting labs	43	43	28
Number of results reported	397	408	260
Statistical outliers	11	19	17
Percentage outliers	2.8%	4.7%	6.5%

Table 4: comparison with previous proficiency tests

In proficiency tests, outlier percentages of 3% - 7.5% are quite normal.

The performance of the determinations of the proficiency tests was compared to the requirements of the respective standards.

The conclusions are given in the following table:

Determination	May 2015	May 2014	May 2013
Acid Number, Total	+	+/-	+/-
Air-release time at 50°C	+	-	n.e.
Color	n.e.	+	++
Conradson Carbon Residue	+	++	-
Ramsbottom Carbon Residue	-		n.e.
Density at 15 °C	-	++	
Evaporation loss by Noack	+		
Flash Point COC	+	+/-	+
Kinematic Viscosity at 40 °C	+		
Kinematic Viscosity at 100 °C	++		-
Viscosity Index	-		+
Stabinger Viscosity at 40 °C			
Stabinger Viscosity at 100 °C			
Pour Point manual	++	-	-
Pour Point automated	+/-	n.e.	n.e.
Rust Prevention	n.e.	n.e.	n.e.
Sulphur	n.e.	+	+/-
Water	++	++	+
Water Separability at 54°C	++	++	++

Table 5: comparison determinations against the standard

The performance of the determinations against the requirements of the respective standards is listed in the above table. The following performance categories were used:

++: group performed much better than the standard

+ : group performed better than the standard

+/-: group performance equals the standard

- : group performed worse than the standard

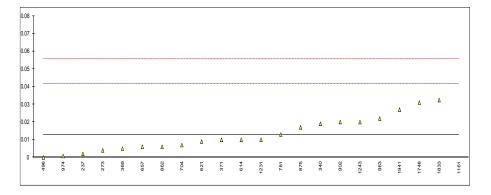
--: group performed much worse than the standard

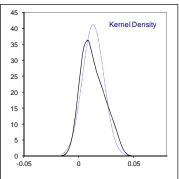
n.e.: not evaluated

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APPENDIX 1
Determination of Acid Number (Total) on sample #15055; results in mg KOH/g

lab	method	value	mark	z(targ)	remarks
237	D974	0.002	man	-0.76	Tomano
273	D974	0.002		-0.62	
311	D974	<0.02			
315	D014				
323	D974	< 0.02			
337	D314				
340	D974	0.019		0.43	
357	D664	<0.05			
369	D974	0.005		-0.55	
371	D974	0.01		-0.20	
396	2011				
432					
445					
446	D974	< 0.02			
485	20				
494	D664	< 0.05			
496	D974	0.000		-0.90	
541	D974	<0.1			
551	20				
601					
614	D974	0.01		-0.20	
621	D664	0.009		-0.27	
657	D974	0.006		-0.48	
704	D974	0.007		-0.41	
781	D974	0.013		0.01	
862	D974	0.006		-0.48	
875	D664	0.017		0.29	
902	D664	0.02		0.50	
922	D664	<0.10			
963	D974	0.022		0.64	
974	D974	0.0008		-0.85	
1011	D974	< 0.02			
1026	D974	< 0.03			
1161	D664	1.002	R(0.01)	69.24	possibly a unit error?
1231	D664	0.01		-0.20	
1243	D974	0.02		0.50	
1349					
1461					
1682					
1748	D664	0.031		1.27	
1833	D664	0.0324		1.36	
1877					
1941	ISO6618	0.027		0.99	
1963					
1971					
					Only ASTM D974 data
	normality	OK			OK
	n	21			16
	outliers	1			0
	mean (n)	0.0129			0.0100
	st.dev. (n)	0.00972			0.00806
	R(calc.)	0.0272			0.0226
	R(D974:14)	0.0400			0.0400

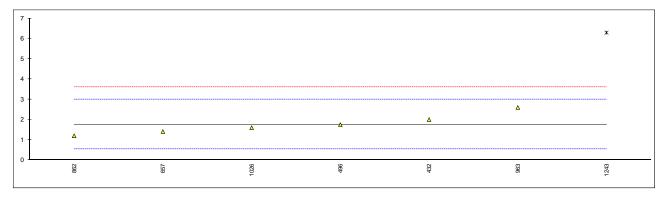




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## Determination of Air-release time at 50°C on sample #15055; results in min

lab	method	value	mark	z(targ)	remarks
237					
273					
311					
315					
323					
337					
340 357					
369					
371					
396					
432	ISO9120	2.0		0.39	
445					
446					
485					
494	D0.407	4.75			
496	D3427	1.75		-0.02	
541 551					
601					
614					
621					
657	D3427	1.41		-0.57	
704					
781	_				
862	D3427	1.2		-0.91	
875 902					
902 922					
963	D3427	2.6		1.36	
974	50121				
1011					
1026	D3427	1.6		-0.26	
1161					
1231					
1243	D3427	6.3	C,G(0.01)	7.37	
1349 1461					
1682					
1748					
1833					
1877					
1941					
1963					
1971					
	normality	unknown			
	normality n	unknown 6			
	outliers	1			
	mean (n)	1.76			
	st.dev. (n)	0.495			
	R(calc.)	1.39			
	R(D3427:12)	1.72			



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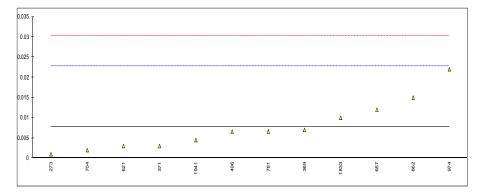
## Determination of Color on sample #15055

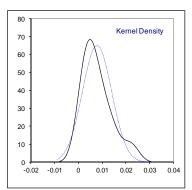
lab	method	value	mark	z(targ)	remarks
237	D1500	L0.5	man	<u>=(ta.g/</u>	Tomarko
273	D1500	L0.5			
311	D1500	L0.5			
315	D1500	L0.5			
323	D1500	L0.5			
337	D1500	L0.5			
340	D1500	L0.5			
357	D1500	L0.5			
369	D1500	L0.5			
371 396	D1500	L0.5 L0.5			
	D1500				
432	D1500	L0.5			
445	D4500				
446	D1500	L0.5			
485	D1500	L0.5			
494	D1500	L0.5			
496	D1500	0.0			
541	D1500	L0.5			
551	D.1500				
601	D1500	L0.5			
614	D1500	L0.5			
621	D1500	L0.5			
657	D1500	L0.5			
704	D1500	L0.5			
781	D1500	L0.5			
862	D1500	L0.5			
875	D1500	L0.5			
902	D1500	L0.5			
922	D1500	L0.5			
963	D1500	0.4			
974	D1500	L0.5			
1011	D1500	L0.5			
1026	D1500	L0.5			
1161	D6045	L0.5			
1231	D1500	L0.5			
1243	D1500	0.1			
1349	D1500	L0.5			
1461	ISO2049	0.5			
1682					
1748	D1500	0			
1833	D1500	L0.5			
1877	D6045	L0.5			
1941	ISO2049	L0.5			
1963					
1971					
	normality	n.a.			
	n	40			
	outliers	n.a.			
	mean (n)	L0.5			
	st.dev. (n)	n.a.			
	R(calc.)	n.a.			
	R(D1500:12)	n.a.			

