Results of Proficiency Test **Natural Gas Analysis** March 2012

Institute for Interlaboratory Studies Spijkenisse, the Netherlands Organised by:

dr. R.G. Visser

mr. I. Kooren & ing. R. Starink

Author: Corrector: Report: Report: iis12S01M

June 2012

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1 Introduction

A first proficiency study for natural gas (composition only) was organised by its in 2009. Afterwards the opinion of the participating laboratories was inventarised. Most participants were very positive and therefore it was decided to repeat the PT annually.

Because iis has limited gas-handling facilities in place to prepare gas samples, a cooperation with EffecTech (Uttoxeter, United Kingdom) was set up. This company is fully equipped and has experience in the preparation of synthetic natural gas samples for PT purposes. EffecTech maintains an ISO17043 accreditation for the preparation of PT samples in homogeneous and stable batches and an ISO17025 accreditation for the calibration and assignment of reference values for these samples.

In this interlaboratory study 36 laboratories from 23 different countries participated. See appendix 3 for the number of participants in per country.

In this report the results of the proficiency test on natural gas are presented and discussed.

2 SET UP

The Institute for Interlaboratory Studies (iis) in Spijkenisse, the Netherlands, was the organizer of this proficiency test.

To optimise the costs for the participating laboratories, it was decided to prepare one natural gas mixture. Samples were divided over a batch of 40 cylinders. The cylinder size is a cost-effective one-litre cylinder. Each cylinder was uniquely numbered. The limited cylinder size is chosen to optimise transport and handling costs.

Participants were requested to report rounded and unrounded results. The unrounded results were preferably used for statistical evaluation.

2.1 QUALITY SYSTEM

The Institute for Interlaboratory Studies in Spijkenisse, the Netherlands, has implemented a quality system based on ISO17043:2010 and ILAC-G13:2007. This ensures strict adherence to protocols for sample preparation and statistical evaluation and 100% confidentially of participant's data. Also customer's satisfaction is measured on regular basis by the distribution of questionnaires.

EffecTech is an accredited provider of proficiency testing schemes under the requirements of ISO/IEC17043:2010 by UKAS (no. 4719).

2.2 PROTOCOL

The protocol followed in the organisation of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of January 2010 (iis-protocol, version 3.2).

2.3 CONFIDENTIALITY STATEMENT

All data present in this report must be regarded as confidential and for use by the participating companies only. Disclosure of the information in this report is only allowed by means of the entire report. Use of the contents of this report for third parties is only allowed by written permission of the Institute for Interlaboratory Studies. Disclosure of the identity of one or more of the participating companies will be done only after receipt of a written agreement of the companies involved.

2.4 SAMPLES

In this proficiency test only one sample was used. A batch of one litre cylinders with artificial natural gas mixture was prepared and tested for homogeneity by EffecTech (Uttoxeter, United Kingdom) in conformance with ISO Guide 35: 2006 and ISO/IEC17043:2010. One batch of 40 cylinders was prepared (job 11/703) starting March 1, 2012. Each cylinder was uniquely numbered. Every cylinder in the batch was analysed using ten replicate measurements. The within bottle and between bottle variations were then assessed in accordance with ISO Guide 35:2006 (Annex A.1). This procedure showed that the between bottle variations were all small compared to the uncertainties on the reference values on each component. Hence, a single reference value could be safely assigned to the entire batch of samples.

The repeatability values (r) were calculated per component by multiplication of the respective standard deviation by 2.8. Subsequently, the calculated repeatabilities were compared with 0.3 times the reproducibility of the reference method in agreement with the procedure of ISO 13528, Annex B2 in the next table:

Parameter	r (abs, observed) in %mol/mol	0.3xR (abs, ISO6974-3) in %mol/lmol
Ethane	0.0038	0.0607
Propane	0.0014	0.0095
n-Butane	0.0009	0.0047
iso-Butane	0.0008	0.0062
Carbon dioxide	0.0024	0.0330
Nitrogen	0.0029	0.0118

Table 1: evaluation of homogeneity test results against ISO6974-3 requirements

From the above table it is clear that all observed repeatability values are far less than 0.3 times the respective reproducibility of the reference method ISO6974-3. Therefore, the homogeneity of the prepared cylinders was assumed.

To each of the participating laboratories one 1L gas cylinder was sent on March 16, 2012.

2.5 STABILITY OF THE SAMPLES

EffecTech (Uttoxeter, United Kingdom) declares that the prepared gas cylinders have a shelf life of at least 6 months. This is sufficient for the proficiency testing purposes.

2.6 ANALYSES

The participants were asked to determine: Methane, Ethane, Propane, n-Butane, iso-Butane, Carbon dioxide, Nitrogen, Caloric Value (sup), Density, Relative Density and Wobbe index. Also some method details were requested to be reported.

To get comparable results a detailed report form, on which the units were prescribed and a letter of instructions were prepared and made available for download on the iis website. A SDS and a form to confirm receipt of the samples were added to the sample package.

3 RESULTS

During four weeks after sample despatch, the results of the individual laboratories were gathered. The original results are tabulated per determination in the appendix 1 of this report. The laboratories are presented by their code numbers.

Directly after the deadline the available results were screened for suspect data. A result was called suspect in case the Huber Elimination Rule (a robust outlier test) found it to be an outlier. The laboratories that produced these suspect data were asked to check the results. Additional or corrected data are put under 'Remarks' in the result tables in appendix 1. Results that came in after deadline were not taken into account in the screening for suspect data and thus these participants were not requested for checks.

3.1 STATISTICS

The protocol followed in the organisation of this proficiency test was the one as described for proficiency testing in the report 'iis Interlaboratory Studies: Protocol for the Organisation, Statistics and Evaluation' of January 2010 (iis-protocol, version 3.2).

For the statistical evaluation the *unrounded* (when available) figures were used instead of the rounded results. Results reported as '<...' or '>...' were not used in the statistical evaluation.

First the normality of the distribution of the various data sets per determination was checked by means of the Lilliefors-test. After removal of outliers this check was repeated. In case a data set does not have a normal distribution, the results of the statistical evaluation should be used with due care.

In accordance with ISO 5725 (1986 and 1994) the original results per determination were submitted subsequently to Dixon and Grubbs outlier tests. Outliers are marked by D(0.01) for the Dixon test and by D(0.01) for the Grubbs test. Stragglers are marked by D(0.05) for the Dixon test and by D(0.05) for the Grubbs test. Both outliers and stragglers were not included in the calculations of the averages and the standard deviations.

For each assigned value, the uncertainty was determined in accordance with ISO13528. Subsequently the calculated uncertainty was evaluated against the respective requirement based on the target reproducibility in accordance with ISO13528. When the uncertainty passed the evaluation, no remarks are made in the report. However, when the uncertainty

failed the evaluation it is mentioned in the report and it will have consequences for the evaluation of the test results.

Finally the reproducibilities were calculated from the standard deviations by multiplying these with a factor of 2.8.

3.2 GRAPHICS

In order to visualise the data against the reproducibilities from literature, Gauss plots were made, using the sorted data for one determination (see appendix 1). On the Y-axis the reported analysis results are plotted. The corresponding laboratory numbers are under the X-axis.

The straight horizontal line presents the consensus value (a trimmed mean). The four striped lines, parallel to the consensus value line, are the +3s, +2s, -2s and -3s target reproducibility limits of the selected standard. Outliers and other data, which were excluded from the calculations, are represented as a cross. Accepted data are represented as a triangle. Furthermore, Kernel Density Graphs were made. This is a method for producing a smooth density approximation to a set of data that avoids some problems associated with histograms. (see appendix 3; nr.13 and 14).

3.3 Z-SCORES

To evaluate the performance of the participating laboratories the z-scores were calculated. As it was decided to evaluate the performance of the participants in this proficiency test (PT) against the literature requirements, e.g. ASTM reproducibilities, the z-scores were calculated using a target standard deviation. This target standard deviation was calculated from the literature reproducibility by division with 2.8.

When a laboratory did use a test method with a reproducibility that is significantly different from the reproducibility of the reference test method used in this report, it is strongly advised to recalculate the z-score, while using the reproducibility of the actual test method used, this in order to evaluate the fit-for-useness of the reported test result.