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## Determination of Conradson Carbon Residue on sample #15055; results in %M/M

lab	method	value	mark z	(targ)	remarks
237					
273	D189	0.001		-0.90	
311					
315					
323	D4530	<0.10			
337					
340	D4530	<0.10			
357					
369	D4530	0.007		-0.10	
371	D189	0.003		-0.63	
396					
432					
445					
446					
485	D.4500				
494	D4530	<0.01		0.45	
496	D4530	0.0066		-0.15	
541					
551 601					
601 614					
621	D189	0.003		-0.63	
657	D4530	0.003		0.57	
704	D189	0.002		-0.76	
781	D4530	0.0066		-0.15	
862	D4530	0.015		0.97	
875	D 1000				
902	D4530	<0.1			
922	D189	<0.01			
963					
974	D4530	0.022		1.90	
1011					
1026					
1161					
1231					
1243	D189	<0.01			
1349					
1461					
1682					
1748					
1833	D4530	0.01		0.30	
1877	1001000				
1941	ISO10370	0.0045		-0.43	
1963					
1971					
	normality	not OK			
	normality n	10t OK 12			
	outliers	0			
	mean (n)	0.0077			
	st.dev. (n)	0.00615			
	R(calc.)	0.0172			
	R(D189:06)	0.0210			
		-			

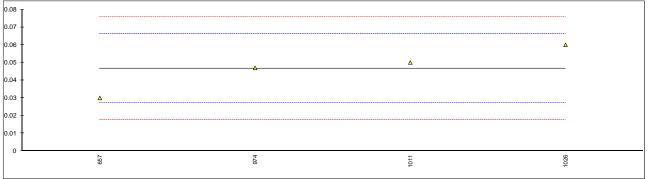




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## Determination of Ramsbottom Carbon Residue on sample #15055; results in %M/M

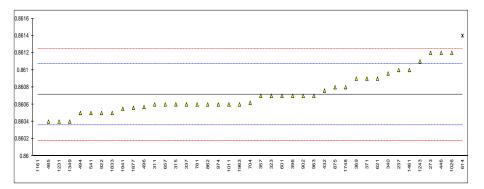
377 311 315 323 323 324 325 327 340 396 397 396 397 396 397 397 445 445 446 485 494 485 697 697 697 797 797 797 797 797 797 797	lab	method	value	mark	z(targ)	remarks
273				man		
311						
315	311					
323 340	315					
340	323					
357	337					
369						
371 396	357					
396						
432						
446						
446						
486						
494 496						
496						
551 601						
601 614 627 D524 0.03 -1.73 704 81 862 875 902 902 903 974 D524 0.047 0.03 1011 D524 0.05 0.34 1026 D524 0.06 1.37 1161 1231 1243 1349 1461 1748 1748 1748 1748 1748 1748 1748 1748 1748 1748 1748 1748 1748 1748 1748 1749 1963 1971  normality unknown n						
614						
621						
657 D524 0.03 -1.73 704 781 862 902 902 963 974 D524 0.047 0.03 974 D524 0.05 0.34 1026 D524 0.06 1.37 1161 1231 1349 1461 1461 1748 1877 1941 1963 1971 normality unknown n						
704		DE04				
781 862 875		D524				
862 875 972 902 903 974 D524 0.047 0.03 1011 D524 0.05 0.34 1026 D524 0.06 1.37 1161 1231 1349 1461 1682 1748 1748 1941 1963 1971   normality unknown n	704 781					
875						
902						
922						
974						
1011 D524 0.05 0.34 1026 D524 0.06 1.37 1161						
1026 D524 0.06 1.37 1161 1231 1243 1349 1461 1682 1748 1833 1941 1963 1971  normality unknown n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027						
1161 1231 1243 1349 1461 1582 1748 1833 1941 1963 1971  normality unknown n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027	1011	D524			0.34	
1231 1243 1349 1461 1582 1748 1877 1941 1963 1971 1971		D524				
1243 1349 1461 1682 1748 1833 1877 1941 1963 1971  normality unknown n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027	1161					
1349 1461 1682 1748 1833 1877 1941 1963 1971  normality unknown n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027						
1461	1349					
1682						
1748 1833 1941 1963 1971  normality unknown n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027						
1833 1841 1963 1971  normality unknown n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027	1748					
1877 1941 1963 1971  normality unknown n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027	1833					
1963 1971 normality unknown n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027						
normality unknown n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027	1941					
normality unknown n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027						
n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027	19/1					
n 4 outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027		normality	unknown			
outliers 0 mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027						
mean (n) 0.047 st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027						
st.dev. (n) 0.0125 R(calc.) 0.035 R(D524:10) 0.027		mean (n)				
R(calc.) 0.035 R(D524:10) 0.027		st.dev. (n)	0.0125			
R(D524:10) 0.027		R(calc.)	0.035			
		R(D524:10)	0.027			
	0.08					
0.07 +						
	0.07	<u></u>				

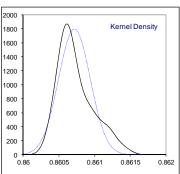


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## Determination of Density at 15°C on sample #15055; results in kg/L

lab	method	value	mark	z(targ)	remarks
237	D4052	0.8610	С	1.61	first reported: 861.0
273	D4052	0.8612		2.73	'
311	D4052	0.8606		-0.63	
315	D4052	0.8606		-0.63	
323	D4052	0.8607		-0.07	
337	ISO12185	0.8606		-0.63	
340	D4052	0.86096		1.38	
357	D4052 D4052	0.8607		-0.07	
369				1.05	
	D4052	0.8609			
371	D4052	0.8609		1.05	
396	D4052	0.8607		-0.07	
432	D4052	0.86076		0.26	
445	D 1050				
446	D4052	0.8612		2.73	
485	D4052	0.8604		-1.75	
494	D4052	0.8605		-1.19	
496	D4052	0.86057		-0.80	
541	D4052	0.8605		-1.19	
551					
601	D1298	0.8607		-0.07	
614	D4052	0.8614	R(0.05)	3.85	
621	D4052	0.8609	С	1.05	probably unit error, reported: 860.9
657	D4052	0.8606		-0.63	
704	D4052	0.86062		-0.52	
781	D4052	0.8606		-0.63	
862	D4052	0.8606		-0.63	
875	D4052	0.8608		0.49	
902	D4052	0.8607		-0.07	
922	D4052	0.8605		-1.19	
963	D4052	0.8607		-0.07	
974	D4052	0.8606		-0.63	
1011	D4052	0.8606		-0.63	
1026	D4052	0.8612		2.73	
1161	ISO3675	0.8570	R(0.01)	-20.79	
1231	D4052	0.8604		-1.75	
1243	D4052	0.8611		2.17	
1349	IP365	0.8604		-1.75	
1461	ISO3675	0.8610	С	1.61	probably unit error, reported: 861.0
1682					
1748	D4052	0.8608		0.49	
1833	D4052	0.8605		-1.19	
1877	D4052	0.86056		-0.86	
1941	D4052	0.86055		-0.91	
1963	D4052	0.8606		-0.63	
1971					
	normality	OK			
	n	39			
	outliers	2			
	mean (n)	0.86071			
	st.dev. (n)	0.000222			
	R(calc.)	0.00062			
	R(D4052:11)	0.00050			

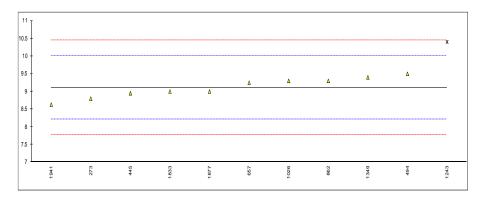


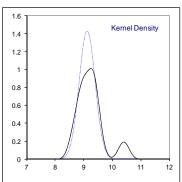


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## Determination of Evaporation loss by Noack test on sample #15055; results in %M/M

lab	method	value	mark	z(targ)	remarks
237					
273	D5800 - B	8.8		-0.70	
311					
315 323					
337					
340					
357					
369					
371					
396					
432 445	D5800 - B	8.95		-0.37	
446	D3600 - B	0.93		-0.37	
485					
494	D5800 - B	9.5		0.87	
496					
541					
551					
601 614					
621					
657	D5800 - B	9.25		0.31	
704					
781					
862	D5800 - B	9.3		0.42	
875					
902 922					
963					
974					
1011					
1026	CEC L-40-93	9.3		0.42	
1161					
1231	DEGGG	40.40	C(0.05)	2.00	
1243 1349	D5800 D5800 - B	10.40 9.4	G(0.05)	2.89 0.64	
1461	D3000 - D			0.04	
1682					
1748					
1833	D5800 - A	9.0		-0.25	
1877	D5800 - A	9.0		-0.25	
1941	D5800 - A	8.63		-1.08 	
1963 1971					
1371					
	normality	OK			
	n	10			
	outliers	1			
	mean (n)	9.113			
	st.dev. (n) R(calc.)	0.2797 0.783			
	R(D5800:15-B)	1.249			Compare R(D5800:15-A) = 1.668
	(2000.10 2)				

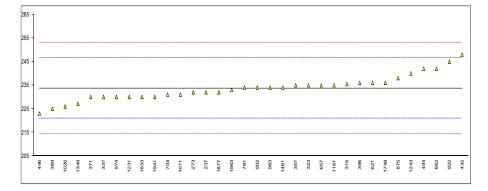


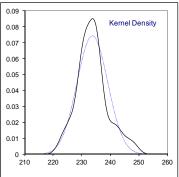


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## Determination of Flash Point C.O.C. on sample #15055; results in °C