The z-scores were calculated according to:

```
z(target) = (result - average of PT) / target standard deviation
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The z(target) scores are listed in the result tables in appendix 1.

Absolute values for z<2 are very common and absolute values for z>3 are very rare.

Therefore the usual interpretation of z-scores is as follows:

|z| < 1 good 1 < |z| < 2 satisfactory 2 < |z| < 3 questionable 3 < |z| unsatisfactory

4 EVALUATION

In this proficiency test several problems were encountered with customs clearance. In total eleven laboratories reported results after the final reporting date and two participants were not able to report any test results. In total 34 participants reported 475 numerical results. Observed were 23 outlying results, which is 4.8% of the numerical results. In proficiency studies outlier percentages of 3% - 7.5% are quite normal.

4.1 EVALUATION PER TEST/COMPONENT

In this section the results are discussed per component. The methods, that were used by the participating laboratories, were taken into account for explaining the observed differences when possible and applicable. These methods are also in the tables together with the original data. The abbreviations, used in these tables, are listed in appendix 3. Not all original data sets proved to have a normal distribution. Non-Gaussian distributions were found for iso-butane. The statistical evaluation of this component should be used with due care, see also paragraph 4.4.

All test results reported by laboratory 602 were deviating, influenced by the very low ethane, n-butane and i-butane results and the very high nitrogen results. Four of the seven test results appeared to be statistical outliers. As the seven test results are not independent, it was decided not to use any of the test results of this laboratory for the statistical evaluation.

Methane: The determination of this component is very problematic. Only one

statistical outlier was detected. However, the calculated reproducibility after exclusion of the statistical outlier, is not at all in agreement with the

requirements of ISO6974-3:2000, nor with ASTM D1945:2003.

Ethane: The determination of this component was problematic. Only one

statistical outlier was detected. The calculated reproducibility after exclusion of the statistical outlier, is not in agreement with the

requirements of ISO6974-3:2000, nor with ASTM D1945:2003.

<u>Propane</u>: The determination of this component may be problematic for a number

of participating laboratories, depending on the test method used by the

laboratory. Only one statistical outlier was detected.

The calculated reproducibility after exclusion of the statistical outlier, is not in agreement with the strict requirements of ISO6974-3:2000.

However, the calculated reproducibility is in full agreement with the

requirements of and ASTM D1945:2003.

<u>n-Butane</u>: The determination of this component may be problematic for a number

of participating laboratories, depending on the test method used by the

laboratory.

Two statistical outliers were detected. The calculated reproducibility after

exclusion of the statistical outliers, is not in agreement with the strict

requirements of ISO6974-3:2000. However, the calculated

reproducibility is in full agreement with the requirements of and ASTM D1945:2003.

<u>i-Butane</u>:

The determination of this component may be problematic for a number of participating laboratories, depending on the test method used by the laboratory.

Only one statistical outlier was detected. The calculated reproducibility is not in agreement with the strict requirements of ISO6974-3:2000. However, the calculated reproducibility is in full agreement with the requirements of and ASTM D1945:2003.

Carbon Dioxide:

The determination of this component may be problematic for a number of participating laboratories, depending on the test method used by the laboratory.

Two statistical outliers were detected. The calculated reproducibility after exclusion of the statistical outliers, is not in agreement with the strict requirements of ISO6974-3:2000. However, the calculated reproducibility is in full agreement with the requirements of and ASTM D1945:2003.

Nitrogen:

The determination of this component is very problematic. Two statistical outliers were detected and the calculated reproducibility after exclusion of the statistical outliers, is not at all in agreement with the requirements of ISO6974-3:2000, nor with ASTM D1945:2003.

<u>Calculated parameters, general remark:</u> In this PT the calculated parameters were reported

for two combustion temperatures (15 and 25°C) as well as for real and ideal gas. This because it had become clear in the previous rounds that the laboratories reported a mix of these results. The reported test results varied over a large range and the results showed bimodal distributions for caloric value, density and Wobbe index.

From the reported test results may be concluded that the majority of the laboratories prefer to report these parameters for real gas, 101.325 kPa and a combustion temperature of 25°C.

Caloric Value:

This time no bimodal distributions are visible and the spreads of the four groups of test results are all much smaller than previously observed: less than 10% of the spread in iis11S01M. However, still a number of laboratories did report results that deviate from the theoretical results, possibly due to calculation errors. These results were excluded from the statistical calculations. One laboratory did report the result for real gas under ideal gas. This was corrected before the statistical calculations.

Density:

This time no bimodal distributions are visible and the spreads of the four groups of test results are all much smaller than previously observed: less than 5% of the spread in iis11S01M.

Relative density: The spreads of the four groups of test results are only little smaller than

the spread observed in the previous PT iis11S01M. However, two laboratories did report results that deviate from the theoretical results, possibly due to calculation errors, and therefore these results were not

used for the statistical calculations.

Wobbe index: This time no bimodal distributions are visible and the spreads of the four

groups of test results are all much smaller than previously observed: less than 5 - 10% of the spread in iis11S01M. However, still a number of laboratories did report results that deviate from the theoretical results,

possibly due to calculation errors.

4.2 Performance evaluation for the group of Laboratories

The average results per component, observed reproducibilities and target reproducibilities, derived from the standard methods ISO 6974-3 and ASTM D1945 are compared in the next table.

	unit	n	cons. value	2.8 * sd	R(ISO6974-3)	R(D1945)
Methane	%mol/mol	32	86.559	0.321	0.173	0.150
Ethane	%mol/mol	33	6.814	0.265	0.204	0.100
Propane	%mol/mol	32	1.061	0.059	0.032	0.100
n-Butane	%mol/mol	32	0.261	0.020	0.016	0.070
iso-Butane	%mol/mol	33	0.349	0.029	0.021	0.070
Carbon dioxide	%mol/mol	31	1.324	0.066	0.040	0.100
Nitrogen	%mol/mol	32	3.643	0.344	0.109	0.100

Table 2: Performance of the group in comparison with the target reproducibilities

Without further statistical calculations it can be concluded that for several components there is not a good compliance of the group of participating laboratories with the relevant standard. The problematic components have been discussed in paragraph 4.1.

4.3 COMPARISON OF THE PROFICIENCY TEST OF APRIL 2012 WITH PREVIOUS PTS

	2012	2011	2010	2009
Number of reporting labs	34	33	29	39
Number of results reported	475	330	280	381
Statistical outliers	23	16	25	30
Percentage outliers	4.8%	4.8%	8.9%	7.9%

Table 3: Comparison with previous proficiency tests

In proficiency tests outlier percentages of 3% - 7.5% are quite normal.

The performances of the determinations in the proficiency tests for NG were compared against the requirements of the two often used standard test methods. See the overview in the following table:

	2012 ISO6974-3	2012 D1945	2011 ISO6974-3	2011 D1945	2010 ISO6974-3	2010 D1945
Methane						
Ethane		++	++	++	++	
Propane	-	++	-	+/-	-	+
n-Butane - ++		-	++	+/-	++	
iso-Butane - ++		++	-	++	+/-	++
Carbon dioxide		++	-	++	-	-
Nitrogen				-		

Table 4: comparison of observed precision with precision of ISO6974-3 / ASTM D1945

From the above table it is clear that the performance of the group of participating laboratories did not improve yet. The following performance categories were used:

- ++: group performed much better than the standard
- + : group performed better than the standard
- +/-: group performance equals the standard
- : group performed worse than the standard
- -- : group performed much worse than the standard

4.4 DISCUSSION

Many of the observed reproducibilities are larger than the reproducibility requirements of ISO6974-3 and therefore it had to be concluded that no improvement was observed since the 2010 PT for Natural Gas and that the determination of the composition of Natural Gas was still problematic for a significant number of participating laboratories.

The consensus values as determined in this PT are compared with the average values from the homogeneity testing by the supplier EffecTech in the following table.

Parameter	Average values by EffecTech in %mol/mol	Consensus values from participants results in %mol/mol	Absolute differences in %mol/mol
Methane	86.619	86.559	-0.060
Ethane	6.747	6.814	+0.067
Propane	1.051	1.061	+0.010
n-Butane	0.260	0.261	+0.001
iso-Butane	0.344	0.349	+0.005
Carbon dioxide	1.314	1.324	+0.010
Nitrogen	3.665	3.643	-0.022

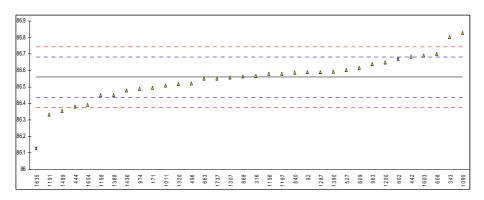
Table 5: comparison of consensus values with values determined by the supplier EffecTech

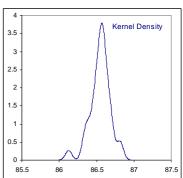
From the comparison in table 5 it is clear that the consensus values as determined in this PT are all very well in line with the values as determined during the preparation of the gas cylinders.

APPENDIX 1

Determination of Methane on sample #12040; results in %mol/mol

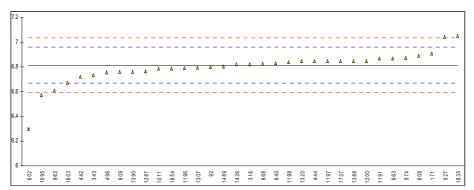
lab	method	value	mark	z(targ)	remarks
92	GPA2286	86.59		0.50	
171	D1945	86.495		-1.04	
316	ISO6974	86.569		0.16	
343	CEA1624	86.802	С	3.93	first reported 86.244
442	D1945	86.6844		2.02	
444	D1945	86.381		-2.88	
496	EN15984	86.521		-0.62	
527	D1945	86.603		0.71	
602	GPA2261	86.6694	ex	1.78	see §4.1
608	GPA2286	86.702	С	2.31	first reported 86.668
609	GPA2261	86.615	С	0.90	first reported 86.796
663	D1945	86.550		-0.15	
840	D1945	86.5858		0.43	
868	GPA2261	86.563		0.06	
963	D1945	86.640	_	1.31	
974	ISO6974	86.490	С	-1.12	first reported 86.990
1011	UOP539	86.508		-0.83	
1081	LIODEGO			4.05	
1095	UOP539	86.828		4.35	
1191	UOP539	86.334		-3.64	
1196 1197	GPA2261	86.579 86.582		0.32 0.37	
1197	D1945 D1945	86.449		-1.78	
1200	UOP539	86.65		1.47	
1200	ISO6974	86.591		0.51	
1307	Fast RGA	86.556		-0.05	
1320	ISO6974	86.518		-0.67	
1388	GPA2261	86.449		-1.78	
1390	in house	86.593		0.54	
1436	ISO6974	86.479		-1.30	
1489	ISO6974	86.355	С	-3.30	first reported 86.391
1603	in house	86.6929	_	2.16	
1622					
1635	D1945	86.127	G(0.05)	-6.99	
1654	D1945	86.392	c` ´	-2.71	first reported 86.430
1737	in house	86.551		-0.13	•
	normality	OK			
	n	32			
	outliers	1			
	mean (n)	86.5593			
	st.dev. (n)	0.11465			
	R(calc.)	0.3210			
	R(ISO6974-3)	0.1731			Compare R(ASTM D1945) = 0.150

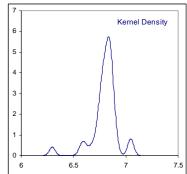




Determination of Ethane on sample #12040; results in %mol/mol

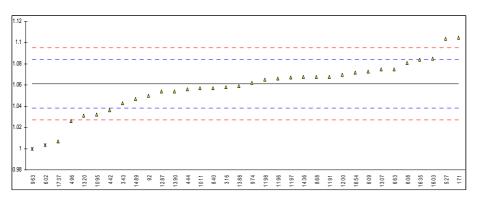
92 GPA2286 6.80 -0.19 171 D1945 6.907 1.27 316 ISO6974 6.822 0.11 343 CEA1624 6.736 -1.07 442 D1945 6.7212 -1.27 444 D1945 6.848 0.46 496 EN15984 6.757 -0.78 527 D1945 7.042 3.12 602 GPA2261 6.2960 G(0.01) -7.10 608 GPA2286 6.892 C 1.07 first reported 6.890 609 GPA2261 6.759 C -0.75 663 D1945 6.870 0.77 840 D1945 6.8325 0.25 868 GPA2261 6.827 0.18 963 D1945 6.6327 0.18 963 D1945 6.610 -2.80 974 ISO6974 6.875 0.83 1011 UOP539 6.787 -0.37 1081 1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25 1320 ISO6974 6.846 0.44
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496 EN15984 6.757 -0.78 527 D1945 7.042 3.12 602 GPA2261 6.2960 G(0.01) -7.10 608 GPA2286 6.892 C 1.07 first reported 6.890 609 GPA2261 6.759 C -0.75 first reported 6.590 663 D1945 6.870 0.77 840 D1945 6.8325 0.25 868 GPA2261 6.827 0.18 963 D1945 6.610 -2.80 974 ISO6974 6.875 0.83 1011 UOP539 6.787 -0.37 1081
527 D1945 7.042 3.12 602 GPA2261 6.2960 G(0.01) -7.10 608 GPA2286 6.892 C 1.07 first reported 6.890 609 GPA2261 6.759 C -0.75 first reported 6.590 663 D1945 6.870 0.77 840 D1945 6.8325 0.25 868 GPA2261 6.827 0.18 963 D1945 6.610 -2.80 974 ISO6974 6.875 0.83 1011 UOP539 6.787 -0.37 1081 1095 1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
602 GPA2261 6.2960 G(0.01) -7.10 608 GPA2286 6.892 C 1.07 first reported 6.890 609 GPA2261 6.759 C -0.75 first reported 6.590 663 D1945 6.870 0.77 840 D1945 6.8325 0.25 868 GPA2261 6.827 0.18 963 D1945 6.610 -2.80 974 ISO6974 6.875 0.83 1011 UOP539 6.787 -0.37 1081
608 GPA2286 6.892 C 1.07 first reported 6.890 609 GPA2261 6.759 C -0.75 first reported 6.590 663 D1945 6.870 0.77 840 D1945 6.8325 0.25 868 GPA2261 6.827 0.18 963 D1945 6.610 -2.80 974 ISO6974 6.875 0.83 1011 UOP539 6.787 -0.37 1081 1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
609 GPA2261 6.759 C -0.75 first reported 6.590 663 D1945 6.870 0.77 840 D1945 6.8325 0.25 868 GPA2261 6.827 0.18 963 D1945 6.610 -2.80 974 ISO6974 6.875 0.83 1011 UOP539 6.787 -0.37 1081 1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
663 D1945 6.870 0.77 840 D1945 6.8325 0.25 868 GPA2261 6.827 0.18 963 D1945 6.610 -2.80 974 ISO6974 6.875 0.83 1011 UOP539 6.787 -0.37 1081 1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