237 D92 232 -0.27 273 D92 232 -0.27 311 D92 232 -0.27 315 D92 235.505 0.28 323 D92 230 -0.58 323 D92 230 -0.58 340	lab	method	value	mark z(targ)	remarks
273 D92 232 -0.27 315 D92 235.505	237	D92	232		
311	273	D92	232		
1922   235					
337 D92 230 -0.58 340 357 D92 235 0.20 369 D92 225 -1.36 371 D92 230 -0.58 396 D92 236 0.35 432 D92 248 2.22 4445 445 D92 223 -1.67 485 D92 242 1.29 496 551 601 614 614 614 D92 236 0.35 657 D92 236 0.35 657 D92 236 0.35 657 D92 236 0.035 657 D92 236 0.035 657 D92 236 0.035 657 D92 235 0.20 704 D92 231 -0.42 781 D92 234 0.04 782 D92 244 0.04 782 D92 244 0.04 784 D92 234 0.04 785 D92 234 0.04 786 D92 234 0.04 787 D92 234 0.04 788 D92 234 0.04 789 D92 230 0.58 789 D92 234 0.04 789 D92 230 0.58 78	315	D92	235.505	0.28	
340	323	D92	235	0.20	
196	337	D92	230	-0.58	
369 D92 225 -1.36 371 D92 230 -0.58 396 D92 236	340				
371 D92 230 -0.58 386 D92 236 0.35 432 D92 248 2.22 445					
396 D92 236 0.35 432 D92 248 2.22 445		D92	225	-1.36	
432 D92 248 2.22 446 D92 223 -1.67 446 D92 223 -1.67 447 D92 242 1.29 486					
445					
486 D92 223 -1.67 485 484 D92 242 1.29 486 541 601 614 614 621 D92 236.0 0.35 657 D92 235 0.20 704 D92 231 -0.42 781 D92 231 -0.42 781 D92 234 0.04 862 D92 242 1.29 875 D92 238 0.67 902 D92 244 0.04 862 D92 245 0.04 875 D92 236 0.05 876 D92 236 0.04 877 D92 237 -0.42 878 D92 238 0.67 902 D92 245.0 1.75 903 D92 245.0 1.75 903 D92 234 0.04 974 D92 230 -0.58 1011 D92 231 -0.42 1026 D92 226 -1.20 1161 ISO2592 235 0.0.20 1231 D92 230 -0.58 1243 D92 240 0.98 1243 D92 240 0.98 1243 D92 240 0.98 1243 D92 230 -0.58 1833 D92 230 -0.58 1839 D92 233 -0.11 1871		D92			
485					
494 D92 242 1.29 496		D92			
496 541 551 601 614 621 D92 236.0 0.35 657 D92 235 0.20 704 D92 231 -0.42 781 D92 234 0.04 862 D92 242 1.29 875 D92 238 0.67 902 D92 234.0 0.04 922 D92 235 0.20 1.75 963 D92 234 0.04 974 D92 230 -0.58 1011 D92 231 -0.42 11026 D92 226 -1.20 1161 ISO2592 235.0 0.20 1231 D92 230 -0.58 1349 D92 227.1 -1.03 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1877 D92 230 -0.58 1877 D92 530 -0.58 1877 D93 5375		B00			
541 551 601		D92			
551 601 614 621 D92					
601 614 621 D92 236.0 0.35 657 D92 235 0.20 704 D92 231 0.42 781 D92 234 0.04 862 D92 242 1.29 875 D92 238 0.67 902 D92 234 0.04 922 D92 245.0 1.75 963 D92 234 0.04 974 D92 230 -0.58 1011 D92 231 1-0.42 1026 D92 126 1.20 1161 ISO2592 235.0 0.20 1231 D92 240 0.98 1349 D92 240 0.98 1349 D92 2271 1.03 1461 ISO2592 234 0.04 1882 1748 D92 230 0.58 1833 D92 230 0.58 1837 D92 233 0.011  normality OK n ormality OK ormality OR ormality OR ormality OR ormality OR ormality OR ormality OR					
614					
621 D92 236.0 0.35 657 D92 235 0.20 704 D92 231 -0.42 781 D92 234 0.04 862 D92 242 1.29 875 D92 238 0.67 902 D92 245.0 1.75 963 D92 245.0 1.75 963 D92 234 0.04 974 D92 230 -0.58 1011 D92 231 -0.42 1026 D92 226 -1.20 1161 ISO2592 235.0 0.20 1231 D92 230 -0.58 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1882 1748 D92 236 0.35 1833 D92 230 -0.58 1833 D92 233 -0.58 1833 D92 230 -0.58 1833 D92 230 -0.58 1833 D92 230 -0.58 1833 D92 230 -0.58 1839 D92 230 -0.58 1839 D92 230 -0.58 1849 D92 227.1 -1.03 1461 ISO2592 234 0.04 1882 1748 D92 236 0.35 1833 D92 230 -0.58 1833 D92 230 -0.58 1833 D92 230 -0.58 1833 D92 230 -0.58 1839 D92 233 -0.11 18961 D92 233 -0.11 18971  normality OK n					
657 D92 235 0.20 704 D92 231 -0.42 781 D92 234 0.04 862 D92 242 1.29 875 D92 238 0.67 902 D92 234.0 0.04 922 D92 245.0 1.75 963 D92 234 0.04 974 D92 230 -0.58 1011 D92 231 -0.42 1026 D92 226 -1.20 1161 ISO2592 235.0 0.20 1231 D92 230 -0.58 1243 D92 240 0.98 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1877 D92 230 -0.58 1877 D92 233 -0.58 1877 D92 230 -0.58 1877 D92 231 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375		DOS			
704 D92 231 -0.42 781 D92 234 0.04 862 D92 242 1.29 875 D92 238 0.67 902 D92 234.0 0.04 922 D92 245.0 1.75 963 D92 234 0.04 974 D92 230 -0.58 1011 D92 231 -0.42 1026 D92 226 -1.20 1161 ISO2592 235.0 0.20 1231 D92 230 -0.58 1243 D92 240 0.98 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1833 D92 236 0.35 1877 D92 230 -0.58					
781 D92 234 0.04 862 D92 242 1.29 875 D92 238 0.67 902 D92 234.0 0.04 922 D92 245.0 1.75 963 D92 234 0.04 974 D92 230 -0.58 1011 D92 231 -0.42 1026 D92 226 -1.20 1161 ISO2592 235.0 0.20 1231 D92 230 -0.58 1243 D92 240 0.98 1243 D92 240 0.98 1244 D92 227.1 -1.03 1461 ISO2592 234 0.04 1882 1748 D92 236 0.35 1877 D92 230 -0.58 1877 D92 233 -0.11 1971  normality OK n					
862       D92       242       1.29         875       D92       238       0.67         902       D92       234.0       0.04         922       D92       245.0       1.75         963       D92       234       0.04         974       D92       230       -0.58         1011       D92       231       -0.42         1026       D92       226       -1.20         1161       ISO2592       235.0       0.20         1231       D92       230       -0.58         1243       D92       240       0.98         1349       D92       227.1       -1.03         1461       ISO2592       234       0.04         1682           1748       D92       236       0.35         1833       D92       230       -0.58         1963       D92       233       -0.11         1971           normality       OK       n       34         outliers       0       mean (n)       233.72         st.dev. (n)       5.375       5.375   <			234		
875 D92 D92 234.0 0.04 902 D92 245.0 1.75 963 D92 234 0.004 974 D92 230 -0.58 1011 D92 231 -0.42 1026 D92 226 -1.20 1161 ISO2592 235.0 0.20 1231 D92 230 -0.58 1243 D92 240 0.98 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375			242		
902 D92 234.0 0.04 922 D92 245.0 1.75 963 D92 234 0.04 974 D92 230 -0.58 1011 D92 231 -0.42 1026 D92 226 -1.20 1161 ISO2592 235.0 0.20 1231 D92 230 -0.58 1243 D92 240 0.98 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1833 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
922 D92 245.0 1.75 963 D92 234 0.04 974 D92 230 -0.58 1011 D92 231 -0.42 1026 D92 226 -1.20 1161 ISO2592 235.0 0.20 1231 D92 240 0.98 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.58 1877 D92 232 -0.58 1963 D92 233 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
963					
974 D92 230 -0.58 1011 D92 231 -0.42 1026 D92 226 -1.20 1161 ISO2592 235.0 0.20 1231 D92 230 -0.58 1243 D92 240 0.98 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1833 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
1011 D92 231 -0.42 1026 D92 226 -1.20 1161 ISO2592 235.0 0.20 1231 D92 230 -0.58 1243 D92 240 0.98 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
1026 D92 226 -1.20 1161 ISO2592 235.0 0.20 1231 D92 230 -0.58 1243 D92 240 0.98 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
1161 ISO2592 235.0 0.20 1231 D92 230 -0.58 1243 D92 240 0.98 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
1231 D92 230 -0.58 1243 D92 240 0.98 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
1243 D92 240 0.98 1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
1349 D92 227.1 -1.03 1461 ISO2592 234 0.04 1682 1748 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375		D92	240		
1682 1748 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
1748 D92 236 0.35 1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375		ISO2592			
1833 D92 230 -0.58 1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
1877 D92 232 -0.27 1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
1941 ISO2592 230 -0.58 1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375			230		
1963 D92 233 -0.11 1971  normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375	1877		232	-0.27	
normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375					
normality OK n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375		D92			
n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375	1971				
n 34 outliers 0 mean (n) 233.72 st.dev. (n) 5.375			014		
outliers 0 mean (n) 233.72 st.dev. (n) 5.375		•			
mean (n) 233.72 st.dev. (n) 5.375					
st.dev. (n) 5.375					
st.dev. (n) 5.375 R(calc.) 15.05					
KICACO TOUCH			5.3/5		
R(D92:12b) 18.00		K(D92.120)	10.00		

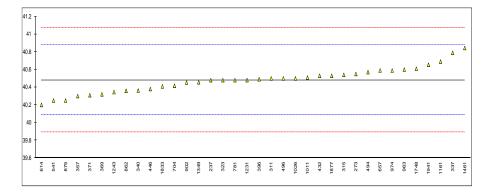


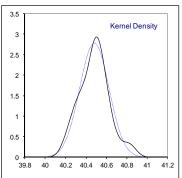


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## Determination of Kinematic Viscosity at 40°C on sample #15055; results in mm<sup>2</sup>/s

lab	method	value	mark	z(targ)	remarks
237	D445	40.48		-0.01	
273	D445	40.55		0.35	
311	D445	40.50		0.10	
315	D445	40.54		0.30	
323	D445	40.48		-0.01	
337	ISO3104	40.79		1.57	
340	D445	40.363		-0.60	
357	D445	40.30		-0.92	
369	D445	40.32		-0.82	
371	D445	40.31		-0.87	
396	D445	40.49		0.04	
432	D445	40.53		0.25	
445					
446	D445	40.38		-0.51	
485	2				
494	D445	40.57		0.45	
496	D445	40.500		0.10	
541	D445	40.25		-1.18	
551	2110				
601					
614	D445	40.2	С	-1.43	first reported: 40
621	2110		Ü		mot roportod. To
657	D445	40.59		0.55	
704	D445	40.416		-0.33	
781	D445	40.48		-0.01	
862	D445	40.36		-0.62	
875	D445	40.25		-1.18	
902	D445	40.4547		-0.13	
922	D773				
963	D445	40.60		0.60	
974	D445	40.59		0.55	
1011	D445	40.51		0.15	
1026	D445	40.50		0.10	
1161	D445	40.69		1.06	
1231	D445	40.48		-0.01	
1243	D445	40.345		-0.69	
1349	D445	40.4564		-0.13	
1461	ISO3104	40.8438		1.84	
1682	1000104				
1748	D445	40.61		0.66	
1833	D445	40.41		-0.36	
1877	D445	40.53		0.25	
1941	ISO3104	40.654		0.23	
1963	.500104				
1971					
1311				<b>-</b>	
	normality	OK			
	n	36			
	outliers	0			
	mean (n)	40.481			
	st.dev. (n)	0.1434			
	R(calc.)	0.402			
	R(D445:15)	0.551			
	11(0770.10)	0.001			

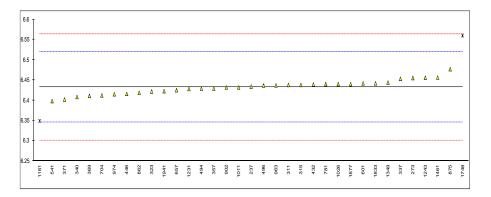


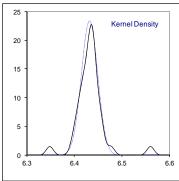


Base Oil: iis15L02 page 20 of 34

## Determination of Kinematic Viscosity at 100°C on sample #15055; results in mm<sup>2</sup>/s

lab	method	value	mark	z(targ)	remarks
237	D445	6.434		0.04	
273	D445	6.455		0.52	
311	D445	6.438		0.13	
315	D445	6.438		0.13	
323	D445	6.422		-0.24	
337	ISO3104	6.453		0.47	
340	D445	6.4082		-0.55	
357	D445	6.429		-0.08	
369	D445	6.411		-0.49	
371	D445	6.402		-0.70	
396	-				
432	D445	6.439		0.15	
445					
446	D445	6.416		-0.38	
485					
494	D445	6.429		-0.08	
496	D445	6.4365		0.09	
541	D445	6.398		-0.79	
551	2				
601	D445	6.442		0.22	
614					
621					
657	D445	6.425		-0.17	
704	D445	6.4123		-0.46	
781	D445	6.440		0.17	
862	D445	6.419		-0.31	
875	D445	6.477		1.02	
902	D445	6.432		-0.01	
922					
963	D445	6.437		0.11	
974	D445	6.415		-0.40	
1011	D445	6.432		-0.01	
1026	D445	6.44		0.17	
1161	D445	6.349	R(0.01)	-1.91	
1231	D445	6.428	( /	-0.10	
1243	D445	6.456		0.54	
1349	D445	6.4439		0.26	
1461	ISO3104	6.4563		0.55	
1682					
1748	D445	6.560	R(0.01)	2.92	
1833	D445	6.442	. ,	0.22	
1877	D445	6.440		0.17	
1941	ISO3104	6.4225		-0.23	
1963					
1971					
	normality	OK			
	n	33			
	outliers	2			
	mean (n)	6.4324			
	st.dev. (n)	0.01705			
	R(calc.)	0.0477			
	R(D445:15)	0.1222			