840 D1945 6.8325 0.25 868 GPA2261 6.827 0.18 963 D1945 6.610 -2.80 974 ISO6974 6.875 0.83 1011 UOP539 6.787 -0.37 1081 1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
868 GPA2261 6.827 0.18 963 D1945 6.610 -2.80 974 ISO6974 6.875 0.83 1011 UOP539 6.787 -0.37 1081 1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
963 D1945 6.610 -2.80 974 ISO6974 6.875 0.83 1011 UOP539 6.787 -0.37 1081 1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
974 ISO6974 6.875 0.83 1011 UOP539 6.787 -0.37 1081 1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
1011 UOP539 6.787 -0.37 1081 1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
1081 1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
1095 UOP539 6.575 -3.27 1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
1191 UOP539 6.868 0.74 1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
1196 GPA2261 6.791 -0.32 1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
1197 D1945 6.848 0.46 1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
1198 D1945 6.837 0.31 1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
1200 UOP539 6.85 0.49 1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
1287 ISO6974 6.767 -0.64 1307 Fast RGA 6.796 -0.25
1307 Fast RGA 6.796 -0.25
1320 1300974 0.040 0.44
1388 GPA2261 6.849 0.48
1390 in house 6.763 -0.70
1622 1625 D1045 7.052 2.26
1635 D1945 7.052 3.26
1654 D1945 6.789 C -0.34 first reported 6.791
1737 in house 6.849 0.48
normality OK
n 33
outliers 1
mean (n) 6.8141
st.dev. (n) 0.09479
R(calc.) 0.2654
R(ISO6974-3) 0.2044 Compare R(ASTM D1945) = 0.100
1(10-003/4-0) 0.2044 Collipate 1(A01W D1340) = 0.100

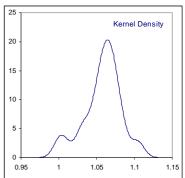




Determination of Propane on sample #12040; results in %mol/mol

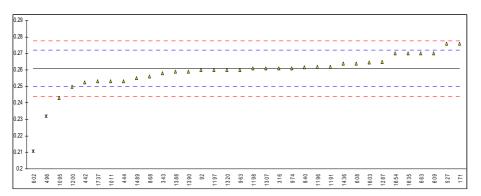
lab	method	value	mark	z(targ)	remarks
92	GPA2286	1.05		-0.98	
171	D1945	1.105		3.86	
316	ISO6974	1.058		-0.27	
343	CEA1624	1.043		-1.59	
442	D1945	1.0365		-2.17	
444	D1945	1.056		-0.45	
496	EN15984	1.026		-3.09	
527	D1945	1.104		3.77	
602	GPA2261	1.0031	ex	-5.10	see §4.1
608	GPA2286	1.081		1.75	
609	GPA2261	1.073	С	1.05	first reported 1.071
663	D1945	1.075		1.22	
840	D1945	1.0573		-0.34	
868	GPA2261	1.068		0.61	
963	D1945	1.000	D(0.05)	-5.38	
974	ISO6974	1.062		0.08	
1011	UOP539	1.057		-0.36	
1081					
1095	UOP539	1.032		-2.56	
1191	UOP539	1.068		0.61	
1196	GPA2261	1.066		0.43	
1197	D1945	1.067		0.52	
1198	D1945	1.065		0.34	
1200	UOP539	1.07		0.78	
1287	ISO6974	1.054		-0.63	
1307	Fast RGA	1.075		1.22	
1320	ISO6974	1.031		-2.65	
1388	GPA2261	1.059		-0.19	
1390	in house	1.054		-0.63	
1436	ISO6974	1.068		0.61	
1489	ISO6974	1.047	С	-1.24	first reported 1.048
1603	in house	1.0849		2.09	
1622					
1635	D1945	1.084	_	2.01	
1654	D1945	1.072	С	0.96	first reported 1.073
1737	in house	1.007		-4.76	
	normality	OK			
	normality	OK 32			
	n outliers	32 1			
	mean (n)	1.0611			
	st.dev. (n)	0.020897			
	R(calc.)	0.020037			
	R(ISO6974-3)	0.0303			Compare R(ASTM D1945) = 0.100
	11(1000017-0)	0.0010			Compare 11/10 11/10 10 10-10/

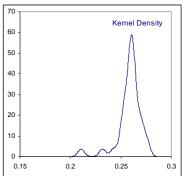




Determination of n-Butane on sample #12040; results in %mol/mol

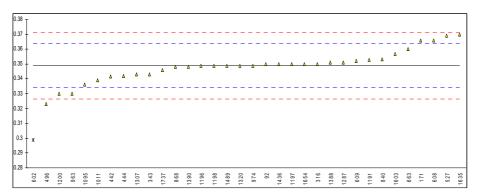
lab	method	value	mark	z(targ)	remarks
92	GPA2286	0.26		-0.17	
171	D1945	0.276		2.69	
316	ISO6974	0.261		0.01	
343	CEA1624	0.258		-0.53	
442	D1945	0.2525		-1.51	
444	D1945	0.253		-1.42	
496	EN15984	0.232	G(0.05)	-5.18	
527	D1945	0.276	, ,	2.69	
602	GPA2261	0.2107	G(0.01)	-8.99	
608	GPA2286	0.264	, ,	0.54	
609	GPA2261	0.270		1.62	
663	D1945	0.270		1.62	
840	D1945	0.2615		0.10	
868	GPA2261	0.256		-0.89	
963	D1945	0.260		-0.17	
974	ISO6974	0.261		0.01	
1011	UOP539	0.253		-1.42	
1081					
1095	UOP539	0.243		-3.21	
1191	UOP539	0.262		0.19	
1196	GPA2261	0.262		0.19	
1197	D1945	0.260		-0.17	
1198	D1945	0.261		0.01	
1200	UOP539	0.25		-1.96	
1287	ISO6974	0.265		0.72	
1307	Fast RGA	0.261		0.01	
1320	ISO6974	0.260		-0.17	
1388	GPA2261	0.259		-0.35	
1390	in house	0.259		-0.35	
1436	ISO6974	0.264		0.54	
1489	ISO6974	0.255	С	-1.06	first reported 0.236
1603	in house	0.2645		0.63	
1622					
1635	D1945	0.270		1.62	
1654	D1945	0.270	С	1.62	first reported 0.271
1737	in house	0.253		-1.42	
	normality	OK			
	n	32			
	outliers	2			
	mean (n)	0.2610			
	st.dev. (n)	0.00722			
	R(calc.)	0.0202			
	R(ISO6974-3)	0.0157			Compare R(ASTM D1945) = 0.070

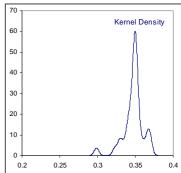




Determination of iso-Butane on sample #12040; results in %mol/mol

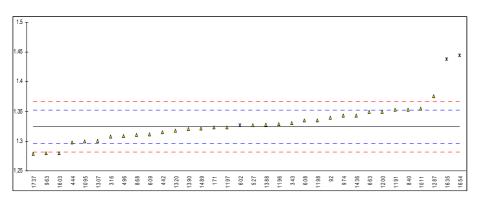
lab	method	value	mark	z(targ)	remarks
92	GPA2286	0.35		0.15	
171	D1945	0.366		2.29	
316	ISO6974	0.350		0.15	
343	CEA1624	0.343		-0.79	
442	D1945	0.3415		-0.99	
444	D1945	0.342		-0.92	
496	EN15984	0.323		-3.46	
527	D1945	0.369		2.69	
602	GPA2261	0.2987	G(0.01)	-6.71	
608	GPA2286	0.366	, ,	2.29	
609	GPA2261	0.352		0.42	
663	D1945	0.360		1.49	
840	D1945	0.3533		0.59	
868	GPA2261	0.348		-0.12	
963	D1945	0.330		-2.52	
974	ISO6974	0.349		0.02	
1011	UOP539	0.339		-1.32	
1081					
1095	UOP539	0.336		-1.72	
1191	UOP539	0.353		0.55	
1196	GPA2261	0.349		0.02	
1197	D1945	0.350		0.15	
1198	D1945	0.349		0.02	
1200	UOP539	0.33		-2.52	
1287	ISO6974	0.351		0.28	
1307	Fast RGA	0.343		-0.79	
1320	ISO6974	0.349		0.02	
1388	GPA2261	0.351		0.28	
1390	in house	0.348		-0.12	
1436	ISO6974	0.350		0.15	
1489	ISO6974	0.349	С	0.02	first reported 0.326
1603	in house	0.3569		1.07	•
1622					
1635	D1945	0.370		2.83	
1654	D1945	0.350		0.15	
1737	in house	0.346		-0.38	
	normality	not OK			
	n	33			
	outliers	1			
	mean (n)	0.3489			
	st.dev. (n)	0.01048			
	R(calc.)	0.0293			
	R(ISO6974-3)	0.0209			Compare R(ASTM D1945) = 0.070
	/				, ,

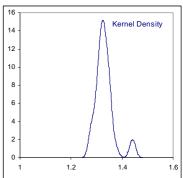




Determination of Carbon Dioxide on sample #12040; results in %mol/mol

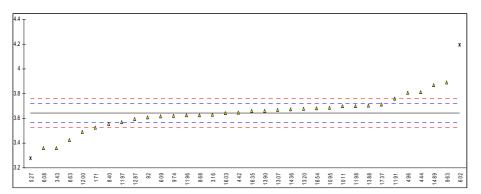
lab	method	value	mark	z(targ)	remarks
92	GPA2286	1.34		1.12	
171	D1945	1.323		-0.08	
316	ISO6974	1.308		-1.14	
343	CEA1624	1.331		0.48	
442	D1945	1.3151		-0.64	
444	D1945	1.298		-1.84	
496	EN15984	1.309		-1.07	
527	D1945	1.327		0.20	
602	GPA2261	1.3269	ex	0.19	see §4.1
608	GPA2286	1.335		0.77	•
609	GPA2261	1.312	С	-0.86	first reported 1.311
663	D1945	1.350		1.82	'
840	D1945	1.3534		2.06	
868	GPA2261	1.311		-0.93	
963	D1945	1.280		-3.11	
974	ISO6974	1.343		1.33	
1011	UOP539	1.355		2.17	
1081					
1095	UOP539	1.300		-1.70	
1191	UOP539	1.353		2.03	
1196	GPA2261	1.329		0.34	
1197	D1945	1.323		-0.08	
1198	D1945	1.335		0.77	
1200	UOP539	1.35		1.82	
1287	ISO6974	1.376		3.66	
1307	Fast RGA	1.301		-1.63	
1320	ISO6974	1.318		-0.43	
1388	GPA2261	1.328		0.27	
1390	in house	1.321		-0.22	
1436	ISO6974	1.343		1.33	
1489	ISO6974	1.322	С	-0.15	first reported 1.306
1603	in house	1.2800		-3.11	·
1622					
1635	D1945	1.438	G(0.01)	8.03	
1654	D1945	1.445	C,G(0.05)	8.52	first reported 1.397
1737	in house	1.279	. ,	-3.18	·
	normality	OK			
	n	31			
	outliers	2			
	mean (n)	1.3241			
	st.dev. (n)	0.02355			
	R(calc.)	0.02555			
	R(ISO6974-3)	0.0397			Compare R(ASTM D1945) = 0.100