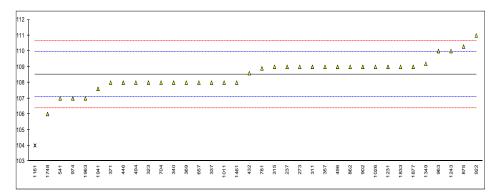


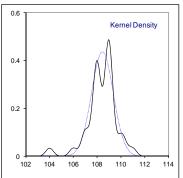


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## Determination of Viscosity index on sample #15055

lab	method	value	mark	z(targ)	calc.iis	mark	remarks
237	D2270	109		0.66	108.73		
273	D2270	109		0.66	109.35		
311	D2270	109		0.66	108.82		
315	D2270	109		0.66	108.64		
323	D2270	108		-0.74	108.19		
337	ISO2909	108		-0.74	108.18		
340	D2270	108		-0.74	108.11		
357	D2270	109		0.66	109.33		
369	D2270	108		-0.74	108.43		
371	D2270	108.0		-0.74	108.07		
396							
432	D2270	108.6		0.10	108.73		
445							
446	D2270	108		-0.74	108.38		
485							
494	D2270	108		-0.74	108.10		
496	D2270	109		0.66	108.75		
541	D2270	107		-2.14	108.16		
551							
601							
614							
621							
657	D2270	108		-0.74	107.83		
704	D2270	108.0		-0.74	108.05		
781	D2270	108.9		0.52	109.00		
862	D2270	109		0.66	108.61		
875	D2270	110.288		2.46	111.71	R(0.01)	E
902	D2270	109		0.66	108.76		
922	D2270	111		3.46	110.79		
963	D2270	110		2.06	108.32		E
974	D2270	107		-2.14	107.39		
1011	D2270	108		-0.74	108.51		
1026	D2270	109		0.66	108.91		
1161	D2270	104	R(0.01)	-6.34	103.99	R(0.01)	Outlier in viscosity at 100°C
1231	D2270	109		0.66	108.46		
1243	D2270	110		2.06	110.33		
1349	D2270	109.2		0.94	109.28		
1461	ISO2909	108		-0.74	108.08		
1682	D0070	4.00		2.54	440.74	D(0.04)	F and autlies in viscosity at 40000
1748	D2270	106		-3.54	113.71	R(0.01)	E and outlier in viscosity at 100°C
1833	D2270	109		0.66	109.41		
1877	D2270	109		0.66	108.77		
1941	ISO2909	107.6		-1.30	107.43		
1963	D7042	107		-2.14			
1971							
	normality	ОК			OK		
	n	35			32		
	outliers	1			3		
	mean (n)	108.53			108.62		
	st.dev. (n)	1.002			0.716		
	R(calc.)	2.81			2.00		
	R(D2270:10e1)	2.00			2.00		
	` '						

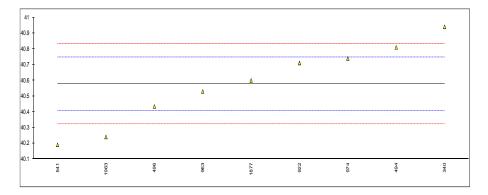


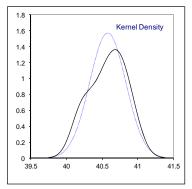


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## Determination of Viscosity Stabinger at 40 °C on sample #15055; results in mm<sup>2</sup>/s

lab	method	value	mark	z(targ)	remarks
237					
273					
311					
315					
323					
337					
340	D7042	40.940		4.29	
357					
369					
371					
396					
432					
445					
446					
485	D7040	40.04		0.75	
494	D7042	40.81		2.75	
496 541	D7042	40.434		-1.69	
541 551	D7042	40.19 		-4.57 	
601					
614					
621					
657					
704					
781					
862					
875					
902					
922	D7042	40.71		1.57	
963	D7042	40.53		-0.56	
974	D7042	40.739		1.91	
1011					
1026					
1161					
1231					
1243					
1349					
1461 1682					
1748					
1833					
1877	D7042	40.60		0.27	
1941	D7012				
1963	D7042	40.24		-3.98	
1971					
	normality	OK			
	n	9			
	outliers	0			
	mean (n)	40.577			
	st.dev. (n)	0.2541			
	R(calc.)	0.711			
	R(D7042:14)	0.237			

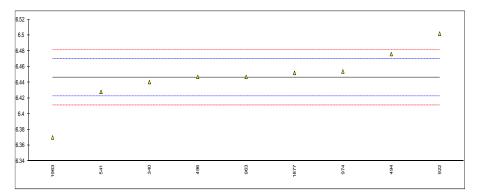


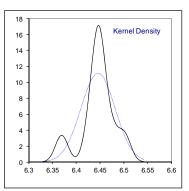


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## Determination of Viscosity Stabinger at 100 °C on sample #15055; results in mm<sup>2</sup>/s

lab	method	value	mark	z(targ)	remarks
237					
273					
311					
315					
323					
337					
340	D7042	6.4404		-0.50	
357					
369					
371					
396					
432					
445					
446 485					
494	D7042	6.476		2.52	
496	D7042	6.447		0.06	
541	D7042	6.428		-1.55	
551	D7012				
601					
614					
621					
657					
704					
781					
862					
875					
902	<b>5</b>				
922	D7042	6.502		4.72	
963	D7042	6.447		0.06	
974 1011	D7042	6.454		0.65	
1011					
1161					
1231					
1243					
1349					
1461					
1682					
1748					
1833	_				
1877	D7042	6.452		0.49	
1941	D70.40				
1963	D7042	6.370		-6.46	
1971					
	normality	not OK			
	n	9			
	outliers	0			
	mean (n)	6.4463			
	st.dev. (n)	0.03583			
	R(calc.)	0.1003			
	R(D7042:14)	0.0331			
	,				

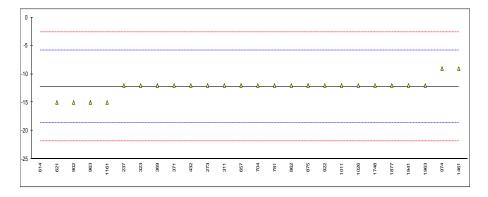


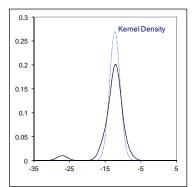


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## Determination of Pour Point manual on sample #15055; results in °C

lab	method	value	mark	z(targ)	remarks
237	D97	-12		0.07	
273	D97	-12		0.07	
311	D97	-12		0.07	
315	20.				
323	D97	-12		0.07	
337	501				
340					
357					
369	D97	-12		0.07	
371	D97	-12		0.07	
396	501				
432	D97	-12		0.07	
445					
446					
485					
494					
496					
541					
551					
601					
614	D97	-27	C,R(0.01)	-4.59	first reported: -24
621	D97	-15.0	-,: (-:)	-0.86	
657	D97	-12		0.07	
704	D97	-12		0.07	
781	D97	-12		0.07	
862	D97	-12		0.07	
875	D97	-12		0.07	
902	D97	-15		-0.86	
922	D97	-12.0		0.07	
963	D97	-15		-0.86	
974	D97	-9		1.01	
1011	D97	-12		0.07	
1026	D97	-12		0.07	
1161	D97	-15		-0.86	
1231					
1243					
1349					
1461	ISO3016	-9		1.01	
1682					
1748	D97	-12		0.07	
1833					
1877	D97	-12		0.07	
1941	ISO3016	-12		0.07	
1963	D97	-12		0.07	
1971					
	normality	suspect			
	n	25			
	outliers	1			
	mean (n)	-12.24			
	st.dev. (n)	1.480			
	R(calc.)	4.14			
	R(D97:12)	9.00			

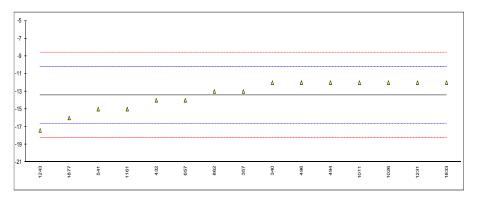


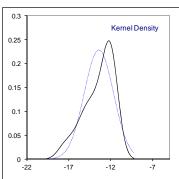


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## Determination of Pour Point automated on sample #15055; results in °C

lab	method	value	mark	z(targ)	remarks
237					
273					
311					
315					
323					
337					
340	D5950	-12		0.89	
357	D5950	-13		0.27	
369					
371					
396	B				
432	D5950	-14		-0.36	
445					
446					
485	DEOCO	40		0.00	
494	D5950	-12		0.89	
496	D5950	-12 15		0.89	
541 551	D5950	-15 		-0.98	
601					
614					
621					
657	D5950	-14		-0.36	
704	D0000				
781					
862	D5950	-13		0.27	
875					
902					
922					
963					
974					
1011		-12		0.89	
1026	D5950	-12		0.89	
1161	D6749	-15		-0.98	
1231	D5950	-12		0.89	
1243	D5950	-17.4		-2.47	
1349					
1461					
1682 1748					
	DEGEO	-12		0.89	
1833 1877	D5950 D5950	-12 -16		-1.60	
1941	D3930	-10		-1.00	
1963					
1971					
1071					
	normality	OK			
	n	15			
	outliers	0			
	mean (n)	-13.43			
	st.dev. (n)	1.745			
	R(calc.)	4.89			
	R(D5950:14)	4.50			





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## Determination of Rust prevention (proc.B) on sample #15055

lab	method	value	mark	z(targ)	remarks
237					
273					
311					
315	D665	Fails			
323	2000				
337					
340					
357					
369					
371					
396					
432					
445	D665	Fail severe			
446	D000				
485					
494					
496	D665	Fail (severe rusting)			
541	D003				
551					
601					
614					
621 657					
704					
781	Door	Carrana mratina			
862	D665	Severe rusting			
875					
902					
922	Deer	 Doos			Folio pogotivo?
963	D665	Pass			False negative?
974					
1011	Door	 			
1026	D665	Fail severe			
1161					
1231					
1243					
1349					
1461					
1682					
1748					
1833					
1877					
1941					
1963					
1971					
	reported	5 fail, 1 pass			

Base Oil: iis15L02 page 27 of 34

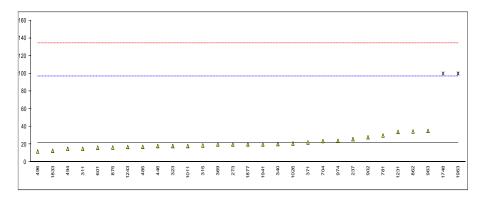
## Determination of Sulphur on sample #15055; results in mg/kg

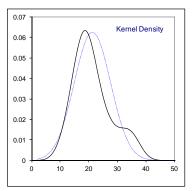
lab	method	value	mark	z(targ)	remarks
237	D4294	<20.0			
273					
311	D2622	<3			
315					
323	D2622	<3			
337					
340	D5453	<0.5			
357					
369					
371	D5453	0.21			
396					
432					
445					
446					
485					
494	ISO20846	0.3			
496	D2622	0.0			
541	D5453	<10			
551					
601					
614					
621	D4294	<20			
657	D5453	0.3	С		first reported: 0.3 %M/M
704	ISO20846	0.73			
781	D5453	<1.0			
862	D2622	<3			
875	D2622	0.7			
902					
922	D4294	<17.0			
963					
974					
1011		<60			
1026	D2622	<3			
1161	ISO8754	2203			False positive result? Possibly a unit error?
1231					
1243	D7000				
1349	D7039	0.0			
1461					
1682					
1748	DEAEO	0.007			
1833	D5453	0.987			
1877 1941					
1963					
1903					
1971					
	normality	ОК			
	n	14			
	outliers	n.a.			
	mean (n)	<3			
	st.dev. (n)	n.a.			
	R(calc.)	n.a.			
	R(D2622:10)	n.a.			Application range: 3 mg/kg – 4.6 %M/M
	(				11

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## Determination of Water on sample #15055; results in mg/kg

lab	method	value	mark	z(targ)	remarks
237	D6304	25.84		0.12	
273	D6304	20.0		-0.03	
311	D6304-A	15		-0.17	
315	D6304-C	18.7		-0.07	
323	D6304-A	18		-0.09	
337	2000.71				
340	D6304-A	20.3		-0.02	
357	2000170				
369	D6304-A	20		-0.03	
371	D6304	22.16		0.02	
396	20001				
432					
445					
446	D6304-A	18		-0.09	
485	D6304-A	17.2		-0.11	
494	D6304-B	15		-0.17	
496	D6304-C	12		-0.24	
541	2000.0				
551					
601	D6304	16.2		-0.13	
614	20001				
621					
657					
704	D6304	23.7		0.07	
781	D6304-A	30		0.23	
862	D6304-C	34.6		0.35	
875	D6304-A	16.507		-0.13	
902	D6304-A	28		0.18	
922	D6304	<10.0			
963	D6304-A	35.2		0.37	
974	D6304-A	24		0.07	
1011	D6304-A	18		-0.09	
1026	D6304-C	21		-0.01	
1161					
1231	D6304-A	34		0.34	
1243	D6304	17		-0.11	
1349					
1461					
1682					
1748	D1744	100	R(0.01)	2.09	
1833	D6304-A	12.7421	. ,	-0.22	
1877	D6304-C	20		-0.03	
1941	D6304	20		-0.03	
1963	D6304-C	100	R(0.01)	2.09	
1971					
	normality	OK			
	n	27			
	outliers	2			
	mean (n)	21.23			
	st.dev. (n)	6.376			
	R(calc.)	17.85			
	R(D6304:07)	105.64			