	(100001 4-0)	0.0007			0011paro 11/10101 D 1010) - 0.100

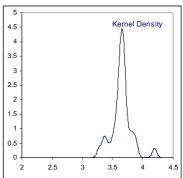




Determination of Nitrogen on sample #12040; results in %mol/mol

lab	method	value	mark	z(targ)	remarks
92	GPA2286	3.61		-0.86	
171	D1945	3.528		-2.96	
316	ISO6974	3.631		-0.32	
343	CEA1624	3.363	С	-7.18	first reported 4.044
442	D1945	3.6488		0.14	'
444	D1945	3.815		4.39	
496	EN15984	3.807		4.19	
527	D1945	3.279	G(0.05)	-9.34	
602	GPA2261	4.1952	G(0.01)	14.13	
608	GPA2286	3.360	c` ´	-7.26	first reported 3.396
609	GPA2261	3.617	С	-0.68	first reported 3.610
663	D1945	3.425		-5.60	'
840	D1945	3.5562		-2.23	
868	GPA2261	3.628		-0.40	
963	D1945	3.890		6.32	
974	ISO6974	3.620	С	-0.60	first reported 3.120
1011	UOP539	3.700		1.45	·
1081					
1095	UOP539	3.686		1.09	
1191	UOP539	3.763		3.06	
1196	GPA2261	3.624		-0.50	
1197	D1945	3.568		-1.93	
1198	D1945	3.700		1.45	
1200	UOP539	3.49		-3.93	
1287	ISO6974	3.597		-1.19	
1307	Fast RGA	3.669		0.65	
1320	ISO6974	3.678		0.89	
1388	GPA2261	3.705		1.58	
1390	in house	3.662		0.48	
1436	ISO6974	3.676		0.83	
1489	ISO6974	3.869	С	5.78	first reported 3.901
1603	in house	3.6449		0.04	
1622	_				
1635	D1945	3.660		0.42	
1654	D1945	3.684	С	1.04	first reported 3.688
1737	in house	3.715		1.83	
	normality	OK			
	n	32			
	outliers	2			
	mean (n)	3.6434			
	st.dev. (n)	0.12269			
	R(calc.)	0.3435			S
	R(ISO6974-3)	0.1093			Compare R(ASTM D1945) = 0.100





Determination of Caloric Value (sup) (101.325 kPa , comb. temp. 25°C, and metering temp 0°C) on sample #12040; results in MJ/m^3

Lab	method	real gas	mark	z(targ)	ideal gas	mark	z(targ)	remarks
92	memod		mark	<u> </u>		mark	<u> </u>	Telliares
171								
316	ISO6976	41.099			40.976			
343	CEA1624	40.9750	E,ex					calculation error?
442								
444	ISO6976	41.018			40.899			
496	DIN51857	40.971	E,ex		40.852			calculation error?
527								
602								
608								
609								
663								
840	ISO6976	41.1169			40.9972			
868	ISO6976	41.100	C(0.05)		40.980			
963	ISO6976	40.880	G(0.05)					first reported 44 442, sole arror?
974 1011	GPA2172	41.213 	C,E,ex					first reported 41.413; calc. error?
1081								
1095								
1191	ISO6976	41.045			40.932			
1196	1000370							
1197								
1198								
1200								
1287	ISO6976	41.071			40.951			
1307	-							
1320	ISO6976	41.065			40.946			
1388	ISO6976	41.070			40.951			
1390	ISO6976	41.054						
1436								
1489	ISO6976	40.980	С		40.861	С		first reported 40.929 / 40.810
1603								
1622								
1635								
1654	ISO6976	41.029	С					first reported 38.932
1737								
	normality n outliers mean (n) st.dev. (n) R(calc.) R(lit.)	OK 11 1 41.0589 0.03997 0.1119 unknown			OK 10 0 40.9345 0.04930 0.1380 unknown			
1.3 T	х х	Δ Δ	Δ Δ	٥	A A	Δ Δ	Δ	6 Kernel Density 5 - 4 - 3 - 2 - 1 -
0.5	9 4 96 3 4 3	68 4 4 60 60 60 60 60 60 60 60 60 60 60 60 60	1390	1320	13.88	316 868	8 40 9 7 4	40.6 40.8 41 41.2 4
.05 T							Δ	8 Kernel Density
95 -		Δ	Δ	Δ	Δ	Δ Δ		6 - 5 - 4 -
35 -	Δ							3 2 1 1 0
	1489	444	1320	1287	1388	316 868	840	40.6 40.8 41 41.2
	4 4	4 É	13	12	13	m &	œ eò	

Determination of Density (101.325 kPa , combustion temp. 25°C, and metering temp. 0°C) on sample #12040; results in kg/m^3

	ilipic # 120	40; results		_		_	_	<u> </u>	_
Lab	method	real gas		z(targ)	ideal gas	mark	z(targ)	remarks	
92									
171	ISO6976	0.9212			0.8188				
316 343	CEA1624	0.8213 0.8228			0.0100				
343 442	OLA 1024	0.0220							
444	ISO6976	0.8220			0.8196				
496	DIN51857	0.8210			0.8186				
527									
602									
608									
609									
663									
840	ISO6976	0.82156			0.81917				
868	ISO6976	0.8213			0.8189				
963	ISO6976	0.8197							
974	GPA2172	0.8193							
1011	D3588	0.8219			0.8175				
1081									
1095	1000070				0.0000				
1191	ISO6976	0.8229			0.8206				
1196									
1197 1198									
1200									
1287	ISO6976	0.8216							
1307	1000070	0.0210							
1320	ISO6976	0.8214			0.8190				
1388	ISO6976	0.8221			0.8197				
1390	ISO6976	0.8210							
1436									
1489	ISO6976	0.8223	С		0.8199	С		first reported 0.8214 / 0.8190	
1603								·	
1622									
1635									
1654	ISO6976	0.7543	C ,G(0.01)					first reported 0.7535	
1737									
	normality n outliers mean (n) st.dev. (n) R(calc.) R(lit.)	OK 15 1 0.8215 0.00099 0.0028 unknowr	n		OK 10 0 0.8192 0.00084 0.0024 unknown				
1.824 T 1.823 -	· · · · · · · ·				<u>a</u> <u>a</u>	Δ Δ	Δ	500 450 - Kernel D 400 - 350 -	Pensity
821 -		Δ Δ	Δ Δ					300 -	
1.82								250 -	
	Δ							200 -	
119 –	-								
318 -								150 -	
								100 -	
817 -								50 -	
816		-							
1654	974	496 1390 868	316	840	1011 444	1388	343	0.8 0.81 0.82	0.83
enn		•		0.821 _T					
600		Kornel Des-it:	1						
500 -		Kernel Density		0.8205 +					
JUU -		1	1	0.82					Δ
400 -		_{{		0.8195				Δ Δ	
		-		0.819			Δ	Δ	
1		11		0.8185	Δ	Δ	-		
300 -				0.818 +					
300 -			1	0.010 T					
300 -				0.9475					
				0.8175 —	7				
				0.8175 -	1				
200 -					Δ				
200 -	0.81	0.82 0.8		0.817 - 0.8165 - 0.816	9 64	316	8 98	1350 444 840 1308	0 8 9

Determination of Relative Density (101.325 kPa , comb. temp. 25°C, and metering temp. 0°C) on sample #12040; unit less results

Lab	method	real gas	mark	z(targ)	ideal gas	mark	z(targ)	remarks
92								
171	100							
316	ISO6976	0.6352			0.6333			
343	CEA1624	0.6364						
442 444	ISO6976	0.6359			0.6343			
496	DIN51857	0.6359			0.6332	E, ex		calculation error?
527	D11401001					L, OX		calculation error:
602								
608								
609								
663	100000							
840	ISO6976	0.63543			0.63395			
868 963	ISO6976 ISO6976	0.6352 0.6343			0.6338			
974	GPA2172	0.6358	С					first reported 0.6337
1011	0.7.22		· ·					ot reported elece.
1081								
1095								
1191	ISO6976	0.6365			0.6351			
1196								
1197								
1198 1200								
1287	ISO6976	0.6355						
1307	1000010	0.0333						
1320	ISO6976	0.6353			0.6338			
1388	ISO6976	0.6358			0.6344			
1390	ISO6976	0.6350						
1436	100000							
1489	ISO6976	0.6360	С		0.6345	С		first reported 0.6353 / 0.6338
1603 1622								
1635								
1654	ISO6976	0.6370	С					first reported 0.6363
1737								
	normality n outliers mean (n) st.dev. (n) R(calc.) R(lit.)	OK 15 0 0.6356 0.00069 0.0019 unknown			OK 8 0 0.6341 0.00055 0.0015 unknown			
0.638 _T								700 _
								Kernel Density
0.637							Δ	600 -
						Δ	Δ	500 -
0.636 +				Δ	Δ Δ	Δ		
0.635 +	Δ Δ	Δ Δ Δ	Δ Δ					400 -
								300 -
0.634 -	1							
								200 -
0.633 -								100 -
0.632	390 66 63	316 868 1320	8 40	88	6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	343	10 4	0.632 0.634 0.636 0.638 0.6
	496 1390	316 868 1320	840	1388	0 4	343	1191	
0.636 T								600
							Δ	Kernel Density
0.635 -							Δ	500 -
0.634 +				Δ	Δ	Δ		400
0.004		Δ	Δ Δ)				
0.633 -	ж 🛕							300 -
0.632								200 -
- 11								
								100 - /
0.631 -								100
0.631 -								
	90 80 90 90 90 90 90 90 90 90 90 90 90 90 90	8 9 8	1320	0 40 40 40	* 89 * 97	989	19	0.632 0.634 0.636 0.638 0.6

Determination of Wobbe Index (101.325 kPa , combustion temp. 25°C, and metering temp. 0°C) on sample #12040; results in MJ/m 3

	Lab	method	real gas	mark	z(targ)	ideal gas	mark	z(targ)	remarks
	92			mank			mank		
## ISO6976	171								
42 SC68976 S1 439 E,ex S1.340 Calculation error? 43 SC68976 S1 5806 S1.4903 Calculation error? 44 SC68976 S1 5806 S1.4903 Calculation error? 45 SC68976 S1 5806 S1.478 Calculation error? 46 SC68976 S1 5806 S1.478 Calculation error? 47 SC69976 S1 5806 S1.478 Calculation error? 48 SC68976 S1 5806 S1.478 Calculation error? 49 SC68976 S1 5806 S1.478 Calculation error? 40 SC68976 S1 5806 S1.478 Calculation error? 41 SC68976 S1 5806 S1.478 S1.48 S1.4	316			0.0/0.55					Continue and Att 070
44 ISO6976 51.439	343	CEA1624		C ,G(0.01)					first reported 14.270
SOB976 S1.448 S1.363 S1.363 S1.36976 S1.5148 S1.363 S1.36976 S1.521 S1.321 S1.32	442 444	ISO6976							
27	496			E,ex					calculation error?
08 SC08976 51.5806 51.4903	527			•					
98	602								
33 Sco6976 51.5806 51.4903	608								
40 ISO6976 51,5806 — 51,4903 — 51,5808 SISO6976 51,5808 — 51,478 — 51,690 C, E, ex — — first reported 52,02, calc. error? 41 ISO6976 51,580 C, E, ex — — — first reported 52,02, calc. error? 41 ISO6976 51,448 — 51,363 — — — — — — — — — — — — — — — — — —	609								
88 ISO6976 51.568	840	ISO6976							
74 GPA2172 S1.69 C, E, ex	868								
11	963		51.33						
191 ISO6976 51.448	974	GPA2172		C, E, ex					first reported 52.02, calc. error?
95 ISO6976 51.448 51.363 97 98 98 97 98 ISO6976 51.521 99 ISO6976 51.506 51.416 90 ISO6976 51.519 91 ISO6976 51.519 91 ISO6976 51.366 C 51.416 92 ISO6976 51.366 C 93 ISO6976 51.366 C 94 ISO6976 51.407 C 95 ISO6976 51.407 C 97 98 ISO6976 51.407 C 99 ISO6976 51.407 C 90 ISO6976 91 ISO6976 91 ISO6976 92 93 ISO6976 94 ISO6976 95 ISO6976 96 ISO6976 97 98 ISO6976 99 ISO6976 90 ISO6976 90 ISO6976 91 ISO6976	011								
91 ISO6976 51.448	1081 1095								
96	191	ISO6976							
97 98 98 99 99 90 90 91 91 92 92 93 95 95 95 95 95 95 95 95 95 95 95 95 95	196								
00	197								
87 ISO6976 51.521	198								
10 15 15 15 15 15 15 15	200	1000070							
20 ISO6976 51.521	287 307	19009/6							
88 ISO6976 51.506	1320	ISO6976							
90 ISO6976 51.519	388								
89 ISO6976 51.386 C 51.297 C first reported 51.351 / 51.262 22	390								
22	1436	1000070		0			_		Continuo anta di Ed. 054 / 54 000
22	489	ISO6976		C			C		TIRST reported 51.351 / 51.262
35	603 622								
54 ISO6976 51.407 C first reported 48.810 first reported 48.	635								
normality OK n 12 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1654	ISO6976	51.407	С					first reported 48.810
n 12 8 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1737								
n 12 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		normality	OK			OK			
mean (n) 51 4827 51.4132 st.dev. (n) 0.07993 0.07943 0.2056 R(claic.) 0.2238 0.2056 unknown un		•							
St.dev. (n) 0.07993						-			
R(calc.) 0.2238									
R(lit.) unknown unknown A A A A A A A A A A A A A A A A A A A									
X A A A A A A A A A A A A A A A A A A A									
A A A A A A A A A A A A A A A A A A A	3 T	. ,				·			
A A A A A A A A A A A A A A A A A A A	7							ĸ	Kernel Density
A A A A A A A A A A A A A A A A A A A	3 +								
A X A A A A A A A A A A A A A A A A A A						Δ Δ	Δ Δ	Δ	2.5 -
A A X 1.5.1.5.5.1.2.5.1.4.5.1.6.5.1.8.52	† -					- "			
Kernel Density State	+	Δ Δ	x ^Δ	-					. /
C C C C C C C C C C		Δ							1.5 -
Kernel Density State	2 +								1 -
Kernel Density State									
Kernel Density S14	1 +								0.5]
S1.6 — S1.5 — A A A S1.3 — A S1.2 — S1.1 — S	1 L								
Kernel Density 51.5 51.4 51.4 51.4 51.1 51.1 51.1 51.1	343	963 1 489 1654	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1191	1390	1320	316	840	51 51.2 51.4 51.6 51.8 52
51.5 -	5				51.6 T				
51.4 - A A A S1.2 - S1.1 - S1	.5 -	∧ Kern	nel Density		E4.E				
51.4	4 -	/ \			01.0				Δ
513 - Δ 512 - 51.1 -	3.5 -	/ \			51.4				Δ Δ
51.3 A S12 - 51.1 - 51.	3 -	/				A		Δ	
51.1	2.5 -	/			51.3				
51.1	2 -	/							
51	.5 -	/			51.2				
51	1	/			F1.1				
	.5 -	/			J1.1				
i1 51.2 51.4 51.6 51.8 52	0								
	51	51.2 51.4 51.6	51.8 52			20 0 20 0	2	191	1320 1320 316

Determination of Caloric Value (sup) (101.325 kPa , comb. temp. 15°C, and metering temp 15°C) on sample #12040; results in MJ/m 3

	method	real gas	mark	z(targ)	ideal gas	mark	z(targ)	remarks
92		38.96	С					reported under 'ideal'
171								
316								
343								
442	ISO6974	38.915			38.822			
444	ISO6976	38.904			38.810			
496	DIN51857	38.858	E, ex		38.765	E, ex		calculation errors?
527			_,			_,		
602	ISO6976	38.4914	G(0.01)		38.4007	G(0.01)		
608	ISO6976	39.097	C			0(0.0.)		first reported 39.104
609	ISO6976	38.984	Č		38.890	С		first reported 38.937 / 38.844
663	D3588	39.00	J			J		mot reported 60.507 / 60.644
					38.9027			
840	ISO6976	38.9970						
868	ISO6976	38.981			38.887			
963	ISO6976	38.770	_					
974	GPA2172	39.177	E, ex					calculation error?
1011								
1081								
1095								
1191	ISO6976	38.935			38.841			
1196								
1197								
1198								
1200								
1287	ISO6976	38.954			38.860			
1307								
1320	ISO6976	38.948			38.854			
1388	ISO6976	38.952			38.858			
1390	ISO6976	38.941						
1436	ISO6976	38.957			38.863			
			C			C		first reported 29 910 / 29 726
1489	ISO6976	38.867	С		38.774	С		first reported 38.819 / 38.726
1603								
1622	1000070							
1635	ISO6976	39.021	_		38.927			
1654 1737	ISO6976	38.914	С					first reported 41.028
	normality n outliers mean (n) st.dev. (n) R(calc.)	OK 18 1 38.9498 0.06768 0.1895			OK 12 1 38.8574 0.04222 0.1182			
39.4 T 39.2 - 39.4 T 39.4 T 38.8 - 38.6 - x 38.4 -	R(lit.) x Δ Δ	unknown	<u>.</u>	- <u>6</u> - 6	unknown	Δ Δ	Δ	7 Kernel Density 6 - 5 - 4 - 3 - 2 - 1 -
92 - 39		unknown	1320	12.87		φ φ φ Δ φ Δ	Δ	6 - Kernel Density 5 - 4 - 3 - 2 - 1 - 0
92 - 39 - 888 - 86 - x 82 -	х Δ Δ	unknown	1350	14.36	unknown		Δ Δ	6 - Kernel Density 5 - 4 - 3 - 2 - 1 - 0 38.2 38.4 38.6 38.8 39 39.2 30 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 - 7 -
92 - 39	х Δ Δ	unknown	1350	14.36	unknown		Δ	6 - Kernel Density 5 - 4 - 3 - 2 - 1 - 0 38.2 38.4 38.6 38.8 39 39.2 38 7 Kernel Density
92 - 339	66 4 11 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	unknown	4 4	12.87	unknown	8 4 0 6 6 3	Δ Δ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6 - Kernel Density 5 - 4 - 3 - 2 - 1 - 0 38.2 38.4 38.6 38.8 39 39.2 3
92 - 39	х Δ Δ	4 4 6 6 6 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1	å å å 330 00 11 12 12 12 12 12 12 12 12 12 12 12 12	1287	unknown	8 4 0 6 6 3	Δ Δ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6 - Kernel Density 5 - 4 - 3 - 2 - 1 - 0 38.2 38.4 38.6 38.8 39 39.2 3
92 - 339 - x 8.8 - x 8.6 - x 8.4 - x 8.2 - 339 - 3	66 4 11 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 6 6 6 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1	1330	12.87	unknown	8 4 0 6 6 3	Δ Δ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6 - Kernel Density 5 - 4 - 3 - 2 - 1 - 0 - 38.2 38.4 38.6 38.8 39 39.2 3 7 - Kernel Density
92 - 39	66 4 11 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 6 6 6 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1	4 4 4 1 3 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	12.88	unknown	8 4 0 6 6 3	Δ Δ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6 - Kernel Density 6 - 4 - 3 - 2 - 1 - 0 - 38.2 38.4 38.6 38.8 39 39.2 3 7 - Kernel Density
92	66 4 11 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 6 6 6 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1	å å (1350)(1350 (1350 (1350 (1350 (1350 (1350 (1350 (1350 (135) (1350 (135)(1350 (1350 (135) (1350 (135) (1350 (135) (1350 (135) (1350 (13	12.87	unknown	8 4 0 6 6 3	Δ Δ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6 - Kernel Density 5 - 4 - 3 - 2 - 1 - 0 - 38.2 38.4 38.6 38.8 39 39.2 3 7 - Kernel Density 6 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 -
339 - 339 - 339 - 339 - 339 - 339 - 339 - 339 - 339 - 339 - 339 - 339 - 339 - 338 - 336 -	66 4 11 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 6 6 6 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 3 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1287	unknown	8 4 0 6 6 3	Δ Δ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6 - Kernel Density 5 - 4 - 3 - 2 - 1 - 0 38.2 38.4 38.6 38.8 39 39.2 3 7 - Kernel Density
339 - x 366 - x 37 - 39 - 39 - 39 - 39 - 39 - 39 - 39 -	66 4 11 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 6 6 6 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1	4 4 4	1287	unknown	8 4 0 6 6 3	Δ Δ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6 - Kernel Density 5 - 4 - 3 - 2 - 1 - 0 38.2 38.4 38.6 38.8 39 39.2 3 7 - 6 - 5 - 4 - 3 - 3 - 3 - 4 - 3 - 3 - 4 - 3 - 3
2 - x	66 4 11 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 6 6 6 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1	å å å	1287	unknown	8 4 0 6 6 3	Δ Δ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	7 Kernel Density 7 6 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 - 4 -
2 - x x 4 - x 2 - 39 7	66 4 11 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 6 6 6 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1	4 4 1330 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1287	unknown	8 4 0 6 6 3	Δ Δ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6 - Kernel Density 5 - 4 - 3 - 2 - 1 - 0 38.2 38.4 38.6 38.8 39 39.2 3 7 - 6 - 5 - 4 - 3 - 3 - 3 - 4 - 3 - 3 - 4 - 3 - 3
2 - x	66 4 11 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 6 6 6 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1	1330	17.88	unknown	8 4 0 6 6 3	Δ Δ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	7 Kernel Density 7 6 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 4
2 - x x 4 - x 2 - 39 7	66 4 11 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	4 4 6 6 6 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1	1320	4	unknown	4 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	Δ Δ 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	7 Kernel Density 7 6 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 3 - 4 - 4

Determination of Density (101.325 kPa , combustion temp. 15°C, and metering temp. 15°C)

on samp	ole #12040;	results	in k	g/m ³

Lab	method	real gas	mark	z(targ)	ideal gas	mark	z(targ)	remarks
92	GPA2286	0.778	С		0.776			first reported 0.774
71								
316								
43	1000074	0.7774			0.7750			
42	ISO6974	0.7771			0.7753			
144 196	ISO6976 DIN51857	0.7788 0.7779			0.7769 0.7760			
527	D11401001	0.7779						
02	ISO6976	0.7756	ex		0.7737	G(0.05)		see §4.1
08	ISO6976	0.7783	C					first reported 0.7782
09	ISO6976	0.7781	С		0.7762	С		first reported 0.7770 / 0.7551
63	D3588	0.6339	G(0.01)					
40	ISO6976	0.77841			0.77653			
868 163	ISO6976	0.7782			0.7763			
63 74	ISO6976 GPA2172	0.7766 0.7763						
11	D3588	0.7789	С		0.7767	С		first reported 0.7787 / 0.7765
81	20000		-			-		
95								
91	ISO6976	0.7798			0.7779			
96								
97								
98								
200	1000070							
87	ISO6976	0.7785						
307	1906076	0 7792			0.7764			
320 388	ISO6976 ISO6976	0.7783 0.7789			0.7764 0.7770			
900 390	ISO6976	0.7789			0.7770			
136	ISO6976	0.7789			0.7771			
189	ISO6976	0.7791	С		0.7772	С		first reported 0.7782 / 0.7764
03								•
22								
35	ISO6976	0.7820	G(0.05)		0.7801	G(0.05)		<i>r</i>
54 37	ISO6976	0.7801	С					first reported 0.7796
	normality n outliers mean (n) st.dev. (n) R(calc.) R(lit.)	OK 19 2 0.7783 0.00095 0.0027 unknown			OK 13 2 0.7766 0.00066 0.0019 unknown			
							*	450 400 - 350 - Kernel Densi
ĺ						_ Δ	Δ Δ	300 -
		Δ Δ Δ	Δ Δ	Δ Δ	A			250 -
	Δ Δ							200 -
	x							
								150 -
								100 -
								50 -
663	602 974 963 442	496 92 1390	609 868 1320	608	1287 444 1436	101 1489	1654 1635	0.77 0.775 0.78
		<u> </u>		0.782 _T		•	· · ·	
	Vo.	nel Density		0.702				
	∧ Kei	not beliatly		0.78				
	7.1							
	\bigcap	1 1		1 1				
-	$\left\{ \right\}$			0.778				
				0.778 -				
-				0.778 -	Δ	Δ Δ	Δ	<u> </u>
-				0.776 -	Δ	Δ Δ	Δ Δ	Δ Δ Δ Δ Δ
) -) -) -) -) -						Δ Δ	Δ Δ	<u> </u>
-				0.776 - 0.774 - x		Δ Δ	Δ	<u> </u>
-				0.776 -		Δ	Δ	<u> </u>

442

0.78

0.77

0.785

1635

Determination of Relative Density (101.325 kPa , comb. temp. 15°C, and metering temp. 15°C) on sample #12040; unit less results

la			tho				eal g	as		ark	z(t	arg)		deal (gas	m	ark	z(t	arg)		marks
	2	GΡ	A22	86			.636		С				0	.634						firs	t reported 0.632
17																					
31																					
34		100)eo-	7.1				,							,						
44			0697				.6342							.6329							
44			0697				.6356							.6343		_	٥.,			امما	aulation array?
49		יווט	N518	557			.6348	5						.6333)		, ex			Cai	culation error?
52 60		ICC	0697	76			 .6329	`	G	(0.05)				 .6317	7	G	(0.05)			200	e §4.1
60)697				.6351		G	(0.03)				.0317		G	(0.03)			366	5 84.1
60)697				.6350		С					.6337	7	С				fire	t reported 0.6341 / 0.6328
66			588	U			.6352		O							O				1113	1 reported 0.0041 / 0.0020
84)697	76			.6352							.6339	95						
86			0697				.6350							.6338							
96			0697				.6340														
97			A21				.6335		Е	, ex										cal	culation error?
101										, -											
108	31																				
109																					
119	91	ISC	0697	76		0	.6363	3					0	.635	l						
119	96																				
119																					
119		_																			
120			588				.6349														
128		ISC	0697	76			.6353	3													
130								_						- 							
132			0697				.6351							.6338							
138			0697				.6356							.6344	ļ						
139			0697				.6348														
143			0697				.6356		_					.634		_				c	1 1 0 0050 / 0 0000
148		150	0697	б			.6358	3	С					.634)	С				TITS	t reported 0.6350 / 0.6338
160																					
162 163		ICC	0697	76			 .6381	1	G	(0.05)				 .6369)	D	(0.05)				
165)697				.6366		C	(0.05)				.0308	,	D	(0.05)			fire	t reported 0.6362
173		130	Josi	O				,	C											1115	r reported 0.0302
		n out me st.c	mali liers an (dev. calc.	n) (n)		1 2 0 0	0K 9 1.6353 1.0006 1.0018 Inkno	64 3					1 2 0 0		56 S						
		17(1	11.)			u	TIKITO	VVII					u	TIKITO	VVII						
639 T																					600
638 -																				×	↑ Kernel Density
337																					500 -
																		Δ	Δ		400 -
36 -														Δ	Δ	Δ 4	Δ				400 -
35 -					Δ	Δ	Δ	Δ	Δ	Δ Δ	Δ	Δ								_	300 -
34 -			Δ	Δ																	
		x																			200 -
533 -	×]] /
332 +																					100 -
631 -																					0
631 -				4 4 2	4 96	1390	1200	8 6 8	609	1320	663	8 40	1287	4 4 4	1388	1436	92	1191	1654	1635	0.63 0.632 0.634 0.636 0.638 0
31 -	602	974	963		-	==	=			= 3			=	-	=	÷ :	-	÷	=	=	
.63	602	974	963	4																	700
.63	602	974	963	4																	
63 — 63 —	602	974	963																	K I	Kernel Density
631 + 63 - 638 T	602	974	963																	*	
631 + 1.63 - 638 T 637 +	602	974	963																	`	Kernel Density
	602	974	963	4														Δ		«	600 - Kernel Density
31 + 63 - 38 T 37 + 36 + 35 +	602	974	8983	4									Δ	Δ		Δ	Δ	Δ			600 - Kernel Density
31 + 63 - 38 T 37 + 36 + 35 +	602	974	896			Δ	Δ		Δ	Δ	Δ		۵	Δ		Δ	Δ	Δ		·	600 - Kernel Density
331 +	602	974	663	x		Δ	Δ		Δ	Δ	Δ		۵	Δ		Δ	Δ	Δ			600 - Kernel Density 500 - 400 - 300 -
331 - 338 T 337 - 336 - 335 - 334 -		974	£968			Δ	Δ		Δ	Δ	Δ		۵	Δ		Δ	Δ	Δ		·	600 - 500 - 400 -
331 - 338 T 337 - 336 - 335 - 334 - 332 -	e05	47.0	963			Δ	Δ		Δ	Δ	Δ		Δ	Δ		Δ	Δ	Δ			600 - Kernel Density 500 - 400 - 300 - 200 -
631 + 1.63 - 638 T 637 + 636 +		47.6	Δ			Δ	Δ		Δ	Δ	Δ		۵	Δ		Δ	Δ	Δ			600 - Kernel Density 500 - 400 - 300 -
331 - 338 T 337 - 336 - 335 - 334 - 332 -		974	٩42 🔻			Δ 609	A		Δ Δ	940 A	<u>4</u>		436	444		A	1489	1611			600 - Kernel Density 500 - 400 - 300 - 200 -

Determination of Wobbe Index (101.325 kPa , combustion temp. 15°C, and metering temp. 15°C) on sample #12040; results in MJ/m 3

CO.	me	thod				gas	;	mark	(Z	(targ)		ideal gas	r	mark	-	z(targ	remarks
92 171																		
316																		- -
343																		_
442	ISC	06974	1		48.8	37												-
444		06976			48.7							-						-
496		N5185			48.7							-	48.713		E, ex			- calculation error?
527																		_
602	ISC	06976	;		48.3	3831		G(0.0	01)			-	48.4300		E, ex			calculation error? real < ideal?
608		06976			49.0			С										
609		06976	;		48.9			С				-	48.853	(0			- first reported 48.898 / 48.829
663		588			48.9													-
840		06976				9292							48.8598					-
868		06976			48.9								48.848					
963		06976			48.6			_										
974 011	GP	A217	2		48.9			С										mot reported 10.22
081																		
095																		
191	ISC	06976	3		48.8								48.739					
196	100	70370	,															
197																		
198																		
200												-						-
287	ISC	06976	3		48.8	373						-						-
307		_				-						-						_
320	ISC	06976	3		48.8	373						-	48.803					-
388	ISC	06976	3		48.8	358							48.788					-
390	ISC	06976	;		48.8							-						
436		06976			48.8	362							48.745		E, ex			 calculation error?
489	ISC	06976	;		48.7	744		С				-	48.677	(2			- first reported 48.716 / 48.643
603												-						-
622																		-
635		06976			48.8			_				•	48.778					
654 737	ISC	06976	j		48.7			С										ot roportou o rrior
	n out me st.d	mality liers an (n) dev. (r calc.) it.))		0.08	3577 3256	1						OK 8 0 48.7932 0.06303 0.1765 unknown					
т																		
x	Δ	Δ	Δ	Δ	Δ	Δ	Δ	Δ	۵	Α	Å	Δ	Δ Δ	Δ	Δ	Δ	Δ	5 4.5 4 - 3.5 - 3 - 2.5 - 2 - 1.5 - 1 -
802 8	Δ 893	7 A	1654	9.64		7611 A	1635	1388	1436	442	1320	1287	1380 974	∆	609	840		4.5
x					Δ		Δ	1388	1436	442	1320	1287	A		609	840	Δ 608 90 90 90 90	4.5
x x 8002					Δ		Δ	1088	1436	442	1320	1287	A		609		Δ	4.5 . Kernel Density 4.5
x x		1489			Δ		Δ	00 00 00 TT	43.6	442	1320	1287	A	898	609	840	Δ 608 90 90 90 90	4.5
x x				96	Δ	1191	Δ		4 3 9 6	442	1320	1287	A	898	609	840	Δ 608 90 90 90 90	4.5 . Kernel Density 4.5
x		1489		96	Δ	1191	Δ		1,436	442	1320	1287	A	898	609	840	Δ 608 90 90 90 90	4.5
x x 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8983	1489		96	Δ	1191	Δ		1436	442	1320	1287	A	898	609	840	Δ 608 90 90 90 90	4.5
x	8983	1489		96	Δ	1191	Δ		14 36	4 4 2	1320	4 1287	A	898	609	840	Δ 608 90 90 90 90	4.5
e005	8983	1489		96	Δ	1191	Δ		60.57	4 4 2	1320	1287	A	898	609	840	Δ 608 90 90 90 90	4.5
e005	8983	1489		96	Δ	1191	Δ		14.06	442	1320	1287	A	898	609	840	Δ 608 90 90 90 90	4.5
x x e e e e e e e e e e e e e e e e e e	8983	1489		96	Δ	1191	Δ		1436	442	1320	1287	A	898	609	840	Δ 608 90 90 90 90	4.5 . Kernel Density 4 - 3.5
602	8983	1489		96	Δ	1191	Δ		1436	442	1320	1287	A	898	609	840	Δ 608 90 90 90 90	4.5

APPENDIX 2

Compression factors used by participants

lab	Compressibility factor @15°C	Compressibility factor @0°C
92	0.9976	
171		
316		0.997
343		1.0024
442	0.9976	
444	0.9976	0.9971
496	0.998	0.997
527		
602	0.997573	
608	0.9975	
609	0.997594402	
663	0.9976	
840	0.99758	0.99709
868	0.9976	0.9971
963	0.9976	0.9976
974	0.9977	0.9977
1011	1.003	
1081		
1095		
1191	0.9976	
1196		
1197		
1198		
1200		
1287	0.99759	0.99709
1307		
1320	0.99759	0.99710
1388	0.997587102	0.997587102
1390	0.9976	0.9971
1436	0.9976	
1489	0.9976	0.9971
1603		
1622		
1635	0.9976	
1654	0.9976	0.9971
1737		

APPENDIX 3

Number of participants per country

- 2 labs in BELGIUM
- 1 lab in CANADA
- 1 lab in CROATIA
- 1 lab in FINLAND
- 1 lab in FRANCE
- 2 labs in GERMANY
- 1 lab in HUNGARY
- 1 lab in INDONESIA
- 1 lab in ITALY
- 6 labs in MALAYSIA
- 1 lab in MEXICO
- 3 labs in P.R. of CHINA
- 2 labs in PORTUGAL
- 2 labs in SAUDI ARABIA
- 1 lab in SLOVAK REPUBLIC
- 1 lab in SPAIN
- 1 lab in THAILAND
- 2 labs in THE NETHERLANDS
- 1 lab in TURKEY
- 1 lab in U.A.E.
- 1 lab in U.S.A.
- 2 labs in UNITED KINGDOM
- 1 lab in VIETNAM

APPENDIX 4

Abbreviations:

C = final result after checking of first reported suspect result

 $\begin{array}{ll} D(0.01) &= \text{outlier in Dixon's outlier test} \\ D(0.05) &= \text{straggler in Dixon's outlier test} \\ G(0.01) &= \text{outlier in Grubbs' outlier test} \\ G(0.05) &= \text{straggler in Grubbs' outlier test} \\ DG(0.01) &= \text{outlier in Double Grubbs' outlier test} \\ DG(0.05) &= \text{straggler in Double Grubbs' outlier test} \\ \end{array}$

ex = excluded from calculations

n/a = not applicable

W = withdrawn on request participant

U = reported in wrong unit
E = error in calculations
SDS = Safety Data Sheet

Literature:

- 1 iis Interlaboratory Studies, Protocol for the Organisation, Statistics and Evaluation, January 2010
- 2 ISO 6974, Natural Gas Determination of composition with defined uncertainty by GC
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- 5 ISO 5725-86
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- 7 M. Thompson and R. Wood, J. AOAC Int, <u>76</u>, 926, (1993)
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- 11 P.L. Davies, First reported Z. Anal. Chem, <u>331</u>, 513, (1988)
- 12 J.N. Miller, Analyst, <u>118</u>, 455, (1993)
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- The Royal Society of Chemistry 2002, Analyst 2002, 127 page1359-1364, P.J. Lowthian and M.

Thompson. (see http://www.rsc.org/suppdata/an/b2/b205600n/)

15 ASTM D1945, Standard test method for Analysis of Natural Gas by GC