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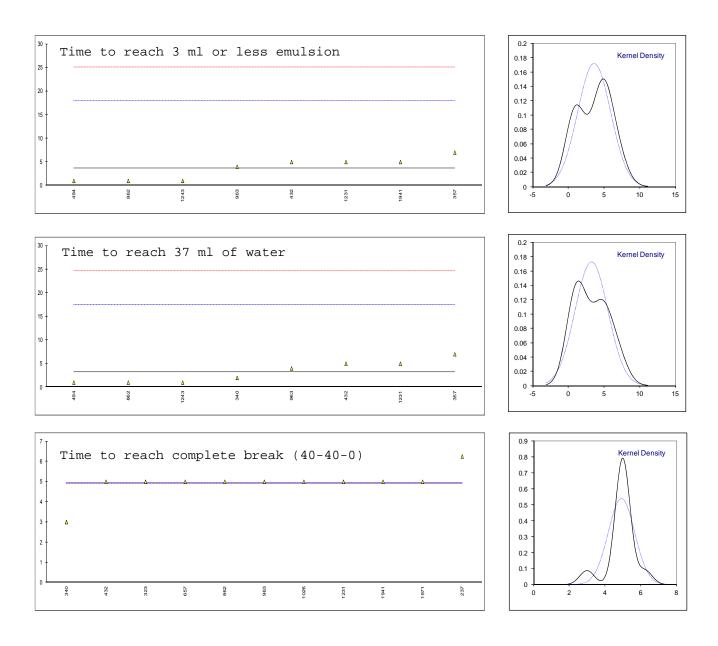
## Determination of Water Separability at 54°C on sample #15055; results in minutes

						time to reach		
		time to reach 3 ml		time to reach		complete break (40-		time test
lab	method	or less emulsion	z(targ)	37 ml of water	z(targ)	40-0)	z(targ)	aborted
237						6.25		
273								
311								
315								
323						5		NO
337								
340				2	-0.18	3		
357	D1401	7	0.47	7	0.53			YES
369								
371								
396								
432	D1401	5	0.19	5	0.25	5		NO
445	D1401	<5		<5		<5		NO
446								
485								
494	D1401	1	-0.37	1	-0.32	<5		NO
496								
541								
551								
601								
614								
621								
657	D1401	<5		<5		5		NO
704								
781								
862	D1401	1	-0.37	1	-0.32	5		
875								
902								
922								
963	D1401	4.0	0.05	4.0	0.11	5		NO
974								
1011								
1026						5		
1161								
1231	D1401	5	0.19	5	0.25	5		NO
1243	D1401	1.0	-0.37	1.0	-0.32			
1349								
1461								
1682								
1748						<5		
1833								
1877	5							
1941	D1401	5	0.19	<5		5		YES
1963								
1971						5		
	normality	unknown		unknown				
	n	8		8				
	outliers	0		0				

normality unknown n 8 outliers 0 mean (n) 3.63 st.dev. (n) 2.326 R(calc.) 6.51 R(D1401:12) 20.00

unknown 8 0 3.25 2.315 6.48 20.00

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## Determination of Water Separability at 54°C sample #15055; results in ml

lab	method	volume oil phase	volume water phase	volume emulsion phase	reported
237					
273					
311					
315					
323		40	40	0	
337					
340		40.0	40.0	0.0	
357	D1401	40	39	1	
369					
371					
396	D4.404	40	40		
432 445	D1401 D1401	40	40	0	
445 446	D1401	40	40 	0	
485					
494	D1401	40	40	0	
496	D1401				
541					
551					
601					
614					
621					
657	D1401				
704					
781					
862	D1401	40	40	0	40-40-0 (5 min)
875					
902					
922					
963	D1401	40	40	0	
974					
1011					
1026					
1161	D4.404	40	40		
1231	D1401	40	40	0	
1243	D1401				
1349 1461					
1682					
1748					
1833					
1877				<del></del>	
1941	D1401	40	40	0	
1963	21101				
1971					

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#### **APPENDIX 2**

## Number of participants per country

- 1 lab in ALGERIA
- 1 lab in ARGENTINA
- 1 lab in AUSTRALIA
- 1 lab in AUSTRIA
- 2 labs in BELGIUM
- 1 lab in BRAZIL
- 1 lab in BULGARIA
- 1 lab in CHINA, People's Republic
- 1 lab in CROATIA
- 1 lab in FINLAND
- 2 labs in FRANCE
- 3 labs in GERMANY
- 1 lab in INDONESIA
- 1 lab in ITALY
- 1 lab in JORDAN
- 2 labs in LATVIA
- 1 lab in MALAYSIA
- 3 labs in NETHERLANDS
- 1 lab in NIGERIA
- 1 lab in PAKISTAN
- 2 labs in POLAND
- 1 lab in PORTUGAL
- 2 labs in RUSSIAN FEDERATION
- 1 lab in SAUDI ARABIA
- 1 lab in SERBIA
- 1 lab in SINGAPORE
- 1 lab in SOUTH AFRICA
- 1 lab in THAILAND
- 3 labs in TURKEY
- 1 lab in UKRAINE
- 1 lab in UNITED ARAB EMIRATES
- 3 labs in UNITED KINGDOM

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#### **APPENDIX 3**

#### Abbreviations:

C = final result after checking of first reported suspect result

 $\begin{array}{ll} D(0.01) &= \text{outlier in Dixon's outlier test} \\ D(0.05) &= \text{straggler in Dixon's outlier test} \\ G(0.01) &= \text{outlier in Grubbs' outlier test} \\ G(0.05) &= \text{straggler in Grubbs' outlier test} \\ DG(0.01) &= \text{outlier in Double Grubbs' outlier test} \\ DG(0.05) &= \text{straggler in Double Grubbs' outlier test} \\ \end{array}$ 

R(0.01) = outlier in Rosner outlier test
R(0.05) = straggler in Rosner outlier test
ex = excluded from calculations
U = reported in different unit

W = result withdrawn on request of the participants

fr. = first reported

S = scope of the reported method is not applicable

n.a. = not applicablen.e. = not evaluated

SDS = Material Safety Data Sheet

